Installation and Verification Results Work Area 2 Stone Column Test Areas Third Runway Embankment Phase 4 SeaTac, Washington



Prepared for HNTB

July 24, 2001 4978-44

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Prepared by Hart Crowser, Inc.



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INSTALLATION AND VERIFICATION RESULTS WORK AREA 2 STONE COLUMN TEST AREAS THIRD RUNWAY EMBANKMENT PHASE 4 SEATAC, WASHINGTON

INTRODUCTION

This report provides a description of the installation and verification of stone columns in four Test Areas of Work Area 2 at the Third Runway Project. Work Area 2 is part of the Embankment Phase 4, and is located to the north of South 156th Street, and to the west of abandoned 12th Avenue South in SeaTac, Washington. Figure 1 is a Vicinity Map of the project area.

This report contains the following:

- Summary;
- Purpose and scope of this report;
- Overview of the stone column test program;
- Discussion of the individual Test Areas; and
- Appendices providing boring logs and cone penetrometer logs recorded before and after the installation of stone columns within each Test Area, as well as pertinent laboratory soil test data.

SUMMARY

Stone column installation tests were completed in Work Area 2 in June 2001. Four test areas were evaluated to assess changes in stone column installation procedure, spacing, and soil variability.

Based on our review, we conclude that while much of the data shows the stone column installations are consistent with expectations, there is significant variability between test results at close spacing. In our opinion, the ambiguity in the verification test data is unacceptable to justify reliance on this method of subgrade improvement for the Third Runway.

Since the four test sections represent the soil conditions we expect for much of the subgrade improvement areas, the results show it would not be practical to

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rely on the verification test results to assure adequate quality control for this project. We note that both the contractor's methods and the verification test procedures in the specs are industry standard for this method of ground improvement, and there is no other generally accepted alternative for quality control. (For instance, it is conceivable but would be problematic to implement a performance spec based on shear wave velocity or load tests, on a production basis).

PURPOSE AND SCOPE OF THIS REPORT

The purpose of this report is to provide a summary and analysis of the Stone Column Test Program that was performed as part of the Phase 4 Embankment work for Third Runway.

The scope of this report includes:

- A general description of the test program;
- A description of each test area;
- A discussion of observations during stone column construction;
- A discussion of the verification program consisting of SPT-N borings and CPT probes, and conclusions drawn from verification testing; and
- Collection of data relative to stone column installation and verification testing.

OVERVIEW OF TEST PROGRAM

Background on Stone Column Work

Stone columns were proposed as an alternative to overexcavation and replacement of potentially liquefiable soils and compressible soils within the embankment subgrade. The intent of stone columns is to densify loose sands and/or provide additional stiffness by vibrating crushed rock into the ground in a regular pattern. Stone columns are designed using the concept of "Area Replacement Ratio," a number represented as A, and calculated as the percentage of stone emplaced within the tributary area of one stone column. The test patterns in Work Area 2 were designed for A, values of 17 and 35 percent.

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Four separate test areas were completed in Work Area 2. The locations of Test Areas 1 through 4 are shown on Figure 2. Verification testing was performed before and after stone column installation, which allowed evaluation of changes in subgrade density resulting from the stone column work. Verification testing included SPT-N blowcounts recorded at 2.5-foot-depth intervals in hollow-stem auger borings, as well as continuous cone tip resistance measured during cone penetration (CPT) tests. In addition, pore pressure dissipation tests were performed at various depths in CPT-05, CPT-06, and CPT-08. Results of these tests are included following the CPT logs, which have been attached with the boring logs in Appendices A through D.

Specifications for the store column work state that acceptance criteria include a measured corrected cone tip resistance of at least 110 tons per square foot, or a measured SPT-N value of at least 22 blows per foot in the verification explorations performed after stone column work. These minimum values are shown as red lines on the summary plots provided in the appendices.

Selected samples taken from borings in Test Areas 1 and 2 were submitted for laboratory grain size analysis. A discussion of these analyses and the test results are presented in Appendix E.

As part of ongoing work for the Third Runway project, Hart Crowser performed several studies in the general area of Work Area 2 that involved test pit explorations and borings. Selected soil samples from these explorations underwent laboratory grain size analyses and Atterberg limits tests. Appendix F presents the results of these tests from previous work in the area.

Hart Crowser Performed Construction QA during Column Installation

During installation of Stone Columns in Test Areas 1 through 4, a Hart Crowser representative was continuously present to record the following data for each stone column:

- Stone column depth of penetration and tip elevation;
- Amount of stone (weight) placed in each column;
- Power demand (in amps) from the probe vibrator; and
- Time required for probe penetration and column construction.

These data allowed us to compute an average column diameter for a given depth interval, as well as an overall average column diameter. Based on our

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observations, it appears that the contractor was successful in achieving the required minimum diameter for stone columns in Work Area 2.

Probe Amperage Monitored and Recorded

As part of the installation monitoring process, a Hart Crowser field representative observed the amperage required to power the vibrating probe during initial probe penetration and subsequent stone column construction (probe withdrawal and repenetration).

It is commonly accepted that higher amperage is related to denser ground conditions, and in some cases stone column contracts require that a minimum amperage be attained while building the column up from the base. In addition, amperage is used to define probe refusal. The contractor for the Third Runway project submitted a work plan that stated maximum probe amperage would be 280 amps for this project.

During typical stone column construction in soft ground, we would normally expect relatively low amperage (on the order of about 150 to 180 amps) at the start of column construction, with the amperage increasing to about 250 amps or higher as compacted stone is continually placed in successive lifts during column construction. Where the probe encounters dense ground refusal at its tip elevation, amperage could be greater than 200 amps at the base of the column, increasing up to over 300 amps during subsequent column construction.

DISCUSSION OF INDIVIDUAL TEST AREAS

Test Area 1

Stone Column Layout

Test Area 1, shown on Figure 2, was completed near the southeast corner of Work Area 2, and had an average ground surface elevation of about 291 feet before stone column work commenced. The test pattern in this area consisted of 32 42-inch-diameter stone columns in a triangular pattern at 8 foot center to center spacing as shown on Figure 3. With the exception noted in the following paragraph, this pattern resulted in a minimum A, for Test Area 1 of 17 percent. Column depths ranged from 17 to 19 feet below ground surface, corresponding to a stone column tip elevation ranging from about 272 to about 274 feet.

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In the southeast corner of Test Area 1, nine additional 28-inch-diameter columns were installed to depths ranging from 15 to 18 feet below ground surface in the center of the triangular pattern to achieve a minimum A_r of 35 percent in this area.

Installation Observations

During installation of stone columns in Test Area 1, water was observed flowing from newly constructed columns up to the ground surface. This phenomenon led to softening of the upper soils, a problem which was exacerbated by rainy weather that soaked the ground around the site. Because the upper soils in the work area became very soft, the front-end loader used during the stone column installation caused deep rutting in the ground surface. The ground surface surrounding the stone columns heaved on the order of about 1 to 3 feet, and this soil was continuously removed during installation to facilitate work activities. In addition to heave at the ground surface, the probe was observed to have substantial cohesive soils sticking to it as it was withdrawn from the hole. This relatively "dirty" probe could be attributed to either the upper soft native soils, or disturbance of relatively stiff native cohesive soils at depth.

During construction of the columns in Test Area 1, the amperage of the probe was observed to remain relatively steady at about 160 to 200 amps as the column was being built to the ground surface. These amp readings are lower than we would normally expect to see as crushed rock in the column is compacted. We attribute the low amp readings to soft ground conditions encountered during construction, which may have resulted in lateral spread of the crushed rock as it was dropped from the base of the probe.

Verification Test Program and Results

Test Program Description. Within Test Area 1, two borings and two cone penetrometers were advanced prior to the installation of stone columns. After completing columns in this area, about 1 foot of ground heave was bladed off the top of the Test Area to try to locate the tops of the stone columns. The ground was allowed to dry for several days to facilitate access for the testing equipment. Six days after columns were complete, three borings were advanced in Test Area 1. Seven days after columns were completed, two cone penetrometers were advanced in this area. Fifteen days after completion of stone columns, one additional boring and one additional cone penetrometer were advanced in Test Area 1. Table 1 lists the numerical designation and location of explorations in Work Area 2, relative to their respective Test Areas.

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Figure 3 provides a map of the stone column layout relative to the explorations advanced before and after column installation. Appendix A contains a summary plot of the borings and cone penetrometers, as well as the individual logs recorded for each of the borings and cone penetrometers in Test Area 1.

Test Program Results. CPT data recorded after stone column installation indicate that some densification occurred from 0 to 6 feet below the ground surface where clean sand is present. The CPT data did not indicate significant change in density for the silty sands present from 6 to 10 feet below the ground surface.

In contrast to the CPT data, the SPT data indicated little improvement in the 0- to 6-foot-depth range after 7 days, and some possible improvement in this area 15 days after column completion. Below 6 feet, SPT data indicated that density might have actually decreased during stone column installation.

Prior to stone column installation, CPT refusal occurred at a depth of 14 feet. After stone column installation, CPT refusal occurred between depths of 16 to 18 feet. This suggests that the deeper soils may have been disturbed during stone column installation.

Test Area 2

Stone Column Layout

Test Area 2 was completed immediately to the north of Test Area 1, as shown on Figure 2, and had an average ground surface elevation of about 291 feet before stone column work commenced. The test pattern in this area consisted of 32 36-inch-diameter stone columns in a triangular pattern at 7-foot center to center spacing. With the exception noted in the following paragraph, this pattern resulted in a minimum A, for Test Area 2 of 17 percent. Column depths ranged from 18 to 19 feet below ground surface, corresponding to a stone column tip elevation ranging from about 272 to about 273 feet.

Similar to Test Area 1, in the southeast corner of Test Area 2, nine additional 25inch-diameter columns were installed to depths ranging from 18 to 19 feet below ground surface in the center of the triangular pattern to achieve a design A, of 35 percent.

Installation Observations

As in Test Area 1, during installation of stone columns in Test Area 2 water was observed flowing from newly constructed columns up to the ground surface.

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This phenomenon led to softening of the upper soils, a problem which was exacerbated by rainy weather that soaked the ground around the site. Because the upper soils in the work area became very soft, the front-end loader used during the stone column installation caused deep rutting in the ground surface. The ground surface surrounding the stone columns heaved on the order of about 1 to 3 feet, and this soil was continuously removed during installation to facilitate work activities. Again as in Area 1, the probe was relatively dirty during withdrawal.

During construction of the columns in Test Area 2, the amperage of the probe was observed to range between about 140 to 220 amps as the column was being built to the ground surface. Again we attribute the low amp readings to soft ground conditions encountered during construction, which may have resulted in lateral spread of the gravel as it was dropped from the base of the probe.

Verification Test Program and Results

Test Program Description. Within Test Area 2, two borings and two cone penetrometers were advanced prior to the installation of stone columns. After completing columns in this area, about 1 foot of ground heave was bladed off the top of the Test Area to try to locate the tops of the stone columns. The ground was allowed to dry for several days to facilitate access for the testing equipment. Five days after columns were complete, two borings were advanced in Test Area 2. Six days after columns were completed, two cone penetrometers were advanced in this area. Fourteen days after completed, two cone penetrometers were advanced in this area. Fourteen days after completion of stone columns, one additional boring, and one additional cone penetrometer were advanced in Test Area 2. Table 1 lists the numerical designation and location of explorations in Work Area 2, relative to their respective Test Areas.

Figure 3 provides a map of the stone column layout relative to the explorations advanced before and after column installation. Appendix B contains a summary plot of the borings and cone penetrometers, as well as the individual logs recorded for each of the borings and cone penetrometers in Test Area 2.

Test Program Results. Data recorded by CPT-10 after stone column installation indicate apparent densification of sand from 0 to 5 feet below ground surface where clean sand is present. The other two CPT tests (CPT-7 and CPT-8) show that the density of this upper soil, interpreted to be silty and clayey sand, was not much improved by the stone columns. The CPT tests show good improvement from depths of 5 to 9 feet, but between 8 and 18 feet, the tip resistance recorded in CPT-10 is in sharp contrast to that recorded in CPT-7 and CPT-8.

Overall, the SPT blowcounts appear to have not changed, or to be somewhat reduced following stone column work.

Prior to stone column installation, CPT refusal occurred at a depth of 14 feet. After stone column installation, CPT refusal occurred at 17 feet. This suggests that the deeper soils may have been disturbed during stone column installation.

Test Area 3

Stone Column Layout

Test Area 3 was completed along the western edge of Work Area 2, near N21018/E10709, and had an average ground surface elevation of about 283 feet before stone column work commenced. The test pattern in this area consisted of 41 42-inch-diameter stone columns in a triangular pattern at 5.8-foot center to center spacing. This pattern resulted in a minimum A, for Test Area 3 of 35 percent. Column depths ranged from 9 to 12 feet below ground surface, corresponding to a stone column tip elevation ranging from about 271 to about 274 feet.

Installation Observations

During installation of stone columns in Test Area 3, the ground surface remained dry, and very little water was brought to the surface through existing columns. Hart Crowser's field representative worked closely with the stone column crane operator to define refusal criteria that were intended to limit any disturbance of the stiff to hard cohesive soils that were present below depths of about 12 feet. These criteria were relatively subjective and required close observation of the behavior and sound of the vibrator probe. Although amperage was continuously monitored during the initial probe advance, the presence of the stiff to hard underlying soils was not definitively indicated by consistent higher amperage. Based on the cleanliness of the probe, as well as the lack of heave at the ground surface, it is likely that there was not significant penetration of the vibrator probe into the stiff to hard underlying soils.

During construction of the columns in Test Area 3, the amperage of the probe was observed to range from about 250 to 300 amps as the column was being built up to the ground surface. These higher amperage readings indicate higher compaction within the stone column, which suggests that the surrounding soils were also being densified.

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Verification Test Program and Results

Test Program Description. Within Test Area 3, two borings and four cone penetrometers were advanced prior to the installation of stone columns. After completing columns in this area, about 6 inches of the ground surface was bladed off the top of the Test Area to locate the tops of the stone columns. Six days after columns were complete, two borings and two cone penetrometers were advanced in this area. Table 1 lists the numerical designation and location of explorations in Work Area 2, relative to their respective Test Areas.

Figure 4 provides a map of the stone column layout relative to the explorations advanced before and after column installation. Appendix C contains a summary plot of the borings and cone penetrometers, as well as the individual logs recorded for each of the borings and cone penetrometers in Test Area 3.

Test Program Results. The four CPT tests performed prior to stone column work show inconsistent tip resistance in the depth interval from 2 to 6 feet. Comparing CPT results after stone column installation, CPT-21 indicates that density decreased in this interval, while CPT-22 indicates large improvement in tip resistance from depths of 2 to 6 feet. In the depth range of 6 to 12 feet, results from CPT-21 and CPT-22 contrast one another, and alternatively indicate lower tip resistance when compared to the four CPT tests performed prior to stone column construction.

The SPT results indicate no improvement in density in the depth interval from 0 to 10 feet, while below a depth of 10 feet, blowcounts decreased following stone column installation, indicating looser subgrade conditions.

Test Area 4

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Stone Column Layout

Test Area 4 was completed near the northern limit of Work Area 2, as shown on Figure 2, and had an average ground surface elevation of about 287 feet before stone column work commenced. The test pattern in this area consisted of 41 42-inch-diameter stone columns in a triangular pattern at 8-foot center to center spacing. This pattern resulted in a minimum A, for Test Area 4 of 17 percent. Column depths ranged from 13 to 16 feet below ground surface, corresponding to a stone column tip elevation ranging from about 271 to about 275 feet, with the majority of columns tipped at 274 feet.

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Installation Observations

During installation of stone columns in Test Area 4, the ground surface remained dry, and very little water was brought to the surface through existing columns. At some column locations, a cone of depression formed around the probe during initial penetration, indication densification of the sands surrounding the probe. As in Test Area 3, Hart Crowser's field representative worked closely with the stone column crane operator to define refusal criteria that were intended to limit any disturbance of the stiff to hard cohesive soils that were present below a depth of about 15 feet. These criteria were relatively subjective and required close observation of the behavior and sound of the vibrator probe. Although amperage was continuously monitored during the initial probe advance, the presence of the stiff to hard underlying soils was not definitively indicated by consistent higher amperage. Based on the cleanliness of the probe, as well as the lack of heave at the ground surface, it is likely that there was not significant penetration of the vibrator probe into the stiff to hard underlying soils.

During construction of the columns in Test Area 4, the amperage of the probe was observed to range from about 220 to 300 amps as the column was being built up to the ground surface. These higher amperage reading indicate denser soil conditions within the stone column, which suggests that the surrounding soils were also being densified.

Verification Test Program and Results

Test Program Description. Within Test Area 4, two borings and four cone penetrometers were advanced prior to the installation of stone columns. After completing columns in this area, about 6 inches of the ground surface was bladed off the top of the Test Area to locate the tops of the stone columns. Two days after columns were complete, two borings and two cone penetrometers were advanced in this area. Table 1 lists the numerical designation and location of explorations in Work Area 2, relative to their respective Test Areas.

Figure 5 provides a map of the stone column layout relative to the explorations advanced before and after column installation. Appendix D contains a summary plot of the borings and cone penetrometers, as well as the individual logs recorded for each of the borings and cone penetrometers in Test Area 4.

Test Program Results. The four CPT tests performed prior to stone column work show significant variability in tip resistance in the depth interval from 0 to 8 feet. Comparing CPT results after stone column installation, CPT-20 shows no improvement in tip resistance compared with CPT-11 down to a depth of 5 feet, with some improvement from depths of 5 to 7 feet. CPT-19 indicates

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improvement in tip resistance from 0 to 6 feet when compared to CPT-14, but no change in tip resistance in the silts and clays down to depths of about 13 feet. CPT-19 had deeper refusal after stone column work compared to CPT-14, indicating that there was potentially some disturbance of the stiff to hard cohesive soils at the base of the stone columns.

The SPT results suggest some improvement has occurred in the density of the sand and silty sand subgrade.

USE OF THIS REPORT

Hart Crowser's work on this project was performed, and this report prepared, in accordance with generally accepted geotechnical engineering practices for the nature and conditions of the work completed in the same or similar localities at the time the work was performed. This report is intended for the exclusive use of HNTB Corporation and the Port of Seattle for specific application to the site described herein. No other warranty, express or implied, is made.

Please call if you have any questions.

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Table 1 - Summary of Explorations in Test Areas

Test Area 1 - Completed Worzool		
Borings before stone column installation	Borings after stone column installation	Interval between completion of columns and exploration
B-1	B-1a	6 days
B-2	B-2a	6 days
	B-5a	6 days
	B-7a	15 days

Cones before stone column installation	Cones after stone column installation	interval between completion of columns and exploration
CPT-3	CPT-5	7 days
CPT-4	CPT-6	7 days
	CPT-9	15 days

Test Area 2 - Completed 6/6/2001

Borings before stone column installation	Borings after stone column installation	Interval between completion of columns and exploration
B-3	B-3a	5 days
B-4	B-4a	5 days
	B-6a	14 days

Cones before stone column installation	Cones after stone column installation	Interval between completion of columns and exploration
CPT-1	CPT-7	6 days
CPT-2	CPT-8	6 days
	CPT-10	14 days

Test Area 3 - Completed 6/21/2001

Borings before stone column installation	Borings after stone column installation	Interval between completion of columns and exploration
B-12	B-22a	6 days
B-13	B-23a	6 days

Cones before stone column installation	Cones after stone column installation	Interval between completion of columns and exploration
CPT-15	CPT-21	6 days
CPT-16	CPT-22	6 days
CPT-17		
CPT-18		

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Table 1 - Summary of Explorations in Test Areas

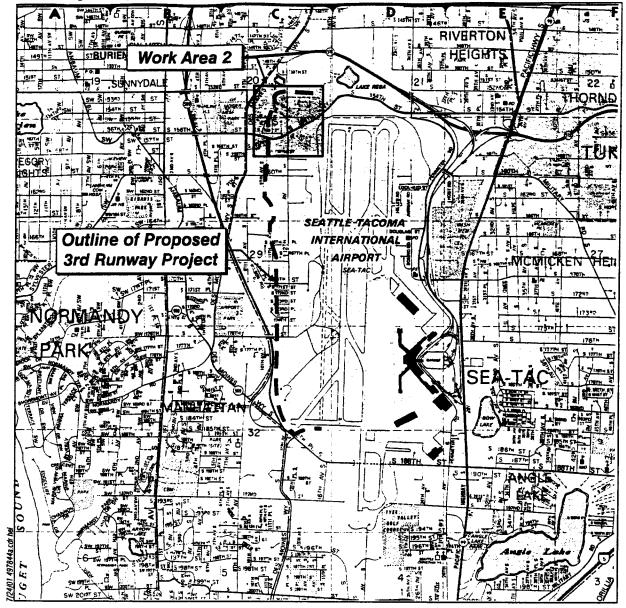
st Area 4 - Completed 6/25/2001			
Borings before stone column installation	Borings after stone column installation	Interval between	
B-10	B-20a	2 days	
B-11	B-21a	2 days	

lated 6/25/2001 Tes B s

Cones before stone column installation	Cones after stone column installation	Interval between completion of columns and exploration
CPT-11	CPT-19	2 days
CPT-12	CPT-20	2 days
CPT-13		
CPT-14		

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Vicinity Map



0 2000 **400**0 Scale in Feet



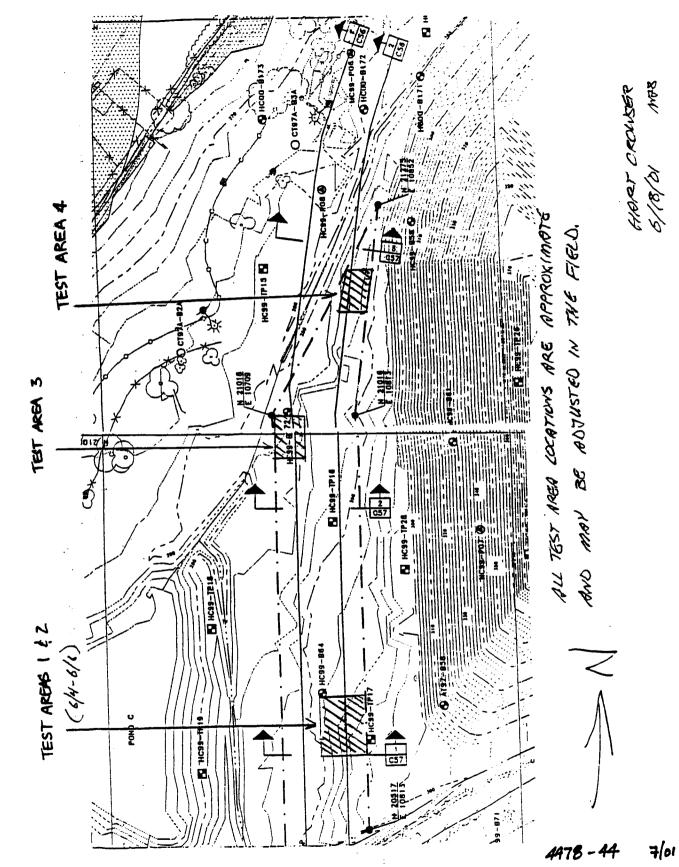
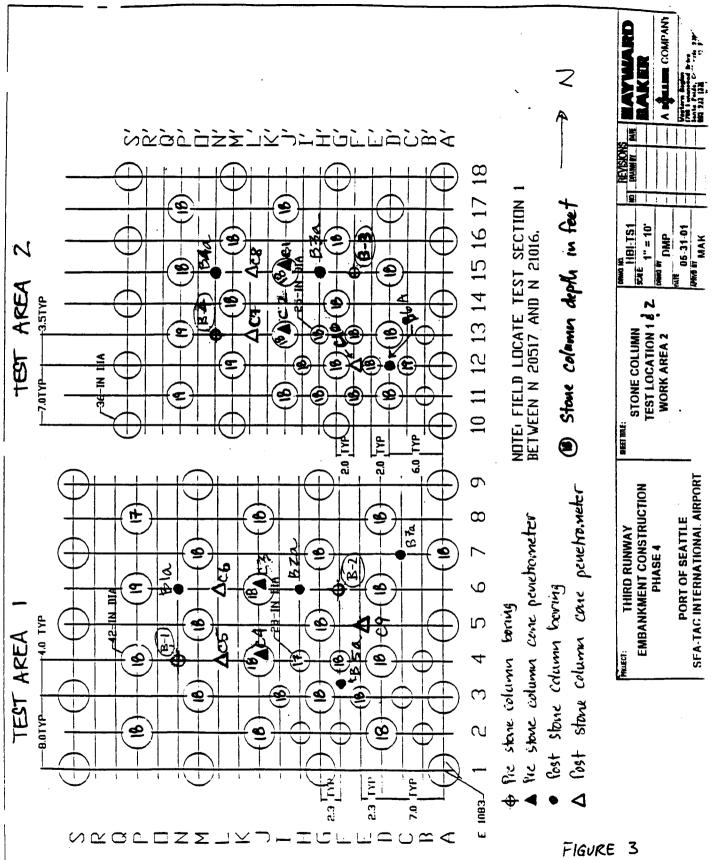
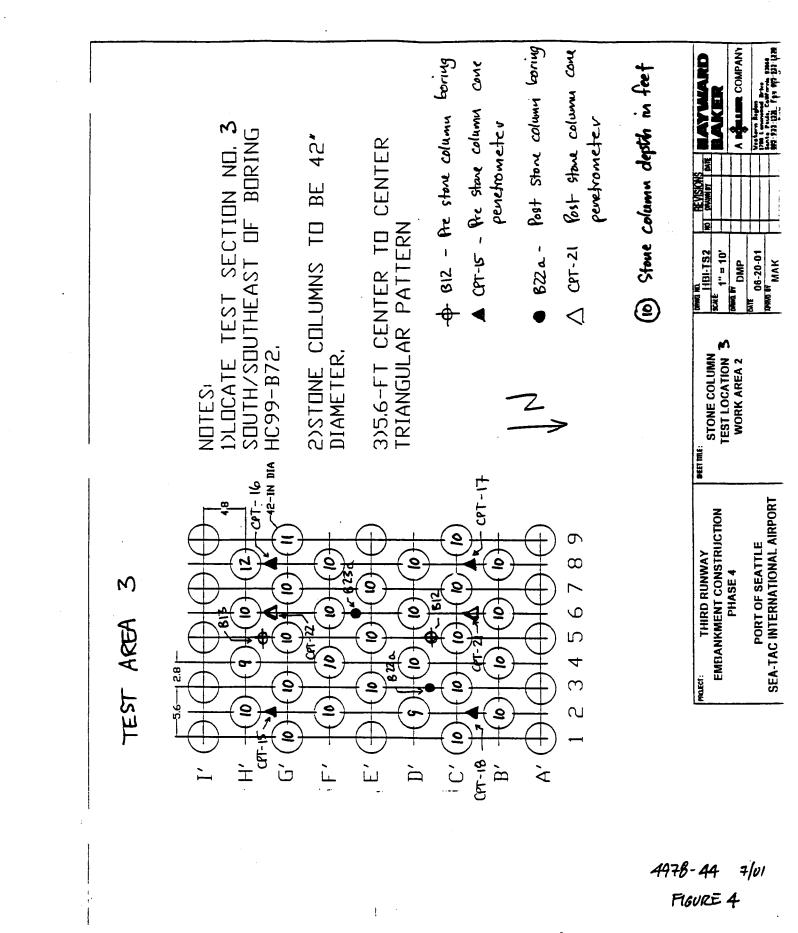


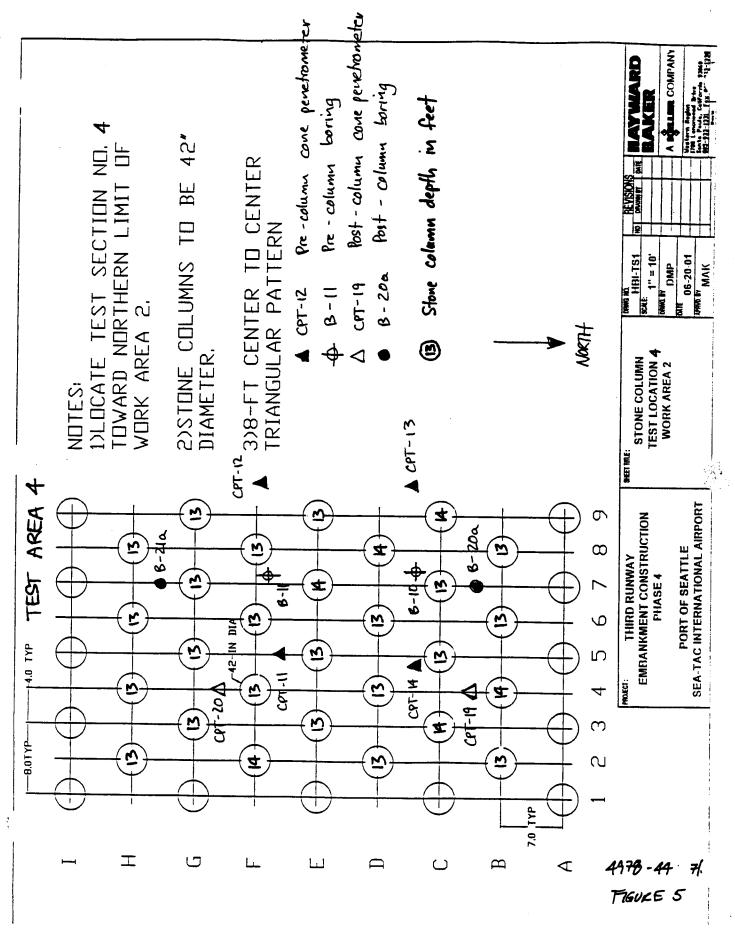
FIGURE 2



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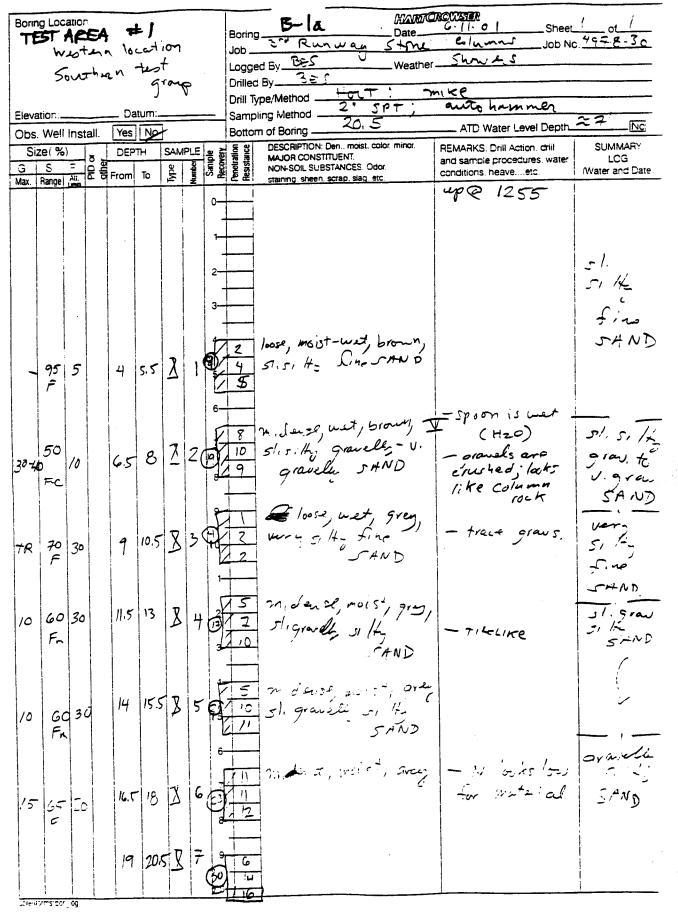
APPENDIX A TEST AREA 1

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AR 050719

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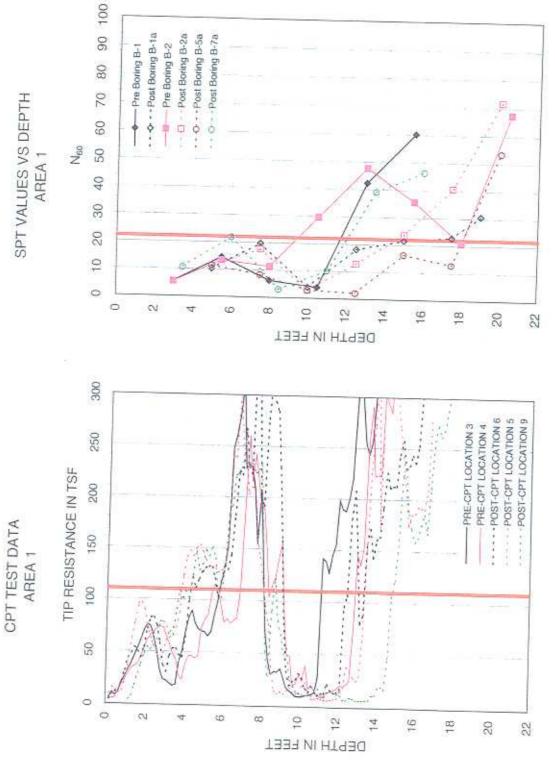
TEST AREA #1

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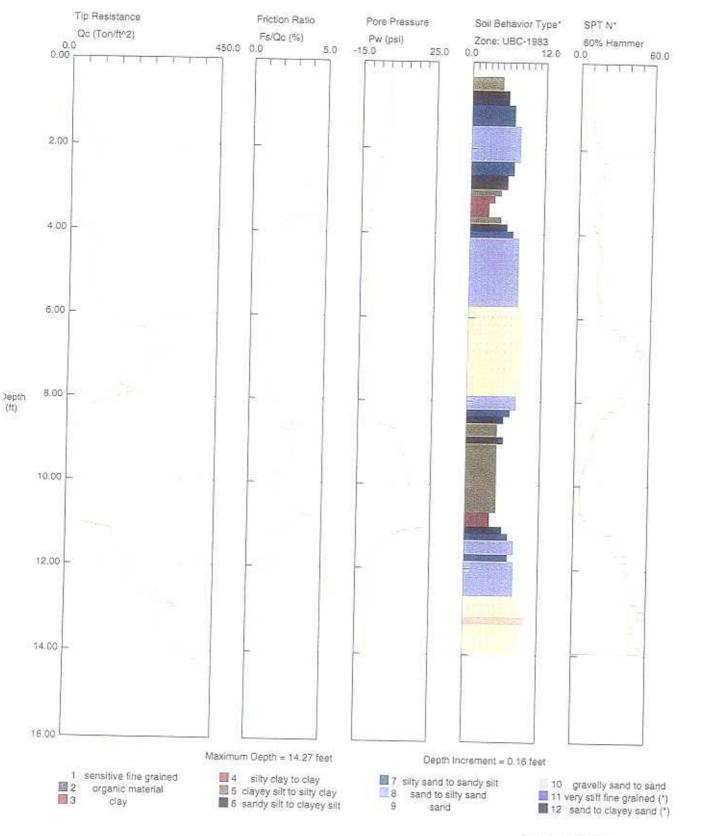


AR 050720

6/29/01

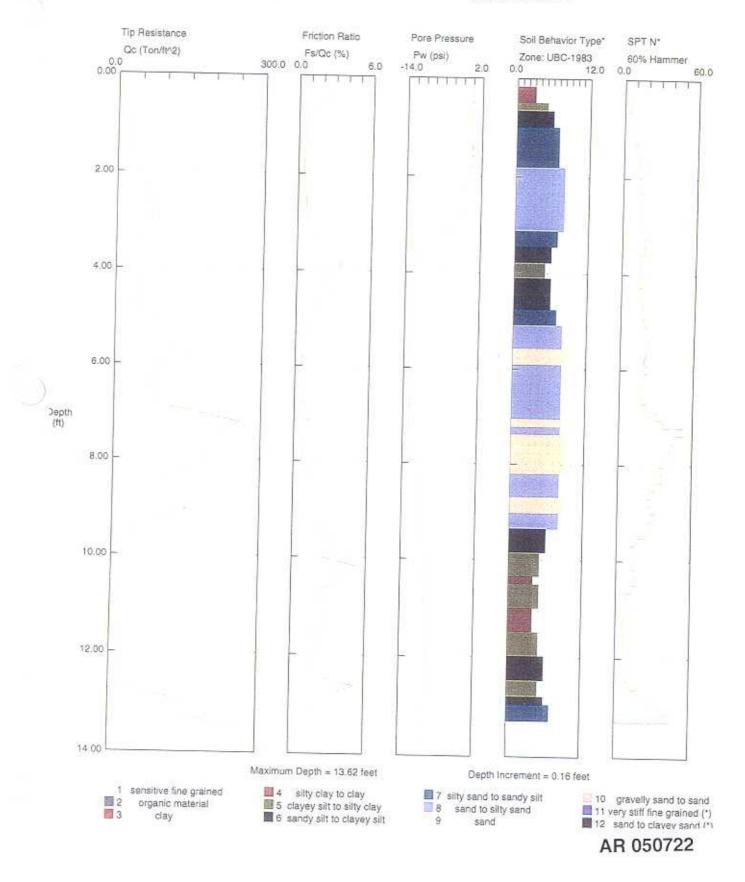
Operator: K.Brown Sounding: CPT-03 Cone Used: 581

CPT Date/Time: 06-01-81 09:21 Location: Third Runway Job Number: 4978-44



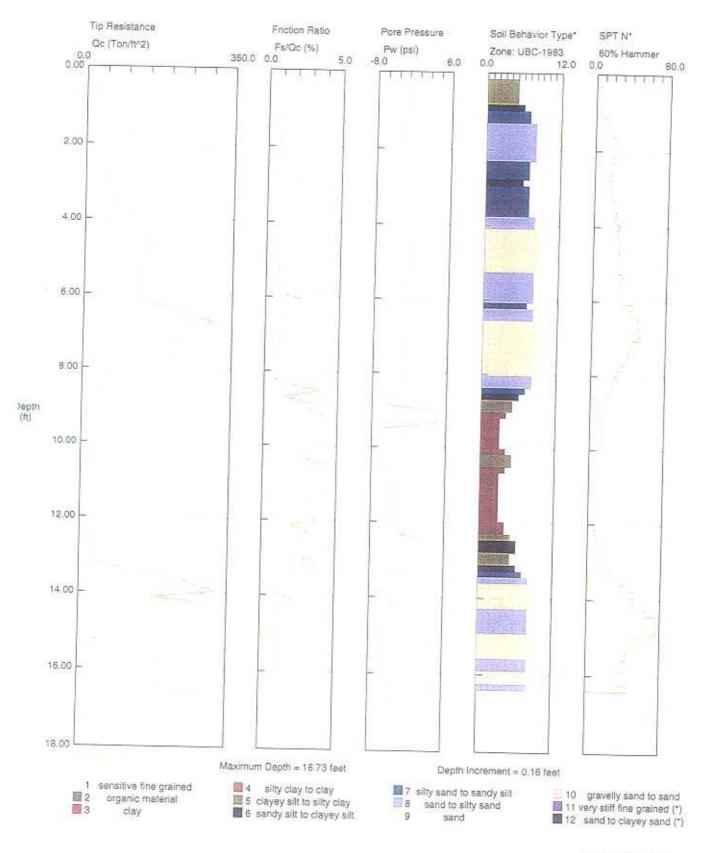
Operator: K.Brown Sounding: CPT-04 Cone Used: 581

CPT Date/Time: 06-01-81 09:42 Location: Third Runway Job Number: 4978-44



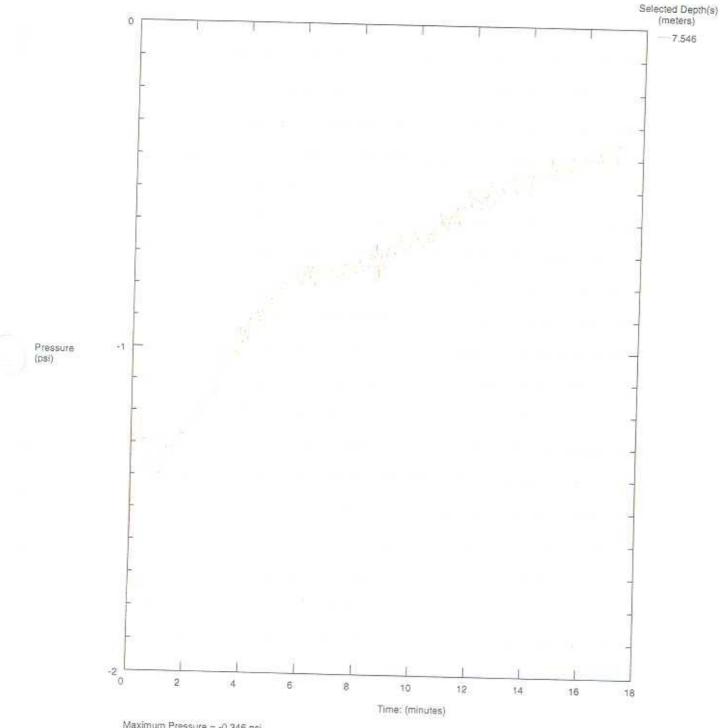
Operator: K.Brown Sounding: CPT-05 Cone Used: 581

CPT Date/Time: 06-12-81 11:35 Location: Third Runway Job Number: 4978-44



Operator K.Brown Sounding: CPT-05 Cone Used: 581

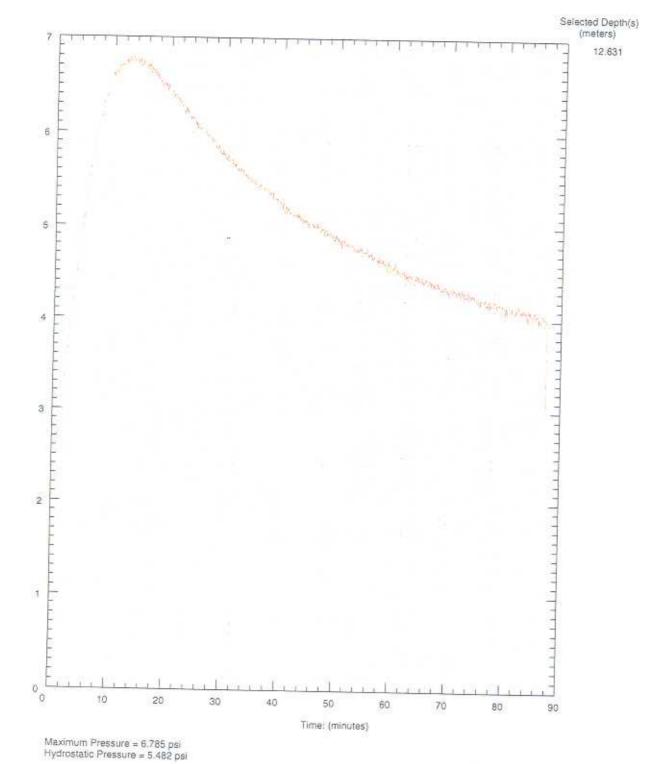
CPT Date/Time: 06-12-81 11:35 Location: Third Runway Job Number: 4978-44



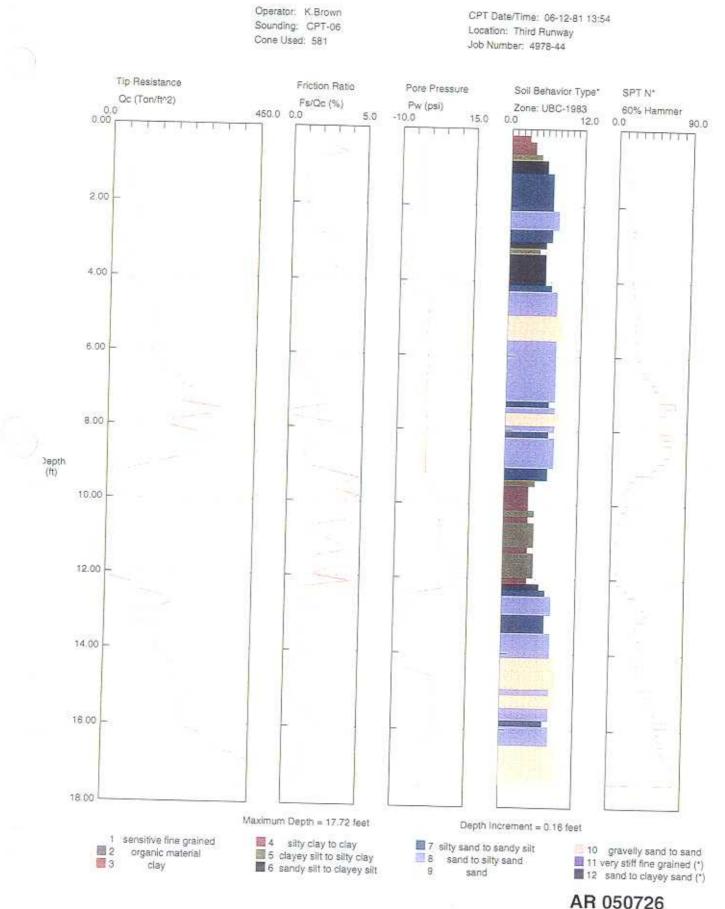
Maximum Pressure = -0.346 psi Hydrostatic Pressure = 3.275 psi

Operator K.Brown Sounding: CPT-05 Cone Used: 581

CPT Date/Time: 06-12-81 11:35 Location: Third Runway Job Number: 4978-44

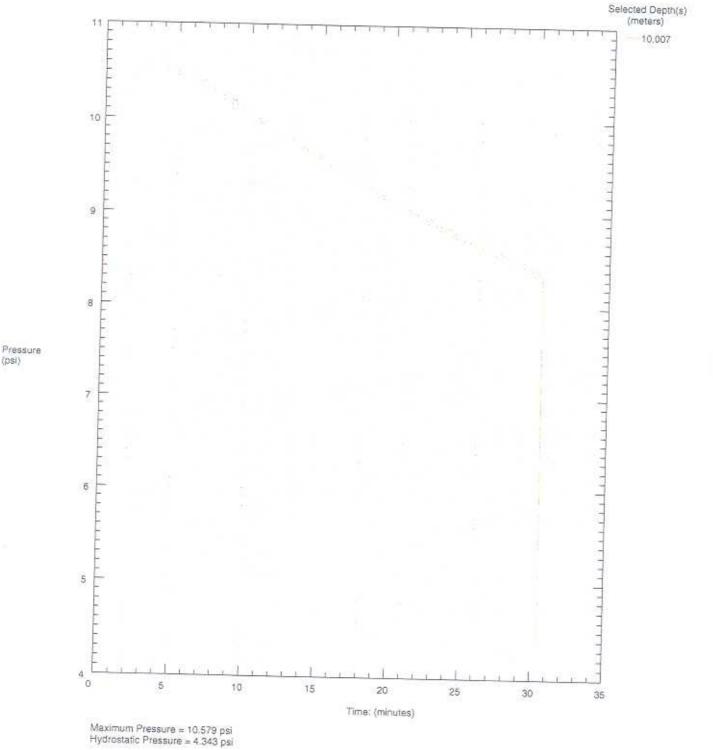




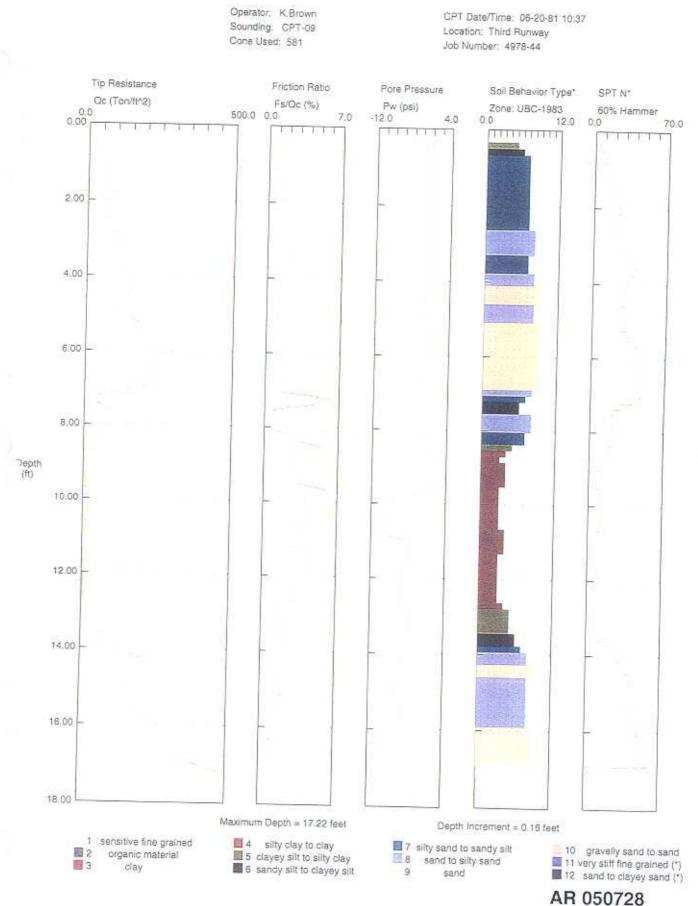


Operator K.Brown Sounding: CPT-06 Cone Used: 581

CPT Date/Time: 06-12-81 13:54 Location: Third Runway Job Number: 4978-44



(psi)

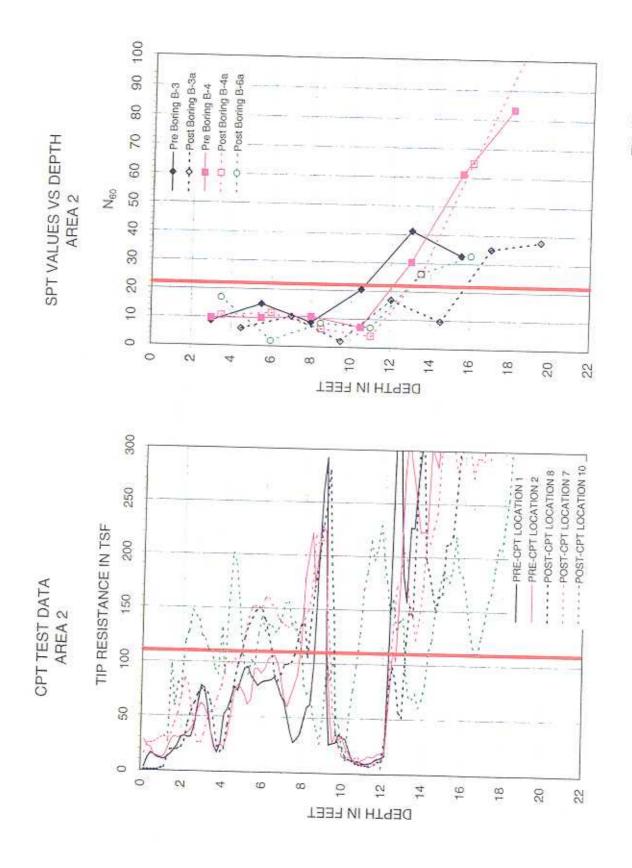


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APPENDIX B TEST AREA 2

Hart Crowser 4978-44 July 24, 2001

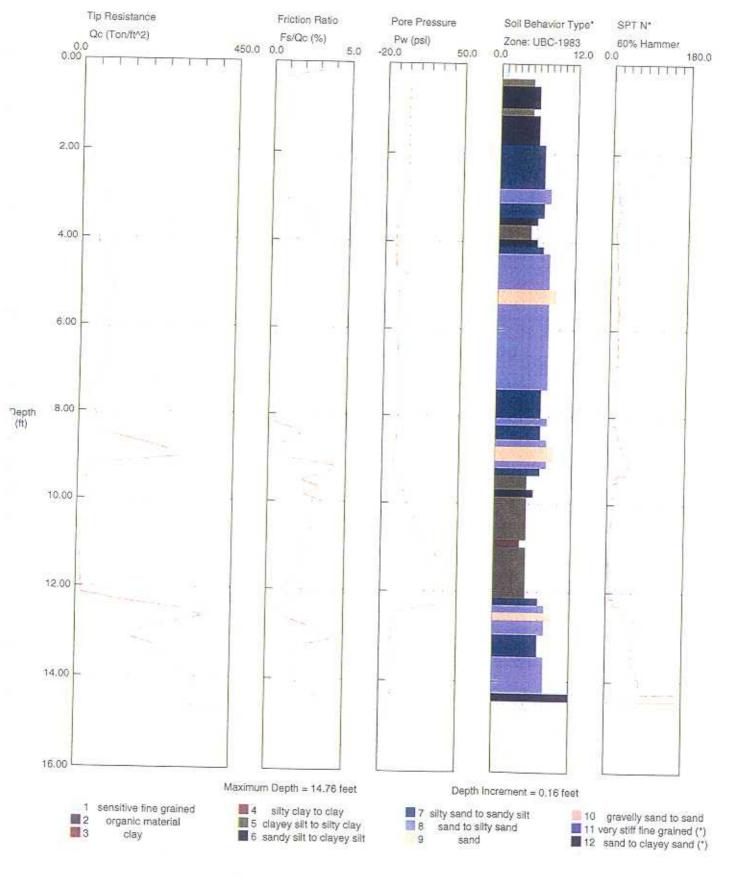
Third Runway - SeaTac Airport Stone Columns - In-Situ Soil Testing J-4978-30

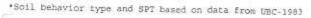


6/29/01

Operator: K.Brown Sounding: CPT-01 Cone Used: 581

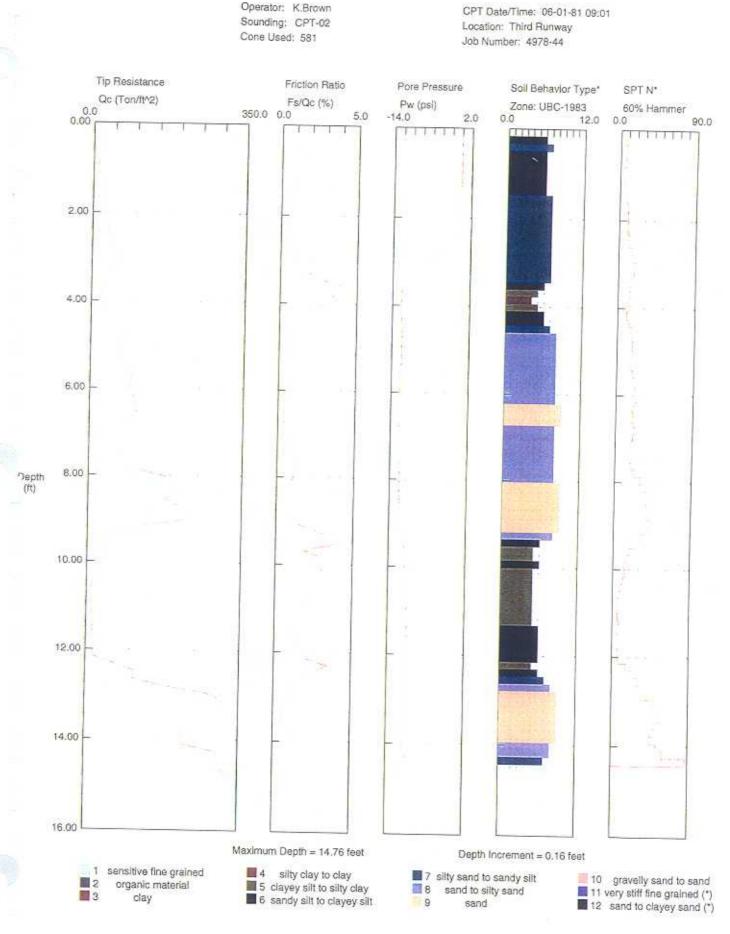
CPT Date/Time: 06-01-81 08:37 Location: Third Runway Job Number: 4978-44





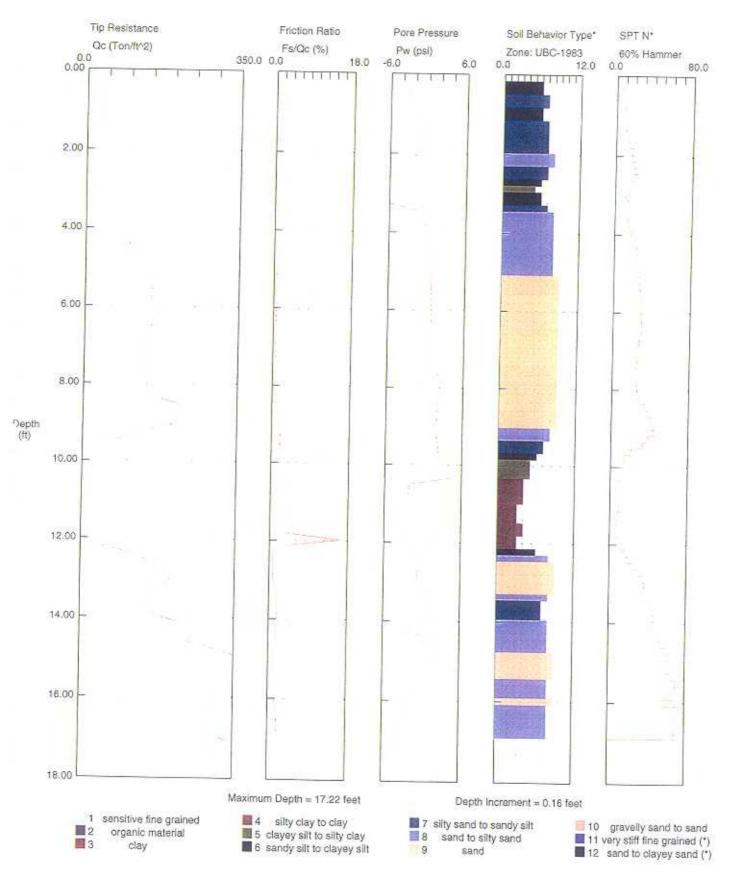


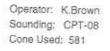




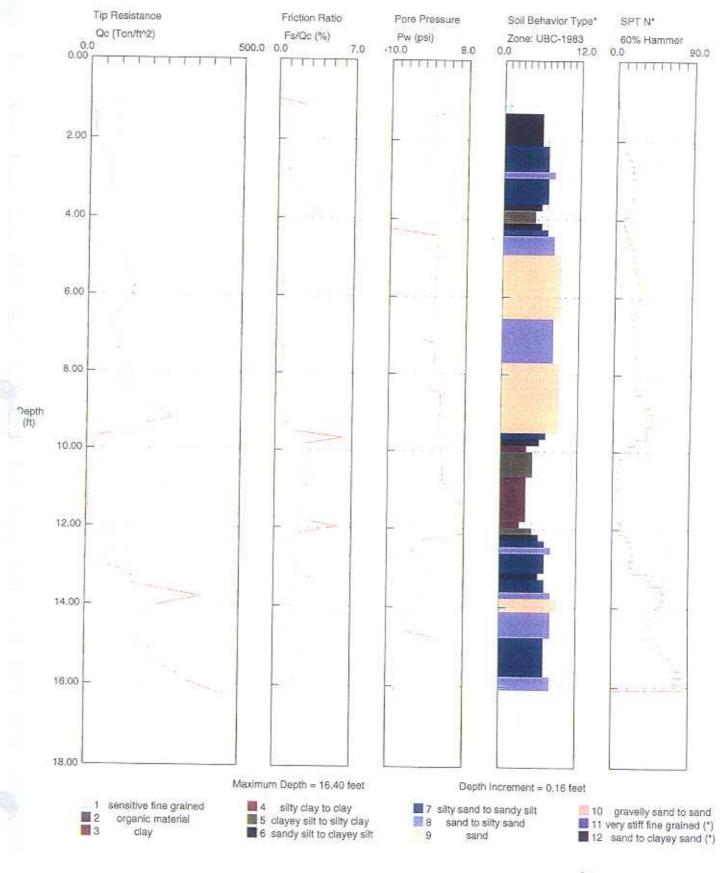
Operator: K.Brown Sounding: CPT-07 Cone Used: 581

CPT Date/Time: 06-12-81 14:46 Location: Third Runway Job Number: 4978-44



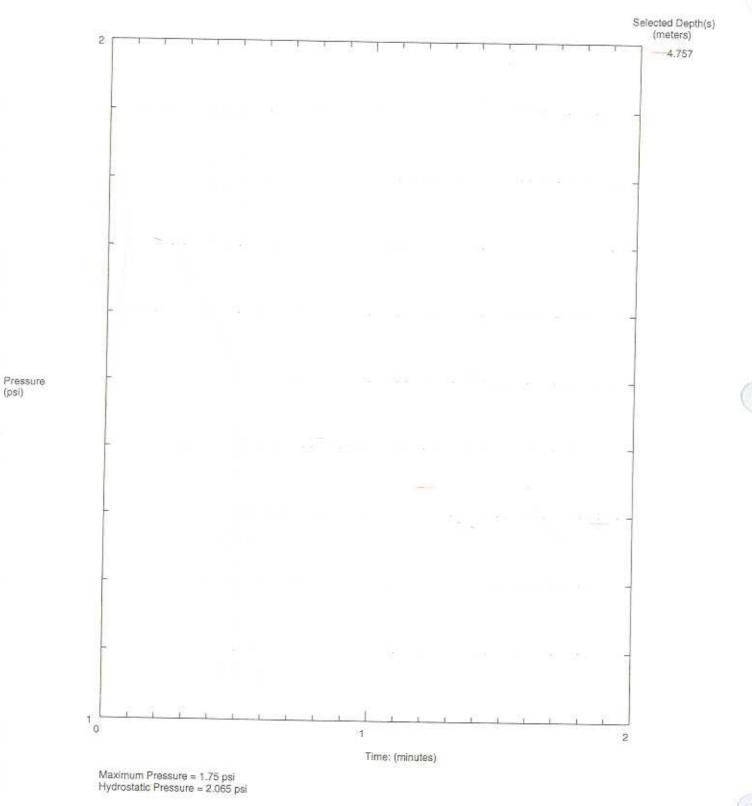


CPT Date/Time: 06-12-81 15:18 Location: Third Runway Job Number: 4978-44



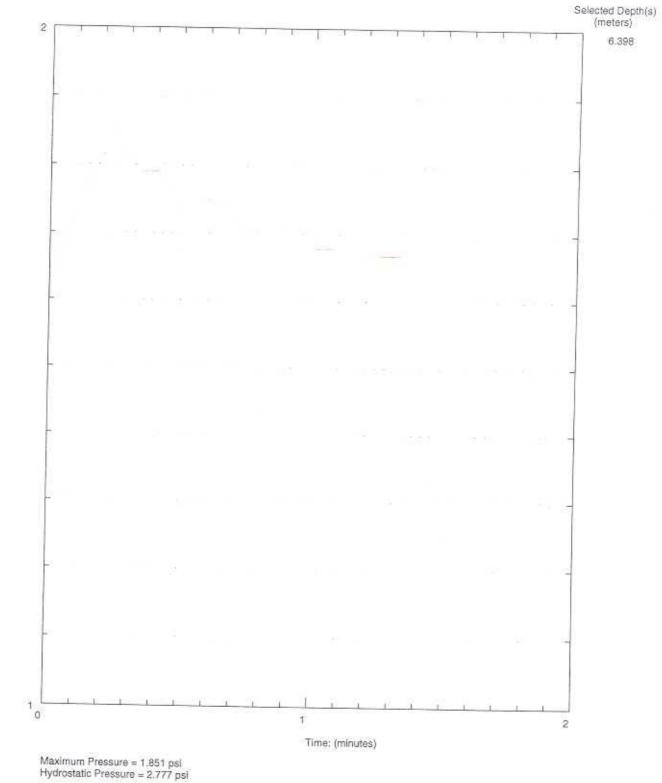
Operator K.Brown Sounding: CPT-08 Cone Used: 581

CPT Date/Time: 06-12-81 15:18 Location: Third Runway Job Number: 4978-44



Operator K.Brown Sounding: CPT-08 Cone Used: 581

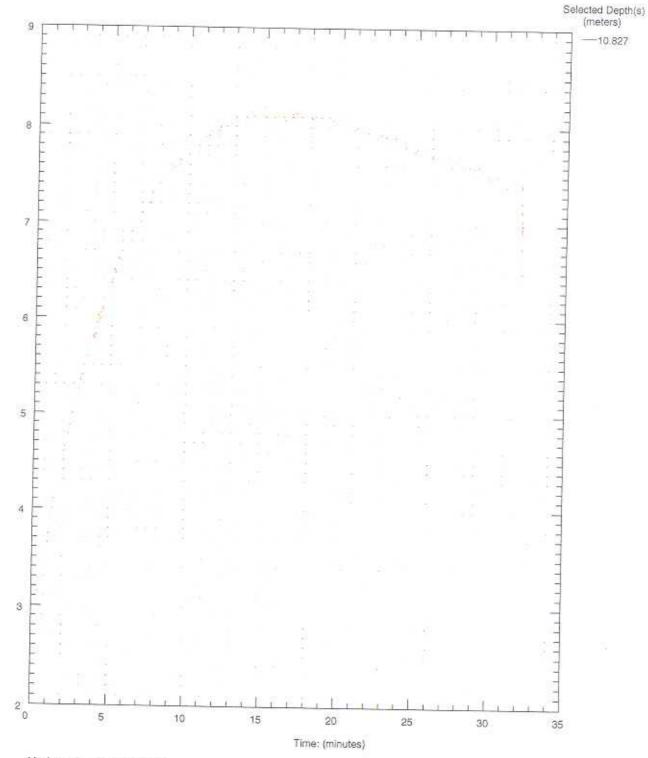
CPT Date/Time: 06-12-81 15:18 Location: Third Runway Job Number: 4978-44



Pressure (psi)

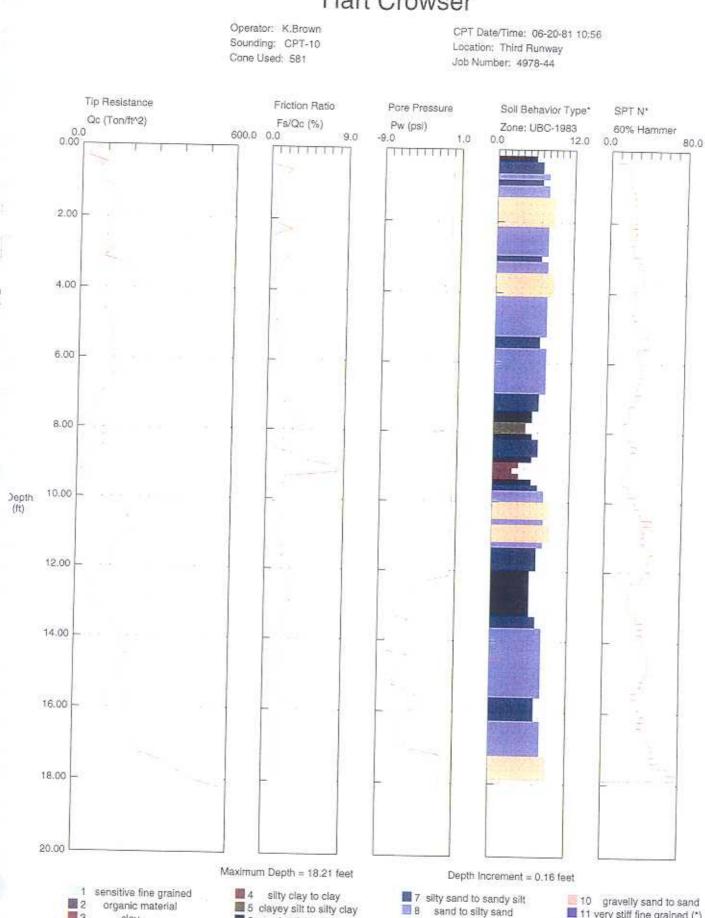
Operator K.Brown Sounding: CPT-08 Cone Used: 581

CPT Date/Time: 06-12-81 15:18 Location: Third Runway Job Number: 4978-44



Maximum Pressure = 8.148 psi Hydrostatic Pressure = 4.699 psi

Pressure (psi)



5 clayey silt to silty clay 6 sandy silt to clayey silt

9

sand

3

clay

AR 050739

11 very stiff fine grained (*)

12 sand to clayey sand (*)

TEST AREA #2 Date 61101 HARMAROWSER **Boring Location:** NSA Area Sheet Boring Job 3R 497 Job No ._ F'15 RAIN Logged By dP Weather -HOL Drilled By_ HSA Drill Type/Method_ SPT Datum: Elevation: Sampling Method ATD Water Level Depth 5.5 No Bottom of Boring _ Obs. Well Install. Yes No 5 0 DESCRIPTION; Den., moist., color, minor, MAJOR CONSTITUENT. a... NON-SOIL SUBSTANCES: Odor, stoining, sheen, scrap, slag, etc. Action, drill and sample procedures, water conditions, heave,...etc... SUMMARY SAMPLE RECOVERY SIZE (%) SAMPLE e o DEPTH drill and sample proced-LOG SF G ures, water conditions, Type Number O d o From (Water & Date) Max. Range Att. То 0 5 INCHES GRAY ORANGE OVER SANDY SILT LOOSE, BROWN, MOIST, S. SILTY M. SAND SI 8 3.5 2.0 95 5 N. NEUSE, NOGT TO WET, BEDUN SL. SZ SILTY 60 15 4.5 62 11 27 SAND GRAVELLY M. STIEF, WET, BRINN / GRAY 85 7.0 53 8 SL. GRAVELLY, SANDY CLANEY SUT 9 N. DENSE, WET, DARK SRAY, ID H Ю 95 11.0 SL SILTY, SL GENJELLY SAND (OUTWASH?) ١D 20 10 **.** • 12 11 DEUSE, MOIST, GRAY, SL 135 120 60 35 17 5 R GRAVELY USILTY SAND TOUSANDY SILT 25 (TILL) DEUSE. MOIST, GRAY GRANCELY, 14.5 16.0 156 15 10 55 35 (3) SILTY TO J. SILTY 'SAND (TICL) M. DENSE, MOIST, GRAT, 7.0 18.5 (19) 65 30 SL. GRAVELLY, SUT-1 F-M SAND 19 12/0

test area #2 Date GIOI Boring Location: USA Arca Z B3 2 STONE Boring___ Sheet. of F' 15 Job No. 447 Weather PAN Logged By ____ 600 Drilled By_ a HSA Drill Type/Method SPT Elevation: Datum: Sampling Method . No ATD Water Level Deptri Bottom of Boring. Obs. Well Install. Yes No Penetration Resistance SIZE (%) SAMPLE RELOVERY DESCRIPTION; Den., moist., color, minor, MAJOR CONSTITUENT. NON-SOIL SUBSTANCES: Odor, REMARKS; Drill action, SUMMARY SAMPLE بقو DEPTH drill and sample proced-LOG SF G Range Att. a. o From Type Number ures, water conditions, (Water & Date) heave,...etc... staining, sneen, scrap, slag, etc. То Max. V.DENSE, WEI, GRAY, 20 82 Z 21 SL SILTY, ASL GRAVEUS H.5 63 70 25 33 5 M -(TH C SAND 2 BOB @ 22 21.0 6/1/01 23 113 24 25 26 27 **7**8-29. 30. 1 2 3 4 5 6 7 8 9 0-

#2 TEST AREA HARTCROWSER **Boring Location:** 6/1/01 BH Date_ . Sheet _ Boring 4476 JOD SE NSA AREA 2 STONE COL JOD NO. NSA AREA N' 13 CLOUDY JPL Weather _ Logged By_ #2 Drilled By_ HOL HS/ Drill Type/Method. SPT Elevation: Datum: Sampling Method. No ATD Water Level Depth . Obs. Well Install. Yes Bottom of Boring. DESCRIPTION: Den., moist., color, minor, MAJOR CONSTITUENT. WON-SOIL SUBSTANCES: Odor, staining, sheen, scrap, slag, etc. ReMARKS; Drill action, drill and sample proces ures, water conditions. heave,...etc... SUMMARY SAMPLE RECOVERY SIZE (%) SAMPLE DEPTH ور او م drill and sample proced-LOG GISIF ures, water conditions, Max. Range Att. a o From Type Number (Water & Date) Тο 0 1 GRAY, DEAUGE 5 INCLES OJER VELY CANDY SILT 2 LOOSE, WET, BROWN A SILTY 66 33 4 2.0 3.5 2 9 SAND 85 18 ٦ 5 LOUSE TO M. DENSE, JUET, 52 5 45 6.0 SL. SILTY TO SIL BROWN - GRAY , 90 D 10 WITH INTERBEDDED E-M SAND GRAY/IRANGE SANDY SILT LEASE 6 LOSE TO M. DEUSE, WET, BROWN, SL SHITY SANT 8.5 7.0 SSA 5 [0] 5 53Ğ STIFF, WET, BROWN TO GRAY SANDY 9 SILT GRAVEL LOOSE, WET, GRAY U. SILTY 95 Q. h Z 9 55 45 CONTACT 7 5 SAND 2י ૪ GRAY, SL. DENSE WET. 12.0 13.5 55 1Z 5 75 D (33 GRAVELLY, SL. SILTY, SAND 19 to silty 14 16 DENE, WET, GRAY, (6.0 145 19 58 SAND (TIL) 39 Genery, SILM **ZY**6 V. DENCE, DAMP TO MOIST, 17.0 18.5 GOANELY, SILTY SANDI (THL) SZ GRAY. 1229 18.5 303 C 6/1/01 19 z ₀ź

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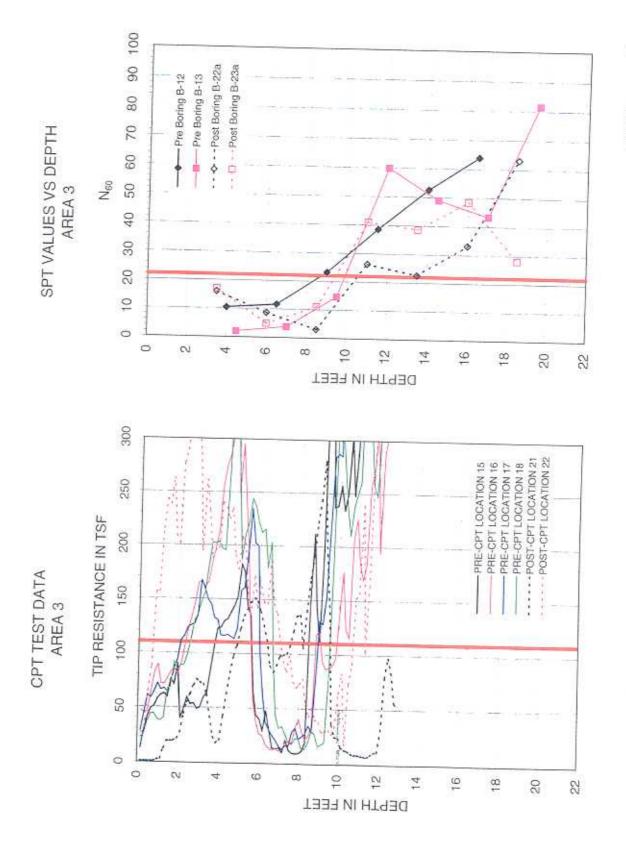
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APPENDIX C TEST AREA 3

Hart Crowser 4978-44 July 24, 2001

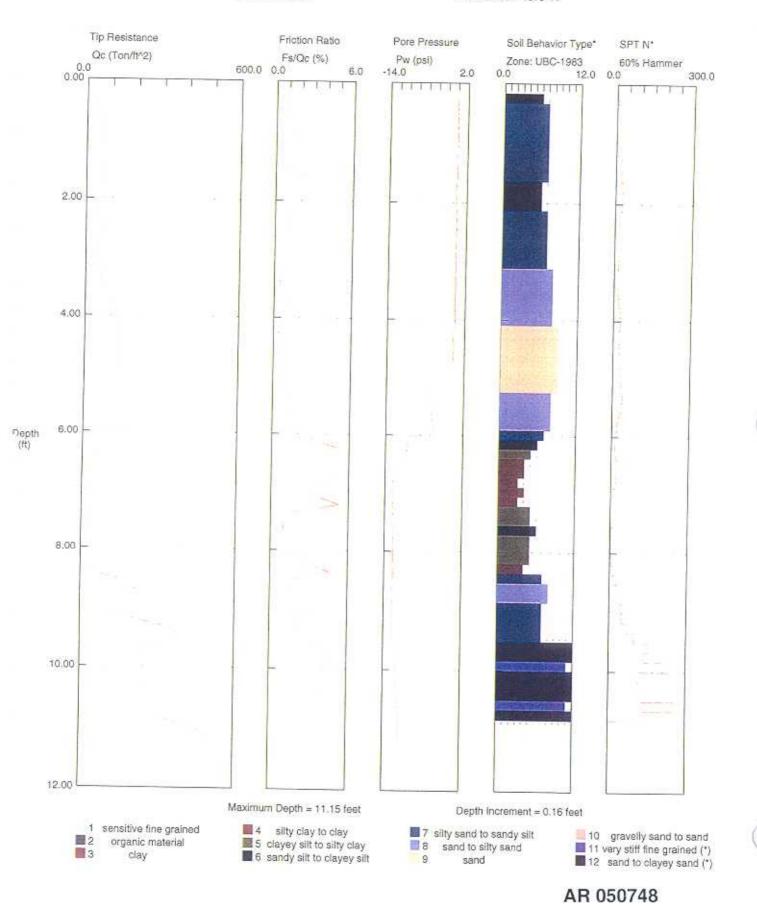
Third Runway - SeaTac Airport Stone Columns - In-Situ Soil Testing J-4978-30



6/29/01

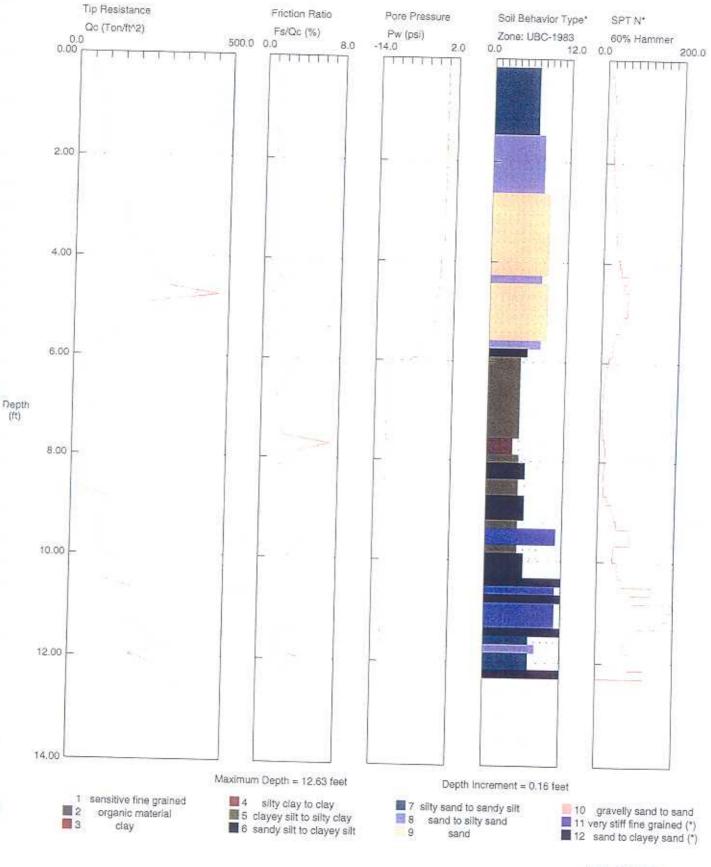
Operator: K.Brown Sounding: CPT-15 Cone Used: 581

CPT Date/Time: 06-20-81 12:31 Location: Third Runway Job Number: 4978-44



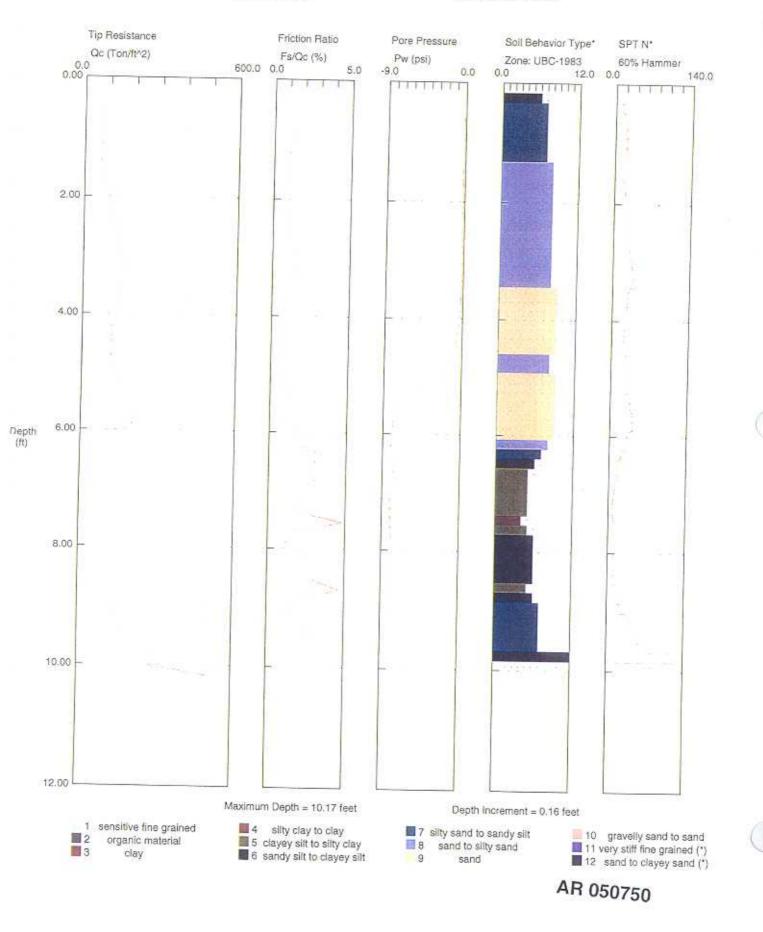
Operator: K.Brown Sounding: CPT-16 Cone Used: 581

CPT Date/Time: 05-20-81 12:44 Location: Third Runway Job Number: 4978-44



Operator: K.Brown Sounding: CPT-17 Cone Used: 581

CPT Date/Time: 06-20-81 12:57 Location: Third Runway Job Number: 4978-44

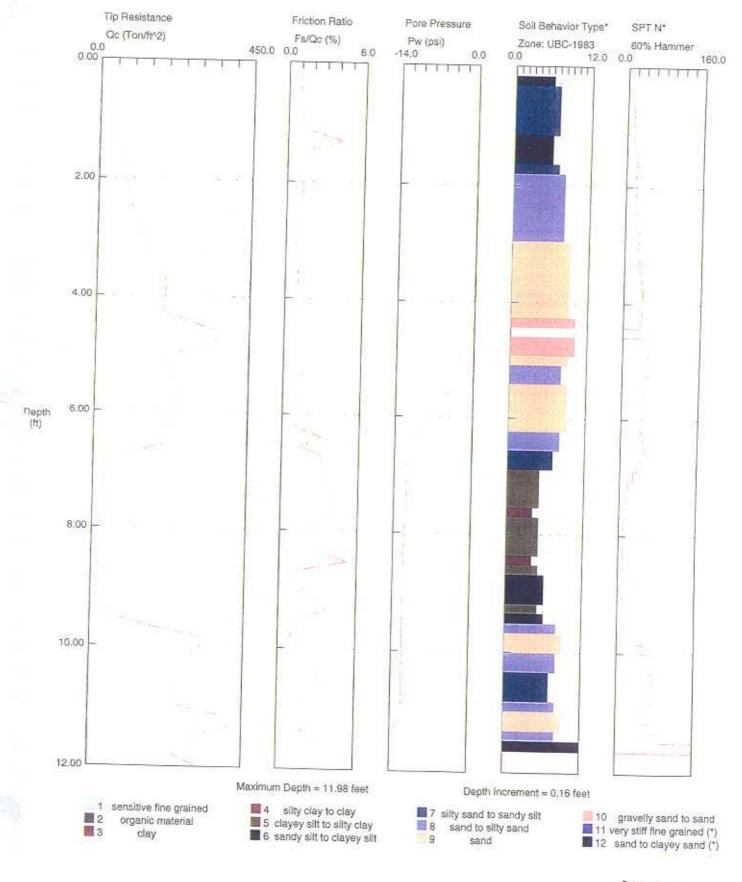


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Hart Crowser

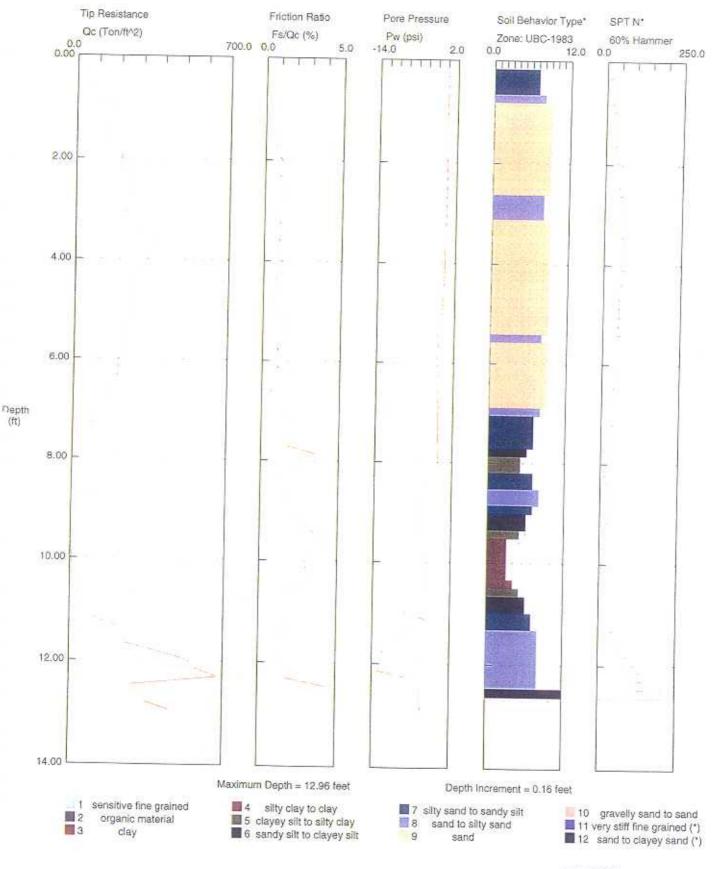
Operator: K.Brown Sounding: CPT-18 Cone Used: 581

CPT Date/Time: 06-20-81 13:09 Location: Third Runway Job Number: 4978-44



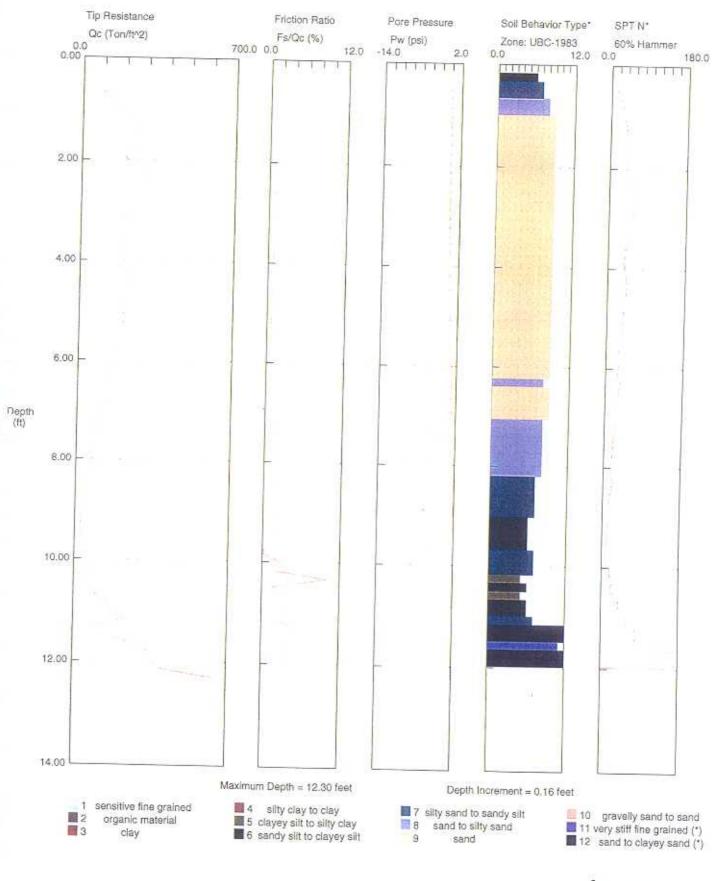
Operator: K.Brown Sounding: CPT-21 Cone Used: 581

CPT Date/Time: 06-27-81 11:09 Location: Third Runway Job Number: 4978-44

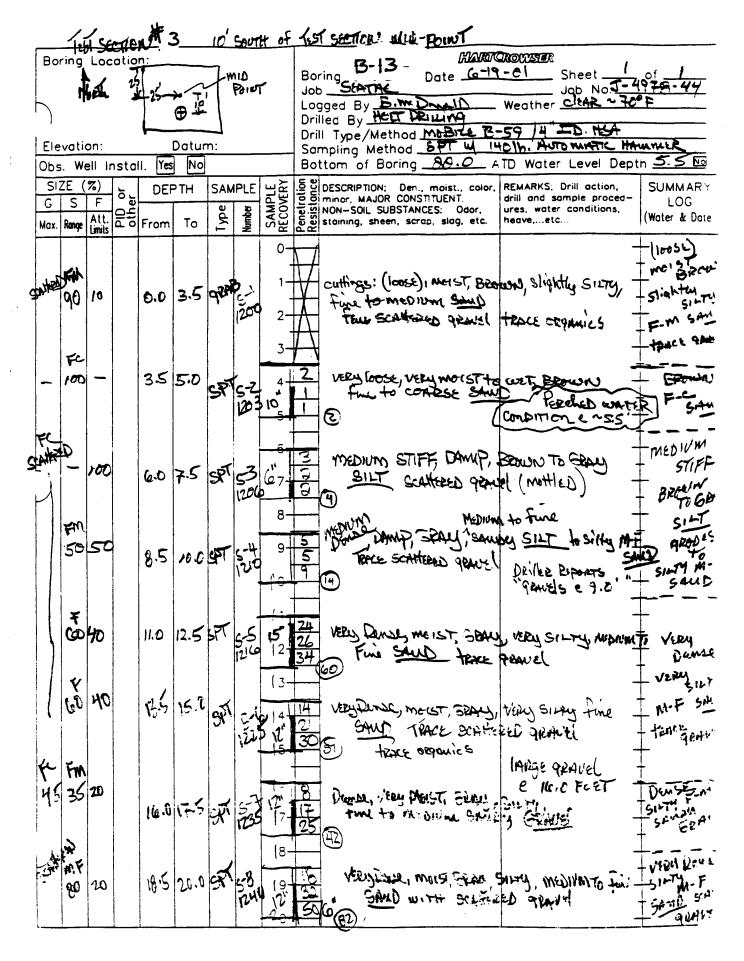


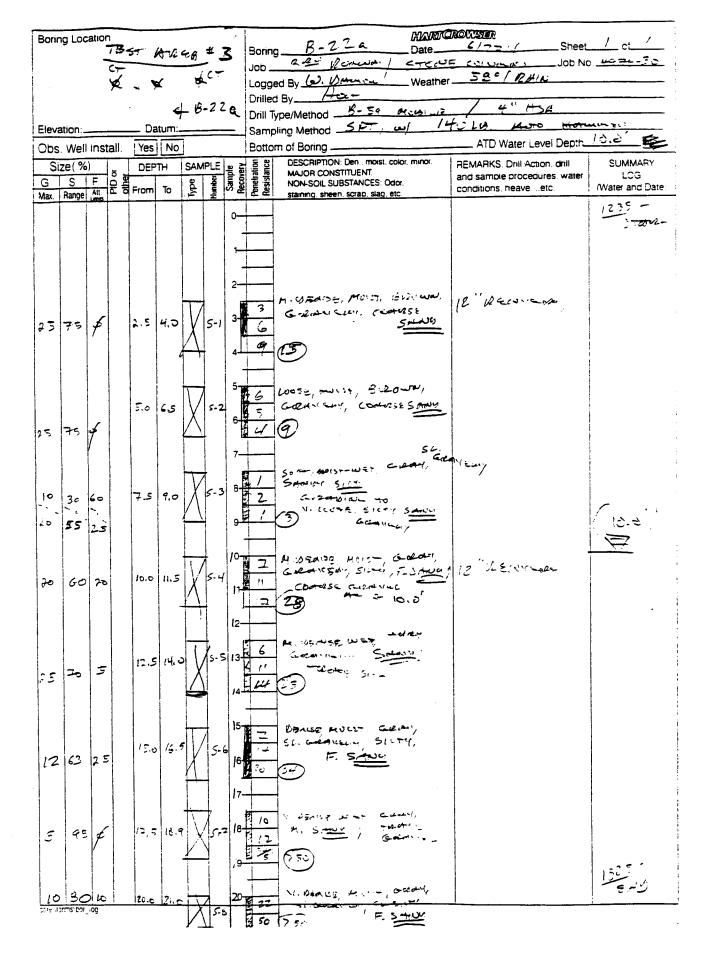
Operator: K.Brown Sounding: CPT-22 Cone Used: 581

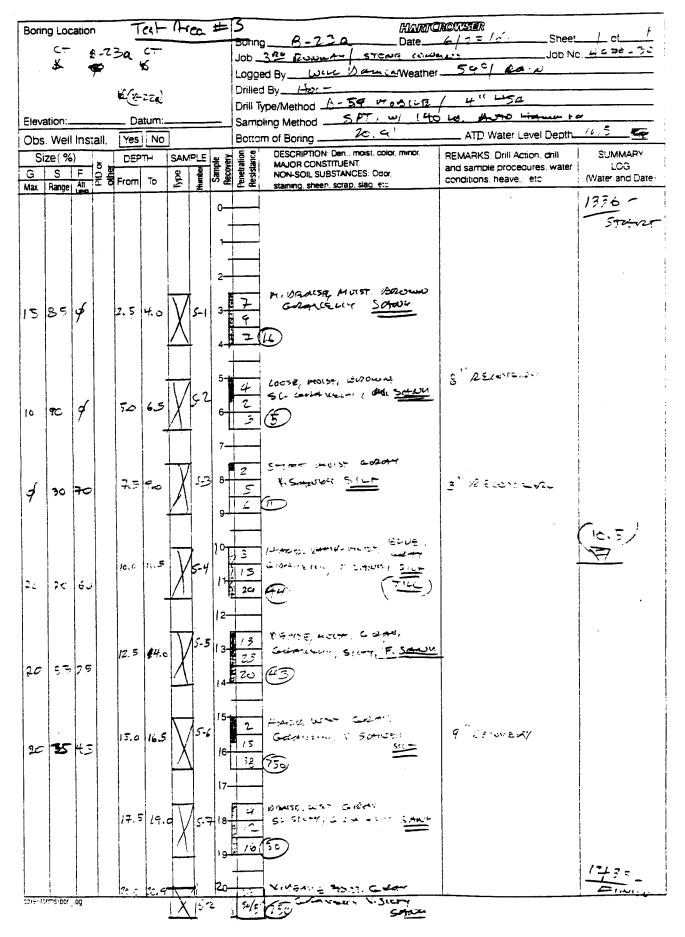
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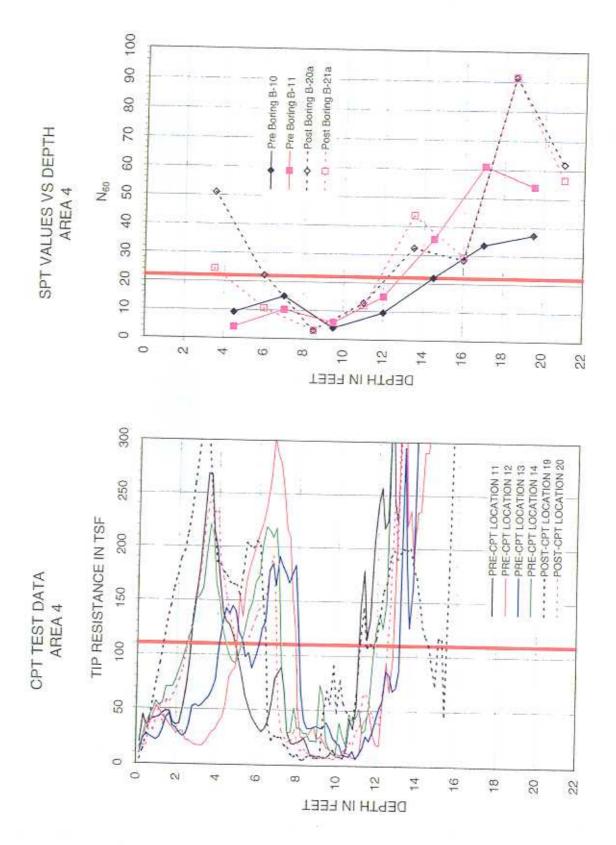




APPENDIX D TEST AREA 4

Hart Crowser 4978-44 July 24, 2001

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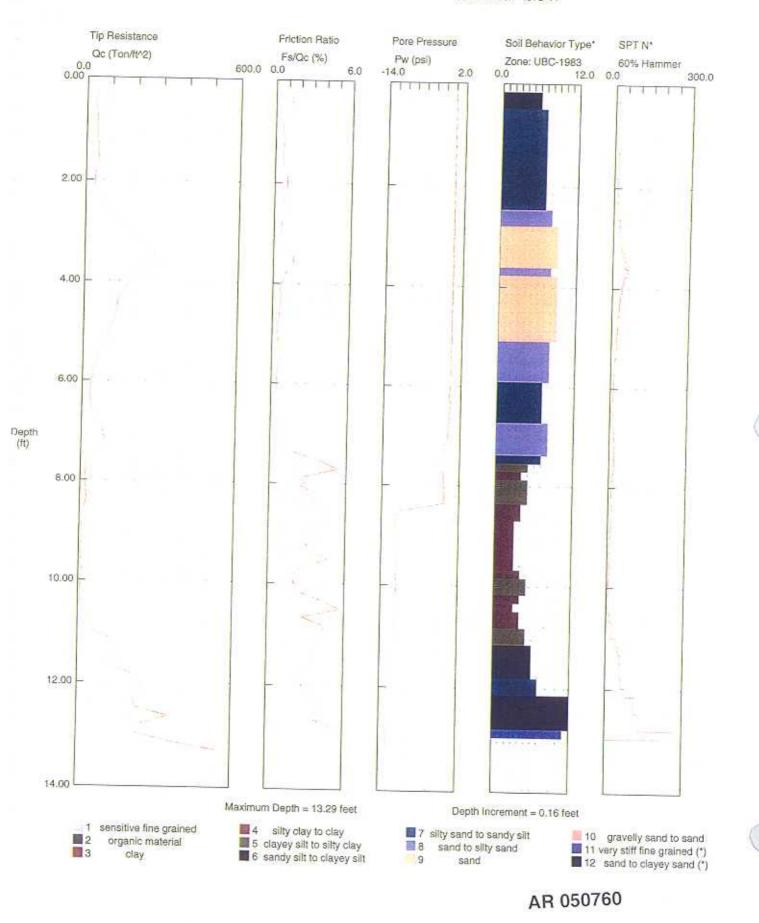


Third Runway - SeaTac Airport Stone Columns - In-Situ Soil Testing J-4978-30



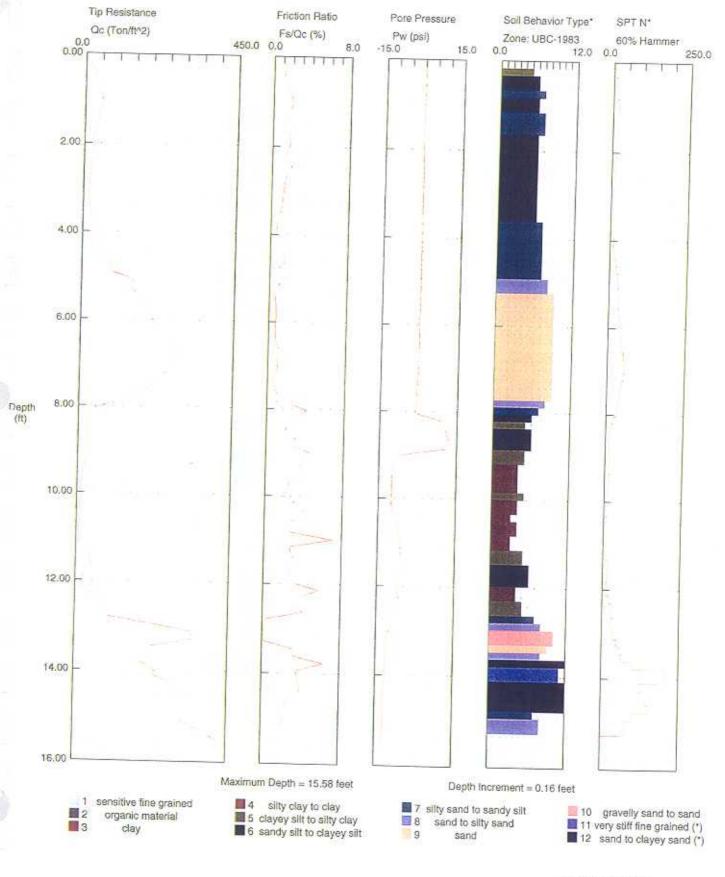
Operator: K.Brown Sounding: CPT-11 Cone Used: 581

CPT Date/Time: 06-20-81 11:15 Location: Third Runway Job Number: 4978-44



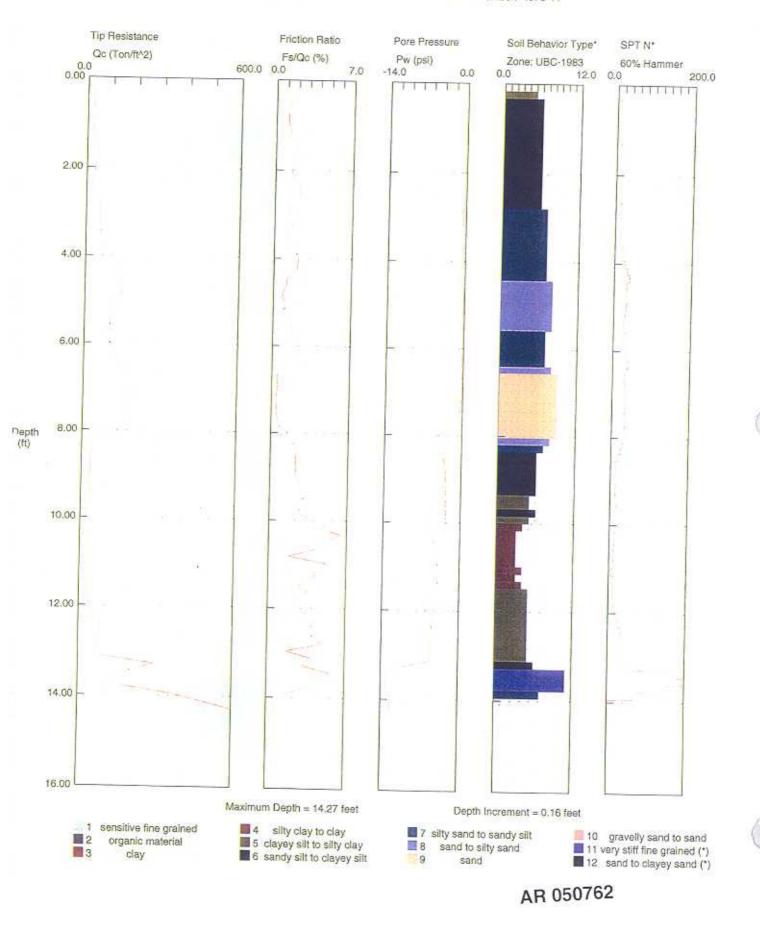


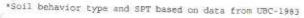
CPT Date/Time: 06-20-81 11:39 Location: Third Runway Job Number: 4978-44



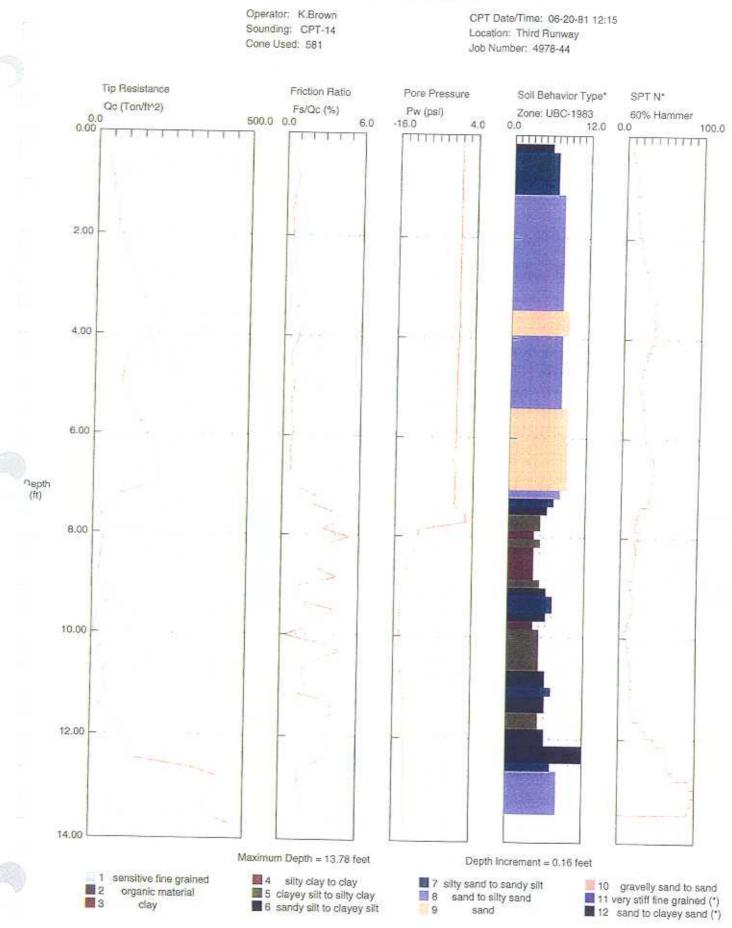
Operator: K.Brown Sounding: CPT-13 Cone Used: 581

CPT Date/Time: 06-20-81 11:54 Location: Third Runway Job Number: 4978-44





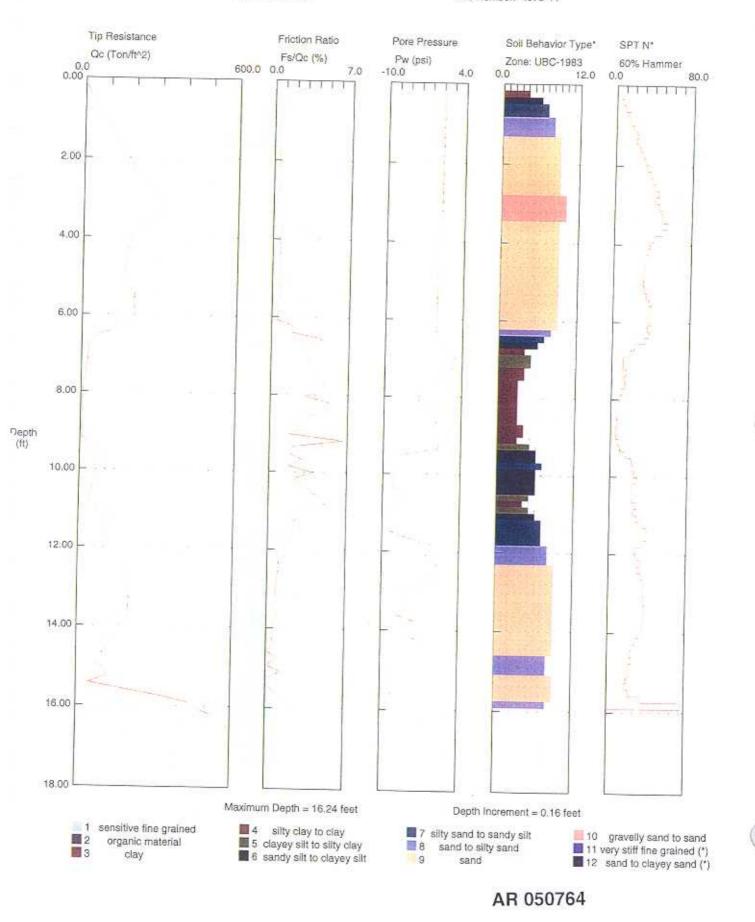
Hart Crowser



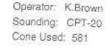
Hart Crowser

Operator: K.Brown Sounding: CPT-19 Cone Used: 581

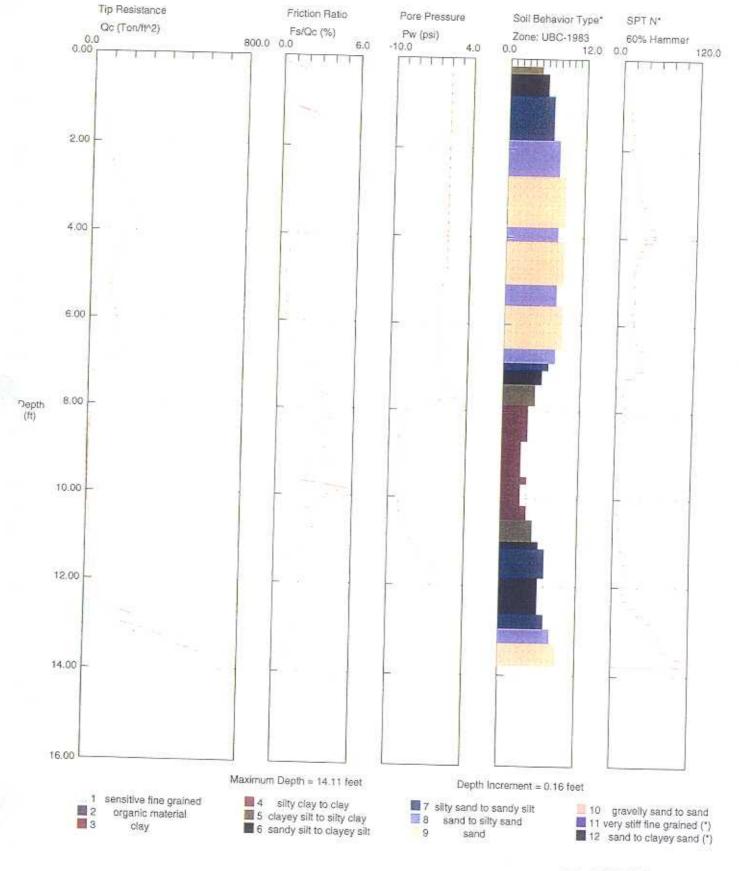
CPT Date/Time: 06-27-81 10:25 Location: Third Runway Job Number: 4978-44



Hart Crowser



CPT Date/Time: 06-27-81 10:46 Location: Third Runway Job Number: 4978-44



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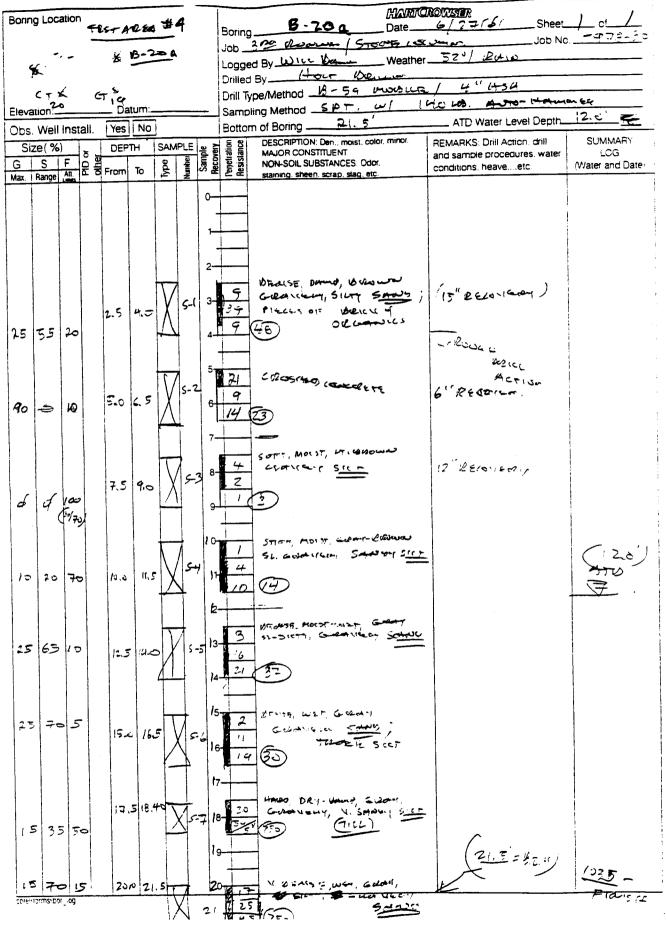
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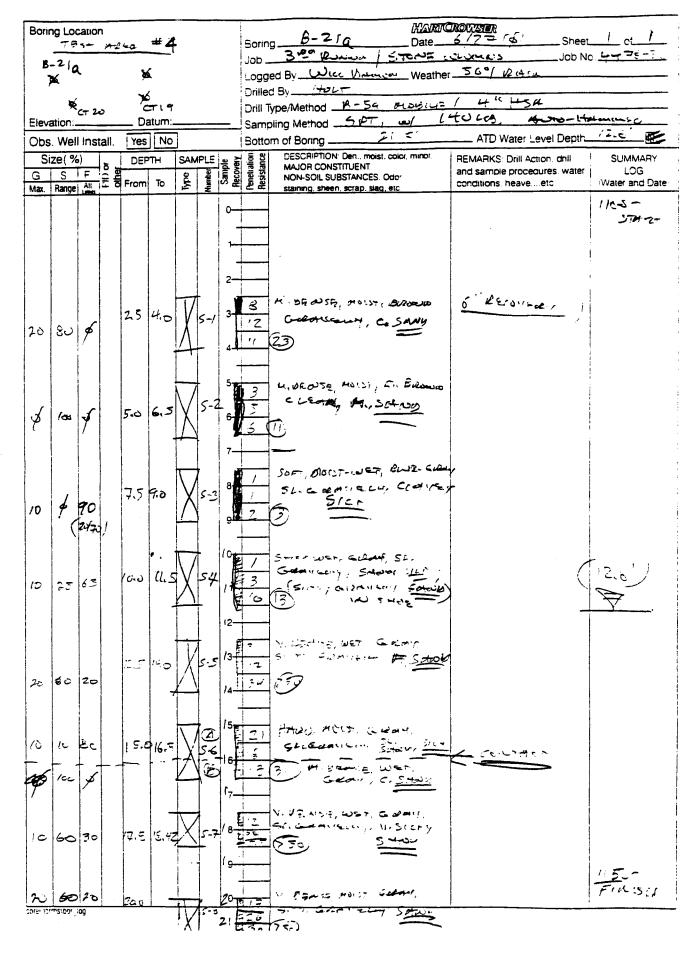
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APPENDIX E LABORATORY TESTING PROGRAM

Hart Crowser 4978-44 July 24, 2001

APPENDIX E LABORATORY TESTING PROGRAM

A laboratory testing program was performed for this study to evaluate the basic index and geotechnical engineering properties of the site soils. Disturbed samples were tested. The tests performed and the procedures followed are outlined below.

Soil Classification

Field Observation and Laboratory Analysis. Soil samples from the explorations were visually classified in the field and then taken to our laboratory where the classifications were verified in a relatively controlled laboratory environment. Field and laboratory observations include density/consistency, moisture condition, and grain size and plasticity estimates.

The classifications of selected samples were checked by laboratory grain size analyses. Classifications were made in general accordance with the Unified Soil Classification (USC) System, ASTM D 2487.

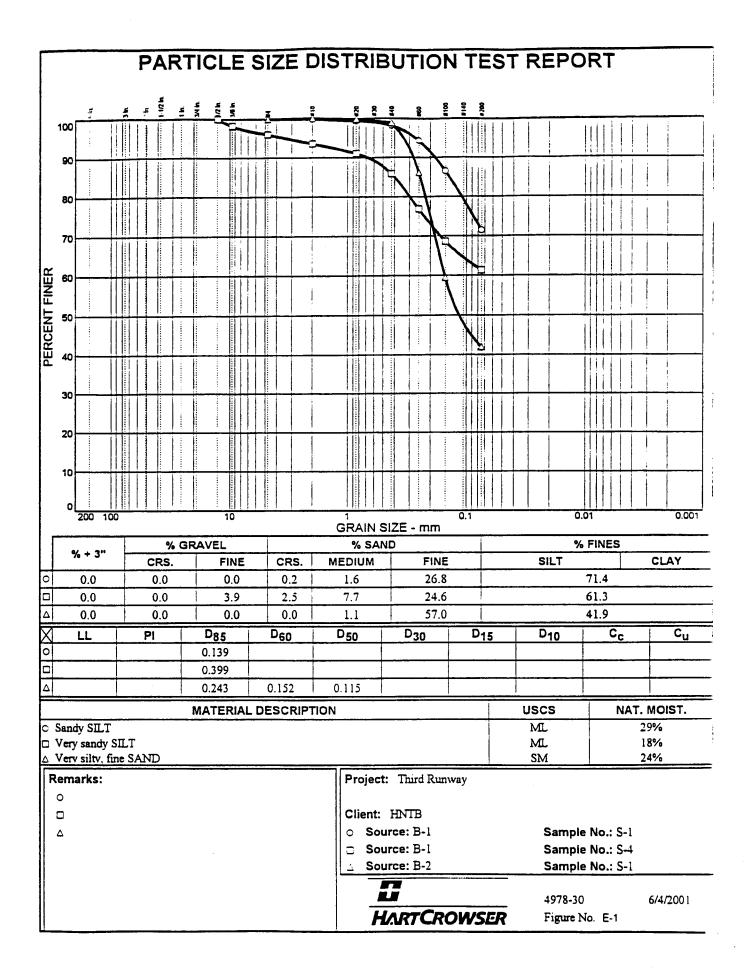
Water Content Determinations

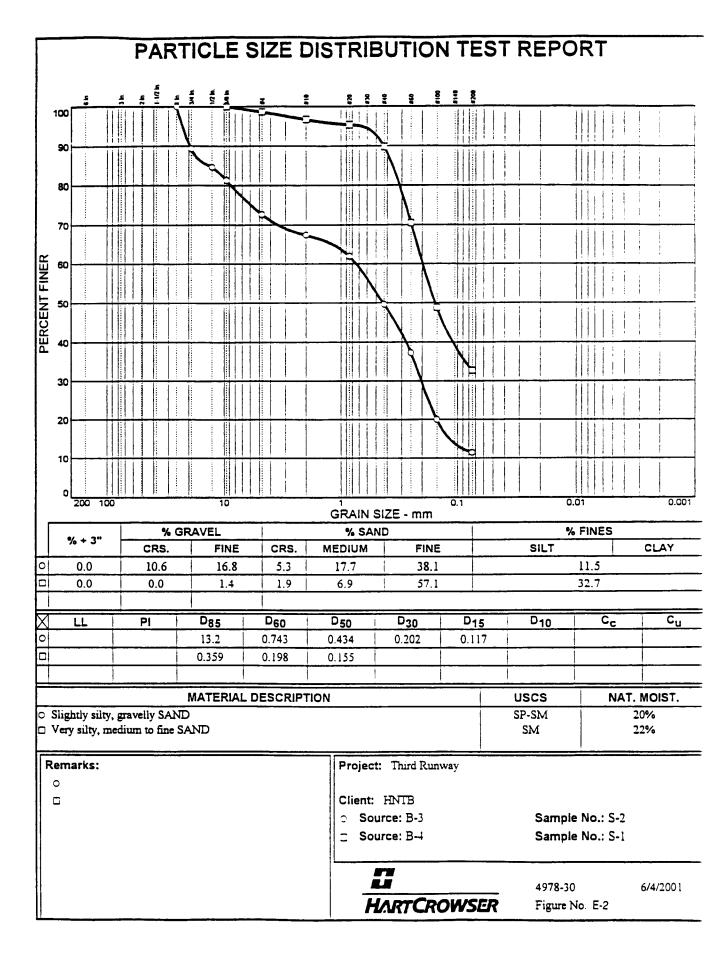
Water contents were determined for specific samples recovered in the explorations in general accordance with ASTM D 2216, as soon as possible following their arrival in our laboratory. Water contents were not determined for samples that were not subject to grain size analyses. The results of these tests are provided with the grain size results.

Grain Size Analysis (GS)

Grain size distribution was analyzed on representative samples in general accordance with ASTM D 422. Wet sieve analysis was used to determine the size distribution greater than the U.S. No. 200 mesh sieve. The size distribution for particles smaller than the No. 200 mesh sieve was determined by the hydrometer method for a selected number of samples. The results of the tests are presented as curves on Figures E-1 and E-2 plotting percent finer by weight versus grain size.

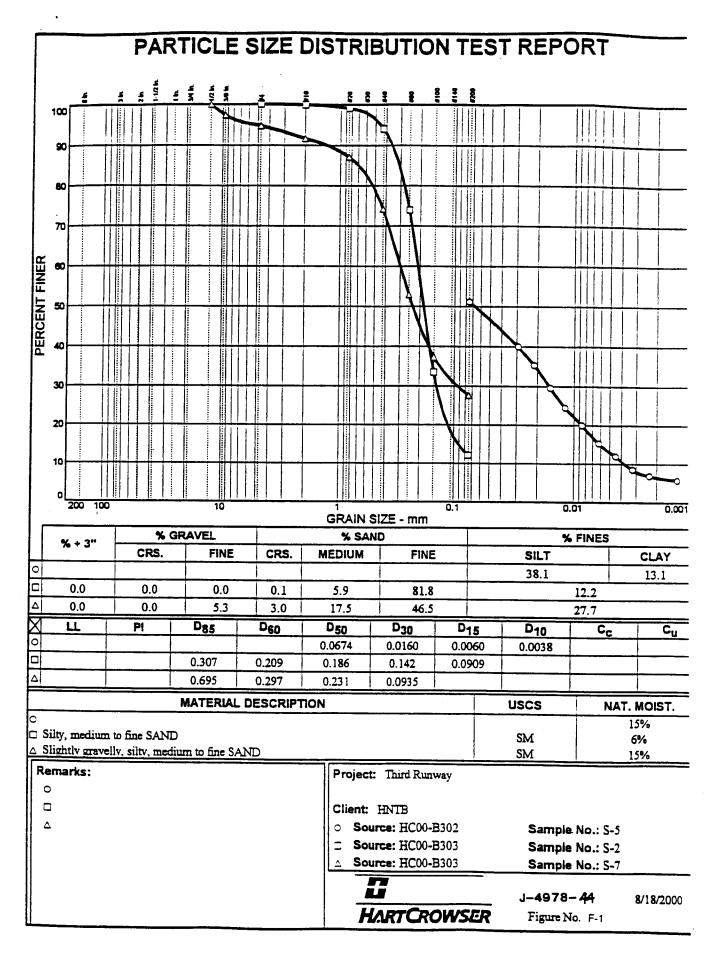
Hart Crowser 4978-44 July 24, 2001 Page E-1

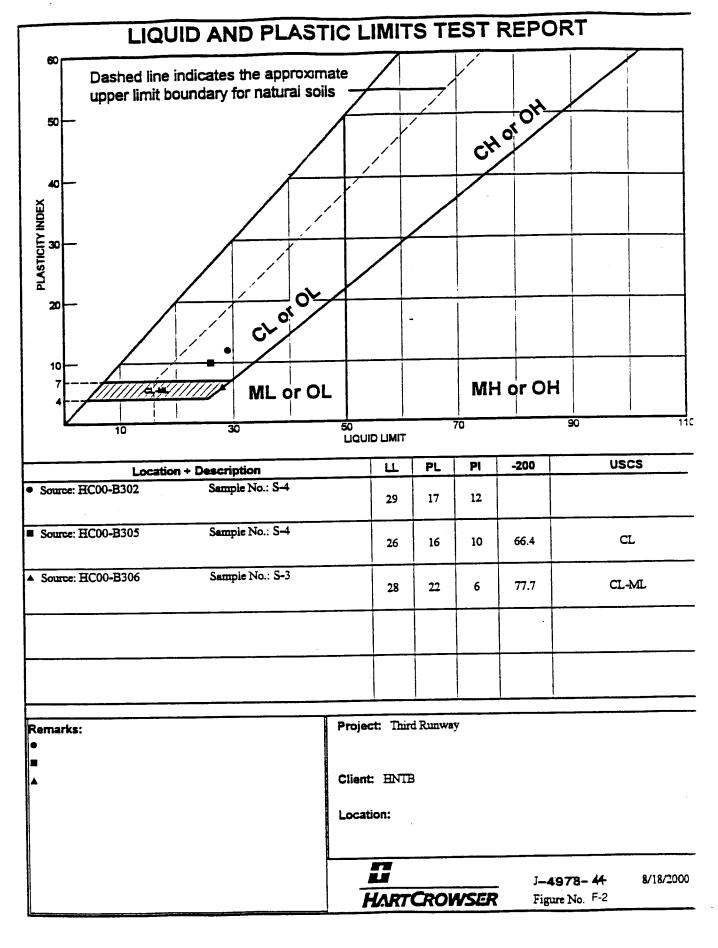




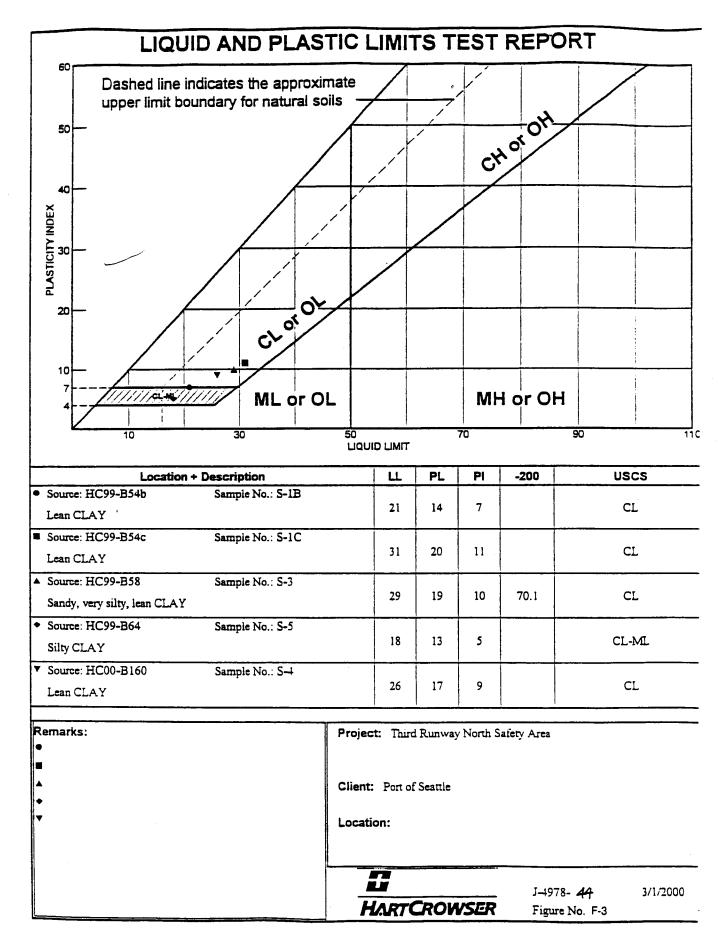
APPENDIX F PREVIOUS LABORATORY ANALYSES IN WORK AREA 2

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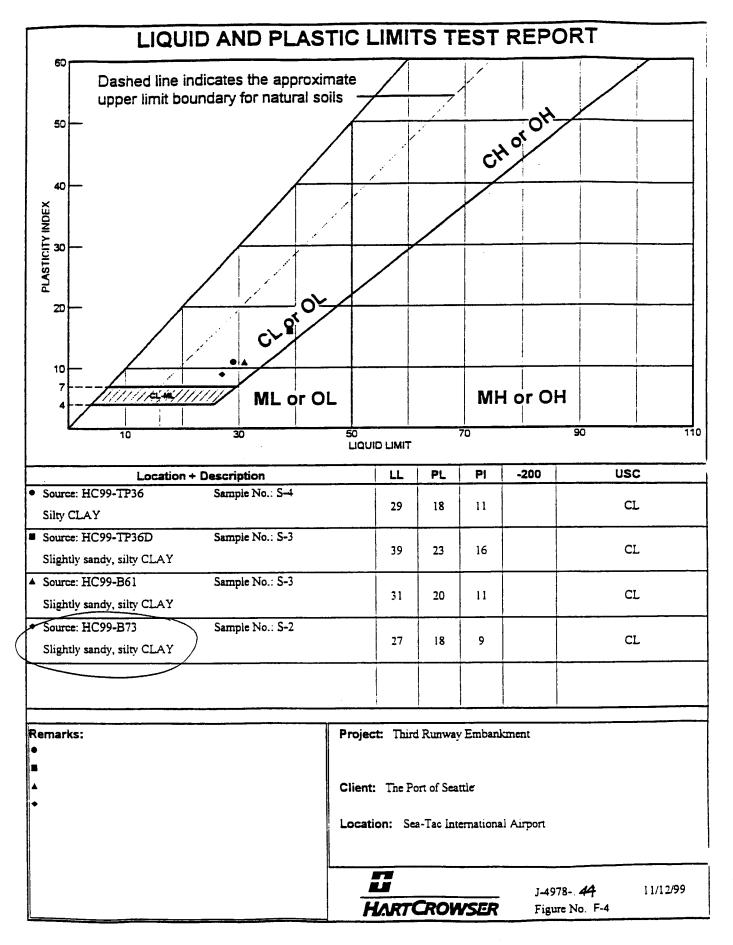




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