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Subsurface Conditions Data Report West MSE Wall Third Runway Embankment Sea-Tac International Airport



Prepared for Port of Seattle and HNTB

June 2000 J-4978-21

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SUBSURFACE CONDITIONS DATA REPORT WEST MSE WALL THIRD RUNWAY EMBANKMENT SEA-TAC INTERNATIONAL AIRPORT

INTRODUCTION

This data report presents information on subsurface conditions, based on geotechnical and hydrogeologic field and laboratory testing to support design of the West MSE Wall and adjacent embankment for the Third Runway Project at the Sea-Tac International Airport.

The site is located at the Sea-Tac International Airport, in SeaTac, Washington (refer to Figure 1, Vicinity Map). The shaded area on Figure 1 is presented on Figure 2, Site and Exploration Plan, showing exploration locations both for this report and those performed previously by Hart Crowser and others. A profile along the proposed mechanically stabilized earth (MSE) wall alignment showing subsurface conditions beneath the proposed wall is presented on Figure 3. Cross sections through the MSE wall showing inferred geologic conditions are provided on Figures 4 through 6. A groundwater elevation contour map is presented on Figure 7.

This report discusses the subsurface soil conditions in the area of the West MSE Wall followed by a discussion of the hydrogeologic conditions. Appendices A and B follow the main text and present results of our subsurface explorations and laboratory testing, respectively.

Subsequent to completion of the explorations and laboratory tests presented in Appendices A and B, additional explorations and tests were accomplished in an area where right-of-entry had not previously been available (Parcel Numbers 302, 303, 304, and 305). Logs of the additional explorations and results of laboratory tests on samples from the additional explorations are presented in Appendix C. The explorations and test results presented in Appendix C were completed in general accordance with the method presented in Appendices A and B.

PURPOSE AND SCOPE

The purpose of this report is to provide information on subsurface soil and groundwater conditions affecting construction in the area of the West MSE Wall. Proposed construction in this area includes the Third Runway embankment and

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the West MSE Wall adjacent to Miller Creek near Wetland 37. Additional information in other reports is listed in the references at the end of this report. The information presented herein provides the basis for our geotechnical engineering analyses and recommendations.

Information presented herein was obtained in general accordance with Task 5.0—Explorations and Tests, presented in our proposal dated August 23, 1999, and subsequent modification.

GENERALIZED GEOLOGIC DESCRIPTION AND SUBSURFACE SOIL CONDITIONS

This section provides a description of the geologic and subsurface soil conditions within the area of the West MSE Wall, shown on Figure 2, based on Hart Crowser's explorations at the site and explorations by others.

Generalized Geologic Conditions

Generalized geologic conditions in the project area have been described in the Preliminary Engineering Report, Volume 2 (Applied Geotechnology Inc., 1994). The following is a summary of the geologic units identified at the Third Runway project site:

- Fill (loose to medium dense, locally dense, variably graded, silt, sand, and gravel);
- Alluvium (primarily soft to stiff peat, clay, and silt; and very loose to medium dense, fine to medium sand);
- Recessional Outwash (primarily loose to dense, silty sand and gravel, and/or medium stiff to hard, sandy silt and/or sandy clay);
- Glacial Till (dense to very dense, silty sand and gravel, and hard sandy silt);
- Advance Outwash (dense to very dense, non-silty to silty sand and gravel); and
- Lawton Clay (very stiff to hard silt and clay).

Subsurface Conditions

Subsurface soil conditions interpreted from materials encountered in explorations at the site and soil properties inferred from laboratory tests formed

the basis for the information contained in this report. Variations between explorations occur due to the variability in gradation, moisture content, and density/consistency of soils at the site. The nature and extent of these variations may not become evident until construction. If variations become evident, it will be necessary to re-evaluate our interpretation of the soil conditions at the site, as well as any recommendations based on those interpretations.

Generalized subsurface conditions in the area are shown on the wall alignment Profile on Figure 3 and Cross Sections A-A' (Runway Station 173+62), B-B' (Runway Station 181+90), and F-F' (Runway Station 180+06) on Figures 4 through 6, respectively.

The following soil materials were observed in this area:

Soft to stiff interbedded Clay and loose to medium dense Sand with organic material (Peat). Several borings (HC00-B128, HC00-B114, HC00-B115, etc.) encountered peat at the ground surface or interbedded to depths of about 15 feet.

Stiff to hard, slightly sandy to very sandy CLAY and slightly silty CLAY to clayey SILT. These fine-grained soils were encountered at depths ranging to about 6 feet from the ground surface to more than 50 feet (i.e., below the bottom of our borings). These soil units range from about 10 feet to more than 20 feet in thickness.

Medium dense to very dense, slightly gravelly to gravelly, slightly silty to very silty SAND. These soils and the interbedded hard CLAY described above are the primary unit underlying the soft or loose surficial soils described above. The sands are typically fine to medium in gradation. The top of these soils typically extend below depths of about 10 feet to 20 feet below the surface.

Summary of Results from Laboratory Tests

Tables 1 through 3 summarize the parameters determined from tests performed on specimens taken from Shelby tube samples obtained during drilling. The samples within the Shelby tubes were extruded and prepared for assigned laboratory tests in general accordance with the applicable ASTM standards as discussed in Appendix B.

Groundwater Occurrence

Seventeen new wells were installed during this phase of work; HC00-B106, HC00-B111, HC00-B118, HC00-B120, HC00-B121, HC00-B123, HC00-B125, HC00-B126, HC00-B129, HC00-B130, HC00-B132, HC00-B133, HC00-B141, HC00-B142, and HC00-B144 through HC00-B146. The water levels observed in the open borings at the time of drilling (ATD) and subsequent to monitoring well installation and development are shown on the boring logs (Appendix A).

Groundwater Monitoring

Groundwater elevation data are now being collected monthly from 26 wells in the area of the West MSE Wall, beginning with the monitoring event on April 11, 2000. The wells that are being monitored monthly include the 19 new wells listed above, and 7 existing wells. Well construction information, depth to water, and groundwater elevation data are compiled and presented in Table 4. As future monitoring events are completed, seasonal changes in groundwater elevation and flow patterns will be evaluated in the area of West MSE Wall.

Groundwater Flow Mapping

Shallow groundwater elevations observed in April 2000 are contoured on Figure 7. These groundwater levels represent wet season conditions, with elevations that are typically about 2 to 3 feet above the dry season lows observed around October 1999.

Groundwater flow patterns appear to be generally unchanged by seasonal water level variations, with flow generally toward Miller Creek from the higher ground of the airport. This is consistent with conceptual models of local hydrogeology (Applied Geotechnology Inc., 1996), where recharge occurs on the higher ground of the airport, and water moves down into the Shallow Regional Aquifer before discharging to the creek. Artesian conditions observed in some wells (e.g., AT94A-B3 and AT96-B4) indicate an upward hydraulic gradient, consistent with the regional discharge of groundwater to the creek drainage basin, and the effects of local interbedding of more and less permeable soil units. Elsewhere water confined in stratified soil units (e.g., HC00-B118) may be artesian where these soil units are encountered down slope.

The pattern of groundwater flow is broadly consistent with the implied occurrence of significant recharge beneath the existing airport. Not all water levels are necessarily reflective of conditions in the Shallow Regional Aquifer,

since perched zones occur above the main water table, and many of the wells are screened in shallower water-bearing zones.

USE OF THIS REPORT

This report has been prepared for the exclusive use of HNTB and the Port of Seattle, for the site and project described herein. We completed this work according to generally accepted geotechnical engineering practices in the same or similar localities, related to the nature of the work accomplished, at the time the services were accomplished. We make no other warranty, express or implied.

Hart Crowser appreciates the opportunity to provide this information. Please call if you have any questions.

Sincerely,

HART CROWSER, INC.

MICHAEL J. BAILEY, P.E.

Project Manager

JOSEPHA D. CELES, E.I.T. Staff Geotechnical Engineer

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Key to Tables 1 through 3

Symbol	Description
W _n	Natural Moisture Content in Percent
Ϋт	Total Unit Weight in pcf
σ _{ν0} '	Initial Effective Vertical Stress in ksf
σ _p '	Past Effective Vertical Stress in ksf
σ _c '	Confining Stress in ksf
σ ₁ - σ ₃	Principal Stress Difference (or axial stress) in ksf
c'	Cohesion Intercept (based on effective stresses) in psf
φ'	Effective Friction Angle in Degrees
\$ave'	Average Effective Friction Angle in Degrees
OCR	Overconsolidation Ratio
C _c	Compression index
C _r	Recompression Index
e ₀	Initial Void Ratio
c,	Coefficient of Consolidation in ft ² /day
E ₅₀	Modulus of Elasticity (determined at 50% of Peak Strength) in ksf
LL	Liquid Limit in Percent
PI	Plasticity Index in Percent
S _u	Undrained Shear Strength in psf

497821/LabResults.xls - Legend of symbols



Table 1 - Summary of Consolidation Results

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Boring	Sample	Depth	Soil Description	^r A	*		op.	OCR	3	ບັ	8	c, at cp
Number	Number	in Feet		in %	In pcf	In ksf	in ksf					In ft*/day
HC00-B132A	51	8.5 to 10.5	Very soft to soft, very silty CLAY	32	120	1.105	1.6	1	0.181	0.010	0.817	0.75
HC00-B115 HC00-B118	5-2-4-	10 to 11 5.5 to 6.5	Medium stiff, very sandy SILT Medium stiff, slighty sandy, clayey SILT	18 32	131 119	1.3 0.6875	> 64 10	> 30 15	not determined 0.184	0.007 0.026	0.49 0.837	not determined 2.5
HC00-B111 HC00-B142	5. 53	5.5 to 7.5 5.5 to 7.5	Stiff, clayey SILT Stiff, sandy SILT	31 26	118 125	0.715 0.715	12 56	17 78	0.307 0.167	0.017 0.016	0.837 0.67	2.4 1.5
HC00-B111	ک و	15.5 to 16.6	Medium dense, gravelly, very silty SAND	15	135	2.015	4	22	0.200	0.007	0.401	2.3
HC00-B118 HC00-B110	5-11	15.5 to 17.4 40.5 to 41.8	Hard, sandy CLAY Hard, very clayey SILT	25 31	123 119.0	1.9375 5.265	20 42	0 8	0.147 0.178	0.024 0.026	0.687 0.817	3 2.4
*Note: 1. Valu 2. Th	les for σ _p ' he value of	'shown in bol f σ _p 'for HC00	d were determined by extrapolation of the -B115, S-4 exceeded the maximum load fr	virgin com ame load c	npression cu capability	irve due to	load frame	limitations				

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497821/LabResults.xk · Table 1

Table 2 - Summary of Isotropically Consolidated Undrained Triaxial Compression (CU) Test Results

Boring Number	Sample Number	Depth in Feet	Soil Description	wn In %	77 In pcf	o°. In kef	at - a; in kaf	h deg	∳' In deg	E.e. in kaf	0 03 ¹⁰ 6	Esolo.
HC00-B132	S-5	9.0 to 11.0	Medium stiff, sandy CLAY	40.5	114.0	6.0	6.0	367		744.6	0 993	124.1
				32.7	124.3	0.6	8.5	35.1	35.1	426.4	0.948	47 A
				25.3	125.1	12.0	16.4	33.4		341.8	1.367	28.5
HC00-B110	S-4	15.5 to 17.4	Very stiff to hard, slightly sandy, very	25.2	125.0	6.0	7.5	33.2		312.6	1.251	52.1
			clayey SILT	23.0	130.5	9.0	17.9	32.9	33.1	497.0	1.988	55.2
				14.2	135.4	12.0	20.0	33.1		4162.6	1.665	346.9
HC00-B111	S-12	40.5 to 42.1	Hard CLAY	29.6	121.3	6.0	13.9	33.0		256.6	2.317	42.8
				30.5	122.2	0.6	22.3	346	34.1	557.5	2.478	61.9
				31.2	122.8	12.0	22.0	34 8		915.2	1.833	/6.3

497821/LabResults.xls - Table 2

Hart Crowser J-4978-21 Table 3 - Summary of Unconsolidated Undrained (UU) Triaxial Compression Test Results

Boring	Sample	Depth	Soil Description	Ŵ	ĥ	Ţ	Р	1 6
Number	Number	in Feet		л %	In pet	8 IN %	in %	in pst
HC00-B118	S-2	5.5 to 6.5	Medium stiff, slightly sandy, clayey SILT	31.7	123.3	30	4	2023
HC00-B129	S-3	5.5 to 6.8	Stiff, slightly sandy CLAY	28.7	128.5	38	15	1313
HC00-B110 HC00-B118	S-11 S-6	40.5 to 41.8 15.5 to 17.4	Hard, very clayey SILT Hard, sandy, very clayey SILT	31.1 25.0	122.8 124.8	41	13	9259 5486

Sheet 1 of 4

Table 4 - West Wall Area Water Level Data

	AT94	IA-B3	AT9(6-B4	AT97	-869	HC95	-B 37	HC9	-B38	HC99	-839	HC99	-B40
	Depth*	Elevation	Depth*	Elevation	Depth*	Elevation	Depth*	Elevation	Depth*	Elevation	Depth*	Elevation	Depth*	Elevation
	in Feet	in Feet	in Feet	in Feet	in Feet	in Feet	in Feet	in Feet						
Measuring Point	00.0	273.4	00.0	279.7	0.00	337.2	0.00	237.65	0.00	230.88	0.00	230.80	0.00	250.63
Ground Level*	1.4	272	-0.3	280	3.2	334	3.1	234.6	3.3	227.6	-0.3	231.1	2.0	248.u
Top of Screen*	23.4	2,50.0	36.7	243.0	27.7	310	9.1	228.6	12.3	218.6	4.7	226.1	14.0	236.6
Bottom of Screen*	33.4	240.0	46.7	233.0	29.7	308	19.1	218.6	22.3	208.6	14.7	216.1	24.0	226.6
Date: 3/8/1999					1	ı	3.52	234.13	4.40	226.48	0.69	230.11	4.88	245.75
3/10/1999					6.18	331.0								
4/5/1999					6.59	330.6	3.58	234.07	4.41	226.47	0.74	230.06	5.26	245.37
5/4/1999					7.43	329.8	3.82	233.83	4.60	226.28	0.86	229.94	5.75	244.88
5/15/1999					1	I								
6/14/1999					8.08	329.1	5.12	232.53	5.90	224.98	1.68	229.12	6.89	243.74
7/13/1999					8.41	328.8	4.72	232.93	5.93	224.95	2.05	228.75	7.18	243.45
8/13/1999					8.83	328.4	5.70	231.95	6.08	224.80	2.18	228.62	7.13	243.50
9/14/1999					9.16	328.0	6.47	231.18	6.48	224.40	2.51	228.29	7.67	242.96
10/13/1999					9.12	328.1	4.50	233.15	5.98	224.90	2.09	228.71	7.32	243.31
11/11/1666					8.13	329.1	3.22	234.43	4.25	226.63	2.90	227.90	5.80	244.83
12/9/1999					6.80	330.4	3.27	234.38	4.38	226.50	0 27	230.53	5.00	245.63
1/13/2000					6.48	330.7	3.20	234.45	4.35	226.53	0.54	230.26	4.86	245.77
2/14/2000					6.54	330.7	3.12	234.53	4.33	226.55	0.59	230.21	4.49	246.14
3/9/2000	Flowing	>272	Flowing	>280	6.82	330.4	3.17	234.48	4.43	226.45	0.61	230.19	5.57	245.06
4/11/2000	Flowing	>272	Flowing	>280	7.45	329.8	3.35	234.30	4.60	226.28	0.88	229.92	5.08	245.55
5/10/2000	Flowing	>272	Flowing	>280	7.78	329.4	3.19	234.46	4.32	226.56	0.88	229.92	5.14	245.49
-	_			•		•						•		

Italics = Estimated

Depth* All depths are below measuring point (NOT below the ground surface) - Indicates data not available.

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Depth* Elevation Depth* Elevation in Feet in Feet in Feet in F Measuring Point 0.00 315.81 0.00 28		HC00-	2		-P120	HC00-	B121	HC00	-8123	HC00	- B12 5	
Measuring Point 0.00 315.81 0.00 28	* Elevation	Depth* I	Elevation	Depth* in Ecot	Elevation	Depth*	Elevation	Depth*	Elevation	Depth*	Elevation	
·	0 286.06	0.00	298.61	0.00	236.93		111 reet		10 Feet 1		IN FEET	
Ground Level* 1.7 314.1 0.8 2	8 285.3	1.0	297.7	2.9	234.0	2.1	2.925	во: 6 С	7 23 4 7	00.0 7 Q	0.122	
Top of Screen* 11.7 304.1 9.8 2	8 276.3	7.0	291.7	17.6	219.3	6.8	225.0	14.0	223.7	3.6	254.2	
Bottom of Screen* 21.7 294.1 19.8 2	8 266.3	12.0	286.7	22.6	214.3	16.8	215.0	24.0	213.7	8.6 8.6	249.2	
Date: 3/8/1999												
3/10/1999			••••									
4/5/1999												
5/4/1999												
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11/11/1999												
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1/13/2000												
2/14/2000 5.49 310.32 6.80 27	0 279.26	6.63	291.98									
3/9/2000 5.50 310.31 6.94 27	4 279.12	6.71	291.90									
4/11/2000 6.21 309.60 8.34 27	4 277.72	7.84	290.77	5.1	231.83	0.80	230.98	2.06	235.58	3.74	254.06	
5/10/2000 6.38 309.43 8.59 27	9 277.47	7.64	290.97	4.92	232.01	0.62	231.16	1.90	235.74	3.89	253.91	
			•		-		-		-			
Italics = Estimated												
Depth* All depths are below mea	ow measuring	g point (NC	JT below	the groun	d surface)							

Table 4 - West Wall Area Water Level Data

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- Indicates data not available.

497821\SeaTacWaterLevels.xls - West Wall

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Sheet 2 of 4

Depth* Elevation Dout 243.12 21.14 21.11 21.13 23.61 112.9 23.61 112.9 23.61 112.9 23.61 112.9 23.61 112.9 23.61 112.9 23.61 112.9 23.61 112.9 23.61 112.9 23.61 12.9 23.61 12.9 23.61 12.9 23.61 12.9 23.61 12.9 23.61 12.9 23.61 12.9 23.61 12.9 23.61	Elevation Depth* Elevation Distribution Distribution <th>Depth* Elevation Depth* Elevation<</th> <th>Depth* Elevation Depth* Elevation Elevation Depth* Elevation</th> <th>Depth* Elevation Depth* Elevation Elevation Elevati</th> <th>Depth* Elevation Depth* Elevation Depth in Feet in Feet in Feet in Feet in Feet in Feet Measuring Point 0.00 251.56 0.00 245.83 0 Ground Level* 1.4 250.2 2.6 243.2 0 Top of Screen* 8.4 243.2 9.6 236.2 1 Bottom of Screen* 13.4 238.2 14.6 231.2 1 Job of Screen* 13.4 238.2 14.6 231.2 1 S/10/1999 5/4/1999 5/4/1999 5/4/1999 5/15/1999 5/15/1999 5/15/1999 5/15/1999 5/15/1999 5/15/1999 5/15/1999 5/15/1999 5/15/1999 5/15/1999 5/15/1999 5/15/1999</th> <th>n Depth* E in Feet 2 2.3</th> <th>levation</th> <th>Depth* E</th> <th>Incitor - 1</th> <th></th> <th></th> <th>+</th> <th>rise in the second</th> <th></th> <th>:</th>	Depth* Elevation Depth* Elevation<	Depth* Elevation Elevation Depth* Elevation	Depth* Elevation Elevation Elevati	Depth* Elevation Depth* Elevation Depth in Feet in Feet in Feet in Feet in Feet in Feet Measuring Point 0.00 251.56 0.00 245.83 0 Ground Level* 1.4 250.2 2.6 243.2 0 Top of Screen* 8.4 243.2 9.6 236.2 1 Bottom of Screen* 13.4 238.2 14.6 231.2 1 Job of Screen* 13.4 238.2 14.6 231.2 1 S/10/1999 5/4/1999 5/4/1999 5/4/1999 5/15/1999 5/15/1999 5/15/1999 5/15/1999 5/15/1999 5/15/1999 5/15/1999 5/15/1999 5/15/1999 5/15/1999 5/15/1999 5/15/1999	n Depth* E in Feet 2 2.3	levation	Depth* E	Incitor - 1			+	rise in the second		:
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Ground Level* 1.4 250.2 2.6 243.2 2.3 223.1 2.6 227.4 2.4 241.1 0.9 Top of Screen* 8.4 243.2 9.6 236.2 7.3 218.1 3.6 226.4 7.4 236.1 12.9 Bottom of Screen* 8.4 243.2 9.6 231.2 11.4 214.1 18.6 211.4 12.4 231.1 229 Jourses 3/8/1999 3/10/1999 13.4 238.2 14.6 231.2 11.4 214.1 18.6 211.4 231.1 229 Jourses 3/10/1999 5/15/1999 <td>1 2502 2.6 243.2 2.3 223.1 2.6 227.4 2.4 241.1 0.9 257.1 1 243.2 9.6 236.2 7.3 218.1 3.6 226.4 7.4 236.1 12.9 245.2 1 238.2 14.6 231.2 11.4 214.1 18.6 211.4 12.4 231.1 22.9 235.2 2 238.2 14.6 231.2 11.4 214.1 18.6 211.4 12.4 231.1 22.9 235.2 2 238.2 11.4 214.1 18.6 211.4 12.4 231.1 22.9 235.2 2<</td> <td>d Level* 1.4 250.2 2.6 243.2 2.3 213.1 2.6 227.4 2.4 241.1 0.9 257.8 2.7 Screen* 8.4 241.2 9.6 236.2 7.3 218.1 3.6 226.4 7.4 236.1 12.9 245.8 17.2 3/10/1999 3/10/1999 3/10/1999 1.14 211.1 18.6 211.4 12.1 22.9 235.8 22.2 5/15/1999 5/17/1999 1.14 214.1 18.6 211.4 12.4 231.1 12.9 235.8 17.2 5/15/1999 5/17/1999 1.14 214.1 18.6 211.4 12.4 231.1 22.9 245.8 17.2 5/13/1999 6/14/1999 10/13/1999 10/13/1999 10/13/1999 10/13/1999 10/13/1999 10/13/1999 10/13/1999 10/13/1999 10/13/1999 10/13/1999 10/13/1999 10/13/1999 10/13/1999 10/13/1999 10/13/1999 10/13/1999 10/13/1999 10/</td> <td>$\begin{array}{ c c c c c c c c c c c c c c c c c c c$</td> <td>5:00:md Levet* 1.4 250.2 2.6 243.2 2.3 213.1 2.6 227.4 2.4 241.1 0.9 257.8 2.7 255.0 0:p of Screen* 8.4 2.43.2 2.36 2.14 2.14 12.4 231.1 12.9 255.8 2.22 250.0 0:p of Screen* 8.4 2.43.2 2.31.2 11.4 21.1 11.4 21.1 12.9 255.8 2.22 250.0 0:p of Screen* 13.4 23.8 21.1.4 21.4 11.4 21.1 12.4 231.1 22.9 255.8 22.2 250.0 0:p of Screen* 13.4 23.8 21.1 21.1 21.1 21.1 21.1 22.9 255.8 22.2 250.0 0:p of 14/1999 5/15/1999 5/14/1999 11.1 11.4 21.4 21.4 21.4 21.4 21.4 21.4 22.9 255.8 257.3 259.4 0:p 11/1/1999 11/1/1/1999 11/1/1/1999 11/1/1/1999 11/1/1/199 11/1/1/199 11/1/1/199 21/1 21.2 250.1 254.4 241.03 8.91.4 250.70 1/13/2000 1.07 249.24 3.10 2.07 2.44.2.5</td> <td>Ground Level* 1.4 250.2 2.6 243.2 Top of Screen* 8.4 243.2 9.6 236.2 Bottom of Screen* 13.4 238.2 14.6 231.2 1 <u>Date:</u> 3/8/1999 3/10/1999 5/4/1999 5/15/1999 5/15/1999</td> <td>2 2.3</td> <td>225.46</td> <td>0.00</td> <td>229.96</td> <td>0.00</td> <td>243.47</td> <td>00'0</td> <td>258.64</td> <td>0.00</td> <td>272.7</td>	1 2502 2.6 243.2 2.3 223.1 2.6 227.4 2.4 241.1 0.9 257.1 1 243.2 9.6 236.2 7.3 218.1 3.6 226.4 7.4 236.1 12.9 245.2 1 238.2 14.6 231.2 11.4 214.1 18.6 211.4 12.4 231.1 22.9 235.2 2 238.2 14.6 231.2 11.4 214.1 18.6 211.4 12.4 231.1 22.9 235.2 2 238.2 11.4 214.1 18.6 211.4 12.4 231.1 22.9 235.2 2<	d Level* 1.4 250.2 2.6 243.2 2.3 213.1 2.6 227.4 2.4 241.1 0.9 257.8 2.7 Screen* 8.4 241.2 9.6 236.2 7.3 218.1 3.6 226.4 7.4 236.1 12.9 245.8 17.2 3/10/1999 3/10/1999 3/10/1999 1.14 211.1 18.6 211.4 12.1 22.9 235.8 22.2 5/15/1999 5/17/1999 1.14 214.1 18.6 211.4 12.4 231.1 12.9 235.8 17.2 5/15/1999 5/17/1999 1.14 214.1 18.6 211.4 12.4 231.1 22.9 245.8 17.2 5/13/1999 6/14/1999 10/13/1999 10/13/1999 10/13/1999 10/13/1999 10/13/1999 10/13/1999 10/13/1999 10/13/1999 10/13/1999 10/13/1999 10/13/1999 10/13/1999 10/13/1999 10/13/1999 10/13/1999 10/13/1999 10/13/1999 10/	$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	5:00:md Levet* 1.4 250.2 2.6 243.2 2.3 213.1 2.6 227.4 2.4 241.1 0.9 257.8 2.7 255.0 0:p of Screen* 8.4 2.43.2 2.36 2.14 2.14 12.4 231.1 12.9 255.8 2.22 250.0 0:p of Screen* 8.4 2.43.2 2.31.2 11.4 21.1 11.4 21.1 12.9 255.8 2.22 250.0 0:p of Screen* 13.4 23.8 21.1.4 21.4 11.4 21.1 12.4 231.1 22.9 255.8 22.2 250.0 0:p of Screen* 13.4 23.8 21.1 21.1 21.1 21.1 21.1 22.9 255.8 22.2 250.0 0:p of 14/1999 5/15/1999 5/14/1999 11.1 11.4 21.4 21.4 21.4 21.4 21.4 21.4 22.9 255.8 257.3 259.4 0:p 11/1/1999 11/1/1/1999 11/1/1/1999 11/1/1/1999 11/1/1/199 11/1/1/199 11/1/1/199 21/1 21.2 250.1 254.4 241.03 8.91.4 250.70 1/13/2000 1.07 249.24 3.10 2.07 2.44.2.5	Ground Level* 1.4 250.2 2.6 243.2 Top of Screen* 8.4 243.2 9.6 236.2 Bottom of Screen* 13.4 238.2 14.6 231.2 1 <u>Date:</u> 3/8/1999 3/10/1999 5/4/1999 5/15/1999 5/15/1999	2 2.3	225.46	0.00	229.96	0.00	243.47	00'0	258.64	0.00	272.7
Top of Screent 8.4 243.2 9.6 236.2 7.3 218.1 3.6 226.4 7.4 236.1 12.9 Bottom of Screent 13.4 238.2 14.6 231.2 11.4 218.1 36 226.4 7.4 236.1 12.9 Date: 3/10/1999 3/10/1999 13.4 238.2 14.6 231.2 11.4 218.1 12.4 231.1 22.9 5/4/1999 5/15/1999 5/15/1999 5/15/1999 5/15/1999 231.1 22.9 231.1 22.9 5/15/1999 6/14/1999 13/10/1999 11.4 218.6 211.4 12.4 231.1 22.9 5/15/1999 6/14/1999 10/13/1999 10/13/1999 10/13/1999 10/13/1999 10/13/1999 10/13/1999 10/13/1999 11/11/1999 2.42.26 2.54.1 240.96 7.9 2/14/2000 2.02 2492.26 2.44.240.30 2.44.240.30 2.44.240.30 2.44.240.30 2.44.240.30 2.44.240.30 2.44.240.30	2432 9.6 236.2 7.3 218.1 3.6 226.4 7.4 236.1 12.9 245 1 238.2 14.6 231.2 11.4 214.1 18.6 211.4 231.1 22.9 235 2 238.2 14.6 231.2 11.4 214.1 18.6 211.4 231.1 22.9 235 2 2 2 2 18.6 211.4 18.6 231.1 22.9 235 2 <td>Screent 8.4 243.2 9.6 236.2 7.3 218.1 3.6 226.4 7.4 236.1 12.9 245.8 17.2 3/8(1999 3/10/1999 3/10/1999 11.4 211.4 11.4 211.4 12.4 231.1 22.9 235.8 12.2 235.8 12.2 3/10/1999 4/5/1999 5/4/1999 11.4 211.4 18.6 211.4 12.4 231.1 22.9 235.8 22.2 3/10/1999 5/4/1999 5/4/1999 12.4 231.1 22.9 235.8 22.2 231.1 22.9 235.8 22.2 3/10/1999 5/1/3/1999 8/13/1999 11.3 24.4 240.96 7.94 250.70 1/13/2000 2.02 249.54 3.07 242.26 1.73 22.37.31 2.55 22.7.41 3.27 3.37 3.37 3.37 3.37 3.37 3.37 3.37 3.37 3.37 3.37 3.37 3.411/2000 2.91.2 2</td> <td>Op of Screent 8.4 243.2 9.6 236.2 7.3 218.1 3.6 226.4 7.4 236.1 12.9 245.8 17.2 235.8 17.2 235.8 17.2 235.8 17.2 235.8 17.2 235.8 17.2 235.8 21.2 13.4 238.2 14.6 231.2 11.4 21.4 21.4 23.1 22.9 235.8 22.2 250.0 9/10/1999 4/5/1999 5/14/1999 5/13/1999 5/13/1999 5/13/1999 2/14/1090 2/14/1090 2/14/1090 2/14/1090 2/14/1090 2/14/1090 2/14/1090 2/14/1090 2/14/1090 2/14/1090 2/14/1090 2/14/1090 2/14/1090 2/14/1000 2/14/1090 2/14/1000 2/14/1090 2/14/1000</td> <td>Cip of Screent 8.4 2.43.2 9.6 236.2 7.3 218.1 3.6 21.4 1.3.4 231.1 2.39 245.8 17.2 235.8 17.2 235.1 235.8 17.2 235.1 235.8 235.2 235.8 17.2 235.1 235.8 17.2 235.1 235.8 17.2 235.1 235.8 17.2 235.1 235.8 17.2 235.1 235.2 235.9 237.2 235.0 237.2 235.0 237.2 235.0 237.2 235.0 237.2 235.0 237.2 235.0 237.2 235.0 237.2 235.0 237.2 235.0 237.2 235.0 237.2 235.0 237.2 235.0 237.2 235.0 237.2 237.1 239.2 239.2 239.2 239.2 239.2 239.2 237.2 269.4 341.3 237.2 249.3 337.2 249.1 337.2 249.1 337.2 249.1 337.2 249.1 337.2 249.1 337.2<!--</td--><td>Top of Screen* 8.4 243.2 9.6 236.2 Bottom of Screen* 13.4 238.2 14.6 231.2 1 <u>Date:</u> 3/8/1999 3/10/1999 4/5/1999 5/4/1999 5/15/1999 5/15/1999</td><td></td><td>223.1</td><td>2.6</td><td>227.4</td><td>2.4</td><td>241.1</td><td>0.9</td><td>257.8</td><td>2.7</td><td>270.</td></td>	Screent 8.4 243.2 9.6 236.2 7.3 218.1 3.6 226.4 7.4 236.1 12.9 245.8 17.2 3/8(1999 3/10/1999 3/10/1999 11.4 211.4 11.4 211.4 12.4 231.1 22.9 235.8 12.2 235.8 12.2 3/10/1999 4/5/1999 5/4/1999 11.4 211.4 18.6 211.4 12.4 231.1 22.9 235.8 22.2 3/10/1999 5/4/1999 5/4/1999 12.4 231.1 22.9 235.8 22.2 231.1 22.9 235.8 22.2 3/10/1999 5/1/3/1999 8/13/1999 11.3 24.4 240.96 7.94 250.70 1/13/2000 2.02 249.54 3.07 242.26 1.73 22.37.31 2.55 22.7.41 3.27 3.37 3.37 3.37 3.37 3.37 3.37 3.37 3.37 3.37 3.37 3.37 3.411/2000 2.91.2 2	Op of Screent 8.4 243.2 9.6 236.2 7.3 218.1 3.6 226.4 7.4 236.1 12.9 245.8 17.2 235.8 17.2 235.8 17.2 235.8 17.2 235.8 17.2 235.8 17.2 235.8 21.2 13.4 238.2 14.6 231.2 11.4 21.4 21.4 23.1 22.9 235.8 22.2 250.0 9/10/1999 4/5/1999 5/14/1999 5/13/1999 5/13/1999 5/13/1999 2/14/1090 2/14/1090 2/14/1090 2/14/1090 2/14/1090 2/14/1090 2/14/1090 2/14/1090 2/14/1090 2/14/1090 2/14/1090 2/14/1090 2/14/1090 2/14/1000 2/14/1090 2/14/1000 2/14/1090 2/14/1000	Cip of Screent 8.4 2.43.2 9.6 236.2 7.3 218.1 3.6 21.4 1.3.4 231.1 2.39 245.8 17.2 235.8 17.2 235.1 235.8 17.2 235.1 235.8 235.2 235.8 17.2 235.1 235.8 17.2 235.1 235.8 17.2 235.1 235.8 17.2 235.1 235.8 17.2 235.1 235.2 235.9 237.2 235.0 237.2 235.0 237.2 235.0 237.2 235.0 237.2 235.0 237.2 235.0 237.2 235.0 237.2 235.0 237.2 235.0 237.2 235.0 237.2 235.0 237.2 235.0 237.2 235.0 237.2 237.1 239.2 239.2 239.2 239.2 239.2 239.2 237.2 269.4 341.3 237.2 249.3 337.2 249.1 337.2 249.1 337.2 249.1 337.2 249.1 337.2 249.1 337.2 </td <td>Top of Screen* 8.4 243.2 9.6 236.2 Bottom of Screen* 13.4 238.2 14.6 231.2 1 <u>Date:</u> 3/8/1999 3/10/1999 4/5/1999 5/4/1999 5/15/1999 5/15/1999</td> <td></td> <td>223.1</td> <td>2.6</td> <td>227.4</td> <td>2.4</td> <td>241.1</td> <td>0.9</td> <td>257.8</td> <td>2.7</td> <td>270.</td>	Top of Screen* 8.4 243.2 9.6 236.2 Bottom of Screen* 13.4 238.2 14.6 231.2 1 <u>Date:</u> 3/8/1999 3/10/1999 4/5/1999 5/4/1999 5/15/1999 5/15/1999		223.1	2.6	227.4	2.4	241.1	0.9	257.8	2.7	270.
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3/9/2000 1.82 249.74 3.15 242.68 241.03 8.9	2 249.74 3.15 242.68 8.91 249 7 249.59 3.59 242.24 1.73 223.73 2.65 227.31 2.53 240.94 10.21 248 7 249.49 3.6 242.23 1.67 223.79 2.55 227.41 2.61 240.86 10.75 247	3/9/2000 1.82 249.74 3.15 242.68 4/11/2000 1.97 249.59 3.59 242.24 1.73 223.73 2.65 227.31 2.53 240.94 10.21 248.43 3.53 3.51 5.710/2000 2.07 249.49 3.6 242.23 1.67 223.79 2.55 227.41 2.61 240.86 10.75 247.89 3.58 5.51 5.710/2000	3/9/2000 1.82 249.74 3.15 242.68 3.27 269. 4/11/2000 1.97 249.59 3.59 242.24 1.73 223.73 2.65 227.31 2.53 240.94 10.21 248.43 3.53 269. 5/10/2000 2.07 249.49 3.6 242.23 1.67 223.79 2.55 227.41 2.61 240.86 10.75 247.89 3.58 269.	3/9/2000 1.82 249.74 3.15 242.68 3.27 269.4 $4/11/2000$ 1.97 249.59 3.59 242.24 1.73 223.73 2.65 227.31 2.53 240.94 10.21 248.43 3.53 269.1 $5/10/2000$ 2.07 249.49 3.6 242.23 1.67 223.79 2.55 227.41 2.61 240.96 10.21 248.43 3.53 269.1 $5/10/2000$ 2.07 249.49 3.6 242.23 1.67 223.79 2.55 227.41 2.61 240.86 10.75 247.89 3.58 269.1 <i>Italics</i> = Estimated Depth* All depths are below measuring point (NOT below the ground surface)	2/14/2000 2.02 249.54 3.07 242.76	9				2.51	240.96	7.94	250.7(
	7 249.59 3.59 242.24 1.73 223.73 2.65 227.31 2.53 240.94 10.21 248 7 249.49 3.6 242.23 1.67 223.79 2.55 227.41 2.61 240.86 10.75 247	4/11/2000 1.97 249.59 3.59 242.24 1.73 223.73 2.65 227.31 2.53 240.94 10.21 248.43 3.53 2 5/10/2000 2.07 249.49 3.6 242.23 1.67 223.79 2.55 227.41 2.61 240.86 10.75 247.89 3.58	4/11/2000 1.97 249.59 3.59 242.24 1.73 223.73 2.65 227.31 2.53 240.94 10.21 248.43 3.53 269.1 5/10/2000 2.07 249.49 3.6 242.23 1.67 223.79 2.55 227.41 2.61 240.86 10.75 247.89 3.58 269.1 Italics = Estimated	4/11/2000 1.97 249.59 3.59 242.24 1.73 223.73 2.65 227.31 2.53 240.94 10.21 248.43 3.53 269.1 5/10/2000 2.07 249.49 3.6 242.23 1.67 223.79 2.55 227.41 2.61 240.86 10.21 248.43 3.58 269.1 5/10/2000 2.07 249.49 3.6 242.23 1.67 223.79 2.55 227.41 2.61 240.86 10.75 247.89 3.58 269.1 Italics = Estimated Depth* All depths are below measuring point (NOT below the ground surface)	3/9/2000 1.82 249.74 3.15 242.68	8				2.44	241.03	8.91	249.73	3.27	269.4
4/11/2000 1.97 249.59 3.59 242.24 1.73 223.73 2.02 227.21 2.03 249.59 240.59 2.00 1.97	7 249.49 3.6 242.23 1.67 223.79 2.55 227.41 2.61 240.86 10.75 247	5/10/2000 2.07 249.49 3.6 242.23 1.67 223.79 2.55 227.41 2.61 240.86 10.75 247.89 3.58 2	5/10/2000 2.07 249.49 3.6 242.23 1.67 223.79 2.55 227.41 2.61 240.86 10.75 247.89 3.58 269. Italics = Estimated	5/10/2000 2.07 249.49 3.6 242.23 1.67 223.79 2.55 227.41 2.61 240.86 10.75 247.89 3.58 269. <i>Italics</i> = Estimated Depth* All depths are below measuring point (NOT below the ground surface)	4/11/2000 1.97 249.59 3.59 242.24	4 1.73	223.73	2.65	227.31	2.53	240.94	10.21	248.4	3.53	269.1
5/10/2000 2.07 249.49 3.6 242.23 1.67 223.79 2.55 227.41 2.61 240.86 10.7			Italics = Estimated	<i>Italics</i> = Estimated Depth* All depths are below measuring point (NOT below the ground surface)	5/10/2000 2.07 249.49 3.6 242.23	3 1.67	223.79	2.55	227.41	2.61	240.86	10.75	247.85	9 3.58	269.1
tatics = Estimated	c = Ectimated			Depth* All depths are below measuring point (NOT below the ground surface)			- + (-							

Table 4 - West Wall Area Water Level Data

Sheet 3 of 4

Hart Crowser J-4978-21

497821\SeaTacWaterLevels.xls - West Wall

Sheet 4 of 4

Table 4 - West Wall Area Water Level Data

	HC00	-B144	HC00	-8145	HC00	-B146
	Depth*	Elevation	Depth [*]	Elevation	Depth*	Elevation
asuring Point	0.00	248.99	0.00	265.11	0.00	111 FEL 263.55
ound Level*	2.4	246.6	2.3	262.8	2.9	260.7
o of Screen*	8.9	240.1	12.3	252.8	11.9	251.7
ttom of Screen*	13.9	235.1	17.3	247.8	16.9	246.7
<u>ate:</u> 3/8/1999						
3/10/1999						
4/2/1999						
5/4/1999				-		
5/15/1999						
6/14/1999						
7/13/1999						
8/13/1999						
9/14/1999						
10/13/1999						
11/11/1999		_				
12/9/1999						
1/13/2000						
2/14/2000			2.94	262.17		
3/9/2000	2.98	246.01	3.14	261.97	3.81	259.74
4/11/2000	3.17	245.82	3.51	261.60	4.02	259.53
5/10/2000	3.00	245.99	3.18	261.93	3.79	259.76
	Italics	= Estimate	q			
	Depth*	All depths	are below	' measurin	g point (N	OT below
	-	Indicates c	lata not av	aldeliev		
		, ,,,,,,,,,,,,,				

Hart Crowser J-4978-21

Vicinity Map



0 200 4000 Scale in Feet **HARTCROWSER** J-4978-21 6/00 Figure 1



RC 6/15/00 1≈100 (xref)see drawing fis/752-color.pcp





200

100

50

0 Scale

in Feel

윢



Profile

Generalized Subsurface West MSE Wall (Looking East

Note: Contacts between soil units are based upon interpolation between borings and represent our interpretation of subsurface conditions based on currently available data.

MSE wail tiers and other geometric details are only conceptual.

5mD'+112826+ 00H 6/16/00 1=1 00 chonie.pc2





AR 045273

3/00 HARTCROWSER Figure 4

J-4978-21



Note: Contacts between soil i between borings and represen conditions based on currently

9012826* Sog asteboow 04=1 00/81/8 HLO





3/00 HARTCROWSER J-4978-21 Figure 5

H

Water Level

ΔIA

N Value

- 5/05

49762107 DuH 6/16/00 1=40 woodstek.pc2



CV0 6/20/00 1≈40 chorie.pc2



APPENDIX A FIELD EXPLORATIONS METHODS AND ANALYSIS

APPENDIX A FIELD EXPLORATIONS METHODS AND ANALYSIS

This appendix documents the processes Hart Crowser used in determining the nature of the soils underlying the project site addressed by this report. The discussion includes information on the following subjects:

- Explorations and Their Location;
- ► The Use of Auger Borings;
- Standard Penetration Test (SPT) Procedures;
- ► Use of Shelby Tubes
- Pocket Penetrometer (PP) and Torvane (TV);
- Excavation of Test Pits;
- Monitoring Well Installation;
- Monitoring Well Development;
- Water Level Measurement; and
- References for Appendix A.

Explorations and Their Location

Subsurface explorations for this project include the following:

Borings

Our first phase of exploration included borings HC00-B106 through HC00-B108, HC00-B110, HC00-B111, HC00-B114 through HC00-B118, HC00-B124, HC00-B126, HC00-B127, HC00-N129, HC00-B131, HC00-B133, HC00-B134, HC00-B139 through HC00-B142, and HC00-B144 through HC00-B146. Logs for these borings are presented in Appendix A. Our second phase of exploration included borings HC00-B113, HC00-B119 through HC00-B123, HC00-B125, HC00-B128, HC00-B130, and HC00-B132. Logs for these borings are presented in Appendix C.

Hand-Auger Borings

Our first phase of exploration included hand-auger borings HC00-A100, HC00-A105, HC00-A109, HC00-A137, and HC00-A143. Logs of these borings are presented in Appendix A.

Test Pits

Our first phase of exploration included test pits HC00-TP100 through HC00-TP108, HC00-TP113 through HC00-TP121, and HC00-TP123 through HC00-TP129. Logs for these test pits are presented in Appendix A. Our second

Page A-1

phase of exploration included test pits HC00-TP110 through HC00-TP112. Logs of these test pits are presented in Appendix C.

The exploration logs within this appendix show our interpretation of the material encountered based on drilling (or excavation), sampling, and testing data. They indicate the depth where the soils change. Note that the change may be gradual. In the field, we classified the samples taken from the explorations according to the methods presented on Figure A-1 - Key to Exploration Logs. This figure also provides a legend explaining the symbols and abbreviations used in the logs.

Location of Explorations. Figure 2 shows the location of explorations. Borings and test pits were located using a global positioning system (GPS) survey by Hart Crowser. Port of Seattle surveyors performed an x, y, z survey for the top of casing elevations of the wells and ground elevations for test pits and some borings completed without wells. Where available, the Port's survey supersedes the GPS locations. Where Port survey data are not available, ground surface elevations were interpreted from the aerial survey topography shown on Figure 2. The method used determines the accuracy of the location and elevation of the explorations.

The Use of Auger Borings

With depths ranging from 14.3 to 74.5 feet below the ground surface, twentyfour hollow-stem auger borings, designated HC00-B106 through HC00-B108, HC00-B110, HC00-B111, HC00-B114 through HC00-B118, HC00-B124, HC00-B126, HC00-B127, HC00-N129, HC00-B131, HC00-B133, HC00-B134, HC00-B139 through HC00-B142, and HC00-B144 through HC00-B146, were drilled from January 27 through February 15, 2000. Samples were obtained by use of the Standard Penetration Test (SPT) samples or a hydraulically pushed thin wall sampler referred to as a "Shelby tube." The borings used a 3-3/8-inch inside diameter hollow-stem auger and were advanced with a truck-mounted drill rig subcontracted by Hart Crowser.

In five locations, hand-auger borings, designated HC00-A100, HC00-A105, HC00-A109, HC00-A137, and HC00-A143, were drilled using portable gear rather than hollow-stem auger borings because of access restraints. Hand-auger boring HC00-A100 was drilled on January 18, 2000, and the other four were drilled on February 14, 2000. In addition, other borings planned for this phase of work have been delayed because of access restrictions and will be reported in the final of this report.

An engineering geologist from Hart Crowser continuously observed the drilling. Detailed field logs were prepared of each boring. Using the Standard

Page A-2

Penetration Test (SPT), we generally obtained split-spoon samples at 5-foot-depth intervals with Shelby tube samples interspersed between from these borings.

Groundwater levels in the borings were noted at the time of drilling (ATD) and following installation and development of observation wells where noted on the boring logs and shown in Table 4.

The borings logs are presented on Figures A-2 through A-25 at the end of this appendix. Figures A-26 through A-28 present the hand-auger boring logs.

Standard Penetration Test (SPT) Procedures

This test is an approximate measure of soil density and consistency. To be useful, the results must be used with engineering judgment in conjunction with other tests. The SPT (as described in ASTM D 1587) was used to obtain disturbed samples. This test employs a standard 2-inch outside diameter split-spoon sampler. Using a 140-pound hammer, free falling 30 inches; the sampler is driven into the soil for 18 inches. The number of blows (N value) required to drive the sampler <u>the last 12 inches only</u> is the Standard Penetration Resistance. This resistance, or blow count, measures the relative density of granular soils and the consistency of cohesive soils. The blow counts are plotted on the boring logs at their respective sample depths.

Soil samples are recovered from the split-barrel sampler, field classified, and placed into water tight jars. They are then taken to Hart Crowser's laboratory for further testing.

In the Event of Hard Driving

Occasionally very dense materials or the presence of gravel and/or cobbles prevented driving the total 18-inch sample. When this happens, the penetration resistance is entered on logs as follows:

Penetration less than six inches. The log indicates the total number of blows over the number of inches of penetration.

Penetration greater than six inches. The blow count noted on the log is the sum of the total number of blows completed <u>after</u> the first 6 inches of penetration. This sum is expressed over the number of inches driven that exceed the first 6 inches. The number of blows needed to drive the first 6 inches is not reported. For example, a blow count series of 12 blows for 6 inches, 30 blows for 6 inches, and 50 (the maximum number of blows counted within a 6-inch increment for SPT) for 3 inches would be recorded as 80/9.

Use of Shelby Tubes

At some boring locations, as noted on the logs, a 3-inch-diameter thin-walled steel (Shelby) tube sampler was pushed hydraulically below the auger to obtain a relatively undisturbed sample for classification and testing of fine-grain soils. The tubes were sealed in the field and taken to our laboratory for extrusion and classification. The undisturbed samples were typically obtained for consolidation and shear strength testing.

Pocket Penetrometer (PP) and Torvane (TV)

The pocket penetrometer and torvane procedures provide quick approximate tests of the consistency (undrained shear strength) of a cohesive soil sample.

The pocket penetrometer device consists of a calibrated spring mechanism that measures penetration resistance of a 1/4-inch-diameter steel tip over a given distance. The penetration resistance is correlated to the unconfined compressive strength of the soil, which is typically twice the undrained shear strength of a saturated, cohesive soil.

The torvane device consists of a 1-inch-diameter plate with eight equally spaced and radially arranged 1/4-inch vanes. The vanes are pressed into the soil and the device is rotated. The vanes force a shear failure to take place over the area of plate face. The resistance at failure, as measured by a calibrated spring, correlates to the undrained shear strength of the sample tested. The exploration logs show the results of the pocket penetrometer and torvane tests.

Pocket penetrometer and torvane test results are generally considered valid only for predominantly fine-grained (non-sandy soils). Results may be artificially low for tests on disturbed samples (i.e., SPT) compared to relatively undisturbed samples from test pits or Shelby tubes.

Excavation of Test Pits

Twenty-five test pits, designated HC00-TP100 through HC00-TP108, HC00-TP113 through HC00-TP121, and HC00-TP123 through HC00-TP129, were excavated across the site with a tractor-mounted backhoe provided by Port Construction Services. The test pits were excavated between January 25 and 28, 2000. The sides of these excavated pits offer direct observation of the subgrade soils. The test pits were located by and excavated under the direction of an engineering geologist from Hart Crowser. The geologist observed the soil exposed in the test pits and reported the findings on a field log. Our geologist

Page A-4

took representative samples of soil types for testing at Hart Crowser's laboratory was noted The geologist noted groundwater levels or seepage during excavation on the log. The density/consistency of the soils (as presented parenthetically on the test pit logs to indicate their having been estimated) is based on visual observation only, as disturbed soils cannot be measured for in-place density.

The test pit logs are presented on Figures A-29 through A-41.

Monitoring Well Installation

Monitoring wells were completed in selected wells as noted on the logs to allow long-term groundwater elevation monitoring. The wells were drilled using standard hollow-stem auger equipment. Two-inch-diameter Schedule 40 PVC riser pipe and 2-inch-diameter 0.020-inch machine-slotted screen were used for the well casings and screens. The well screen and casing riser are lowered down through the hollow-stem auger. As the auger is withdrawn, No. 10/20 silica sand is placed in the annular space from the base of the boring to approximately 2 to 3 feet above the top of the well screen. In some borings the bottom of the borehole was backfilled with bentonite chips prior to placement of the screen and in one case the bottom of the borehole caved prior to installation of the screen.

Well seals were constructed by placing bentonite chips in the annular space on top of the filter sand to within 3 feet of ground surface. The remaining annular space was backfilled with concrete to complete the surface seal. For security, the monitoring wells were completed with locking stick-up steel monuments set in concrete. The monitoring well construction details are illustrated on the boring logs.

The monitoring well installations were constructed in accordance with Washington State Department of Ecology regulations.

Monitoring Well Development

The monitoring wells were developed using a Whale electric submersible pump, surge block, and/or a stainless steel bailer. First, sediment was removed from the bottom of the wells using a stainless steel bailer. Then the wells were surged during development using either a surge block, a stainless steel bailer, or by moving the submersible pump up and down within the well screen depth interval.

Page A-5

A minimum of ten casing volumes was removed during development, in addition to the volume of water added during drilling, if any. Where possible, development continued until negligible turbidity was visible. Sediment thickness at the bottom of the well was measured and recorded before and after development. Observations were recorded on a Well Development data form. Visual changes in turbidity during development were recorded in the comments space on this form. All development water was discharged to the ground surface in accordance with the Third Runway project Storm Water Pollution Prevention Plan (Parametrix, 1999).

Water Level Measurement

Water levels were measured using a Solinst water level probe, graduated in 0.01-foot increments. Depth to water was measured below the top of casing and recorded to the nearest hundredth of a foot. Depth to water was converted to groundwater elevation using survey information for the top of casing in the wells. Depth to water data and groundwater elevations are summarized in Table 4.

References for Appendix A

Parametrix 1999. Seattle-Tacoma International Airport Third Runway Project Geotechnical Explorations Stormwater Pollution Prevention Plan, Prepared for Port of Seattle, January 29, 1999.

F:\docs\jobs\497821\WestMSEWall(rpt).doc

Key to Exploration Logs

Sample Description

Classification of soils in this report is based on visual field and laboratory observations which include density/consistency, moisture condition, grain size, and plasticity estimates and should not be construed to imply field nor laboratory testing unless presented herein. Visual-manual classification methods of ASTM D 2488 were used as an identification guide.

Soil descriptions consist of the following:

Density/consistency, moisture, color, minor constituents, MAJOR CONSTITUENT, additional remarks.

Density/Consistency

Soil density/consistency i Soil density/consistency in	n borings is related p test pits is estimated	primarily to the Standar I based on visual observa	d Penetration Resistance. Ition and is presented pare	enthetically on the test pit logs.
SAND or GRAVEL Density	Standard Penetration Resistance (N) in Blows/Foat	SILT or CLAY Consistency	Standard Penetration Resistance (N) in Blows/Foot	Approximate Shear Strength in TSF
Very loose	0 - 4	Very soft	0 - 2	<0.125
Loose	4 - 10	Soft	2 - 4	0.125 - 0.25
Medium dense	10 - 30	Medium stiff	4 - 8	0.25 - 0.5
Dense	30 + 50	Stiff	8 - 15	0.5 - 1.0
Very dense	>50	Very stiff	15 - 30	1.0 - 2.0
		Hard	>30	>2.0

Moisture

- Little perceptible moisture Dry
- Damp Some perceptible moisture, probably below optimum
- Moist Probably near optimum moisture content
- Much perceptible moisture, probably above optimum Wet

Legends

Sa	ampling Test Symbols
BO	RING SAMPLES
	Split Spoon
	Shelby Tube
Ш	Cuttings
] Core Run
*	No Sample Recovery
P TI	Tube Pushed, Not Driven EST PIT SAMPLES
	Grab (Jar)
	Bag
	Shelby Tube
G	roundwater Observations
	Z 7 Z 7



Minor Constituents

Minor Constituents	Estimated Percentage
Not identified in description	0 - 5
Slightly (clayey, silty, etc.)	5 - 12
Clayey, silty, sandy, gravelly	12 - 30
Very (clayey, silty, etc.)	30 - 50

Test Symbols

- GS Grain Size Classification
- CN Consolidation
- Unconsolidated Undrained Triaxial UU
- Consolidated Undrained Triaxial CU
- CD **Consolidated Drained Triaxial**
- Unconfined Compression QU
- DS Direct Shear
- к Permeability
- Pocket Penetrometer Approximate Compressive Strength in TSF PP
- τv Torvane Approximate Shear Strength in TSF
- CBR California Bearing Ratio
- MD Moisture Density Relationship
- Atterberg Limits AL
 - Water Content in Percent Le Liquid Limit
 - Natural Plastic Limit (NP=Non Plastic)
- PID Photoionization Detector Reading
- CA Chemical Analysis
- DT In Situ Density Test



Boring Log HC00-B106 N 17284 E 10878



STANDARD PENETRATION

LAB

- 2. Soil descriptions and stratum lines are interpretive
- and actual changes may be gradual. 3. Groundwater level, if indicated, is at time of drilling (ATD) or for date specified. Level may vary with time.

J-4978-21 2/00 Figure A-2

Boring Log HC00-B107 N 17398 E 10953



and actual changes may be gradual.
 Groundwater level, if indicated, is at time of drilling (ATD) or for date specified. Level may vary with time.

Figure A-3 AR 045286

Boring Log HC00-B108 N 17407 E 11067



AR 045287

HEM 2/28/0// 1=1 woodstock pc2 497821 LOGS
Boring Log HC00-B110 N 17422 E 10895



woodstack pc2

нЕм 2/28/0// 1=1 497821 LOGS

and actual changes may be gradual. 3. Groundwater level, if indicated, is at time of drilling (ATD) or for date specified. Level may vary with time.

AR 045288

2/00

J-4978-21

Boring Log HC00-B111 N 17617 E 11163



STANDARD PENETRATION

- 2. Soil descriptions and stratum lines are interpretive
- and actual changes may be gradual. 3. Groundwater level, if indicated, is at time of drilling (ATD) or for date specified. Level may vary with time.

J-4978-21 2/00 Figure A-6

woodstock pc2 HEM 2/28/0// 1=1 LOCS 497821

Boring Log HC00-B114 N 18122 E 10953



V

+45

+50

-55

 ± 60





1. Refer to Figure A-1 for explanation of descriptions and symbols.

- 2. Soil descriptions and stratum lines are interpretive and actual changes may be gradual.
- Groundwater level, if indicated, is at time of drilling (ATD) or for date specified. Level may vary with time.

HARTCROWSER J-4978-21 2/00 Figure A-7

N 18225

E 10990



and actual changes may be gradual.
Groundwater level, if indicated, is at time of drilling (ATD) or for date specified. Level may vary with time.

AR 045291

Figure A-8

woodstock pc2 HEM 2/28/0// 1=1 1065 497821

N 18291

E 10971



- 2. Soil descriptions and stratum lines are interpretive
- and actual changes may be gradual. 3. Groundwater level, if indicated, is at time of drilling (ATD) or for date specified. Level may vary with time.

J-4978-21 2/00 Figure A-9

pc2

N 17271

E 10931



STANDARD PENETRATION

- 2. Soil descriptions and stratum lines are interpretive
- and actual changes may be gradual. 3. Groundwater level, if indicated, is at time of drilling (ATD) or for date specified. Level may vary with time.

Figure A-10

AR 045293

woodstock pc2 нЕМ 2/28/0// 1=1 497821 LOGS

Boring Log HC00-B118 N 17456 E 10947



STANDARD PENETRATION

LAB

- and actual changes may be gradual.
- 3. Groundwater level, if indicated, is at time of drilling
- (ATD) or for date specified. Level may vary with time.

AR 045294

Figure A-11

woodstock pc2

Boring Log HC00-B124 N 18016 E 10939



and actual changes may be gradual. 3. Groundwater level, if indicated, is at time of drilling (ATD) or for date specified. Level may vary with time.

Figure A-12 AR 045295

HEM 2/28/0// 1=1 woodstock pc2 497821 LOGS

Boring Log HC00-B126 N 18232 E 11112



(ATD) or for date specified. Level may vary with time.

AR 045296

Figure A-13

woodstock HEM 2/28/0// 1=1 497821 LOCS

pc2

Boring Log HC00-B127 N 18215 E 10869



and actual changes may be gradual. 3. Groundwater level, if indicated, is at time of drilling (ATD) or for date specified. Leve: may vary with time.

woodstock pc2

нЕМ 2/28/0//1=1

497821 LOGS

Figure A-14

Boring Log HC00-B129 N 18256





woodstock pc2 HEM 2/28/0// 1=1

AR 045298

LOCS 497821

Boring Log HC00-B131 N 18329 E 10804



pc2 woodstock HEM 2/28/0// 1≖1 497821 LOCS

Boring Log HC00-B133 N 18471 E 10859



2. Soil descriptions and stratum lines are interpretive

woodstock pc2

HEM 2/28/0// 1=1 49/821 LOGS

and actual changes may be gradual.
 Groundwater level, if indicated, is at time of drilling (ATD) or for date specified. Level may vary with time.

J-4978-21 2/00 Figure A-17

Boring Log HC00-B134 N 18438 E 10953



and actual changes may be gradual. 3. Groundwater level, if indicated, is at time of drilling (ATD) or for date specified. Level may vary with time.

AR 045301

Figure A-18

woodstock pc2 LOCS 497821

HEW 2/28/0//1=1

Boring Log HC00-B139 N 18759 E 10889

Descriptions	Depth		RESISTANCE	LAB TEST
ox. Ground Surface Elevation in Feet: 255	in Feet	Sample	 Blows per Foot 	
	0	S_1 (TT)		00
Loose, to medium dense, wet, brown to gray, slightly gravelly, silty to very silty fine to medium SAND.				
	-5	s-2		– GS
		S-3		
Very dense, wet, gray, slightly gravelly to gravelly, silty SAND.				
5 / /	- 15	S-4 🔀		50/6
		S-5 🗷		50/6
Bottom of Boring at 19.5 Feet. Completed 2/15/00.	+20			
	-25			
	-30			
	-			
	- 35			
	_ 45			
	-50			
	- 55			
	⊥60		I I	00
Refer to Figure A-1 for explanation of de	scriptions			

Soil descriptions and stratum lines are interpretive and actual changes may be gradual.
 Groundwater level, if indicated, is at time of drilling (ATD) or for date specified. Level may vary with time.

AR 045302

J-4978-21 Figure A-19 1/00

woodstock pc2 HEM 2/28/0// 1=1 497821 LOGS

Boring Log HC00-B140 N 18498 E 10940

Descriptions	Depth	Samole	RESISTANCE	LAB TESTS
x. Ground Surface Elevation in Feet. 207	in Feet		▲ Blows per Foot 1 2 5 10 20 50 100	,
Loose to medium dense, wet, brown, slightly grovelly, silty to very silty SAN		*S-2		
	- 5 - -			
Manual final scale with brown motified	- 10	S-3		
gravelly, sandy SILT to very sitty SAND.	$-\frac{\nabla}{15}$	S-4 S-5	P-	- AL - PP: 1
Dense to very dense, wet, gray, graveliy, silty to very silty SAND.	 + 20	S-6		- GS
		s-74	- - - 50	/1
		5 9		
Bottom of Boring ct 29.3 Feet. Completed 2/14/00.	- 30	3-0		/ 4
	- 35			
	40			
	45			
	- 50			
	- 55			

- 1. Refer to Figure A-1 for explanation of descriptions and symbols.

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Soil descriptions and stratum lines are interpretive and actual changes may be gradual.
 Groundwater level, if indicated, is at time of drilling (ATD) or for date specified. Level may vary with time.

HARTCROWSER J-4978-21 1/00

Figure A-20

Boring Log HC00-B141 N 18597 E 10941

Descriptions Depties box. Ground Surface Elevation in Feet: 258 Depties of Casing Elevation in Feet: 258.64 C Loose (to dense), wet, brown to gray, silty, gravelly SAND with concrete debris. (FILL) C Stiff, wet, gray, slightly gravelly, sandy SILT with organic material. C Loose to medium dense, wet, gray with orange mottling, slightly gravelly, very silty SAND with trace organic material. 1		Sample G-1 S-1B S-2 S-3	RESIST A Blows 1 2 P P - - - - - - - - - - - - -	per Foot	•	50 10	00	
of Gasing Elevation in Feet: 258.64 C Loose (to dense), wet, brown to gray, silty, gravelly SAND with concrete debris. (FILL) C Stiff, wet, gray, slightly gravelly, sandy SILT with organic material. 5 Loose to medium dense, wet, gray with orange mottling, slightly gravelly, very silty SAND with trace organic material. 1		G-1 $S-1B$ $S-2$ $S-3$	1 2	5 10	20	50 10	00	
Loose (to dense), wet, brown to gray, silty, gravelly SAND with concrete debris. (FILL) Stiff, wet, gray, slightly gravelly, sandy SILT with organic material. Loose to medium dense, wet, gray with orange mottling, slightly gravelly, very silty SAND with trace organic material.		$\begin{array}{c} G-1 \\ S-1B \\ S-2 \\ S-3 \end{array}$			•			
Stiff, wet, gray, slightly gravelly, sandy 5 SILT with organic material. - Loose to medium dense, wet, gray with orange mottling, slightly gravelly, very silty SAND with trace organic material. - - -		S-1B S-2 S-3			-			
Loose to medium dense, wet, gray with orange mottling, slightly gravelly, very silty SAND with trace organic material.	10	s-3						
	F.H. 1							- GS
	15	s-4 🗙						
Very soft drilling noted.					\mathbf{X}			
Dense to very dense, wet to moist, gray, slightly gravelly, silty SAND.	20	S-5						
	25	S-6 🗙					50/6	
Bottom of Boring ot 29.3 Feet 3 Completed 1/28/00.	30 30	S-7 ≥					50/4	
	35							
	40							
	45							
	50							
	5 6							
	55							
-								
L - L 6	60	ł		5 10	20	50 10	00 L	
			■ Water	Content in	Percent	i W		
Refer to Figure A-1 for explanation of descriptio	ons						<u> </u>	

- Soil descriptions and stratum lines are interpretive and actual changes may be gradual.
 Groundwater level, if indicated, is at time of drilling (ATD) or for date specified. Level may vary with time.

AR 045304

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J-4978-21

N 19263

E 10890



- and actual changes may be gradual.
 Groundwater level, if indicated, is at time of drilling (ATD) or for date specified. Level may vary with time.

AR 045305

Boring Log HC00-B144 N 18792 E 10787

10707			STANDARD PENE	TRATION	LAB
Descriptions		Sample	RESISTANCE		TESTS
of Casing Elevation in Feet: 247 in	reet		- blows per root 1 2 5 10	20 50 100	
Loose to medium dense, dark brown to gray, slightly gravely, non-silty to silty SAND with trace organic material.	T ^o	S-1			
	-5	S-2			– GS
Very dense, wet, gray, sitty, slightly graveliy to very gravelly SAND.	10 ATD 11	S-3			
		S-4 🗙		50/5	5
Bottom of Boring at 14.4 Feet. Completed 2/15/00.	- 15				
	20				
	-				
	+25				
	+ 30				
	- 35				
	-				
	- 40 -				
	- 45				
	-				
	-50			<u></u>	
	-				
	- 55				
	- - -				
I	160				L
			 Water Content in 	Percent	
			• Water Content in	Percent	

- Soil descriptions and stratum lines are interpretive and actual changes may be gradual.
 Groundwater level, if indicated, is at time of drilling (ATD) or for date specified. Level may vary with time.

Figure A-23 AR 045306

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J-4978-21

woodstack pc2 HEM 2/28/0// 1=1 497821 LOGS

Boring Log HC00-B145 N 18964 E 10866



AR 045307

Boring Log HC00-B146 N 19242 E 10784



and actual changes may be gradual. 3. Groundwater level, if indicated, is at time of drilling (ATD) or for date specified. Level may vary with time.

pc2

woodstock

HEM 2/28/0// 1=1

LOGS

497821

AR 045308



Hand-Auger Boring Log HC00-A105



- 1. Refer to Figure A-1 for explanation of descriptions and symbols.
- Soil descriptions and stratum lines are interpretive and actual changes may be gradual.
 Groundwater conditions, if indicated, are at the time
- Groundwater conditions, if indicated, are at the time of excavation. Conditions may vary with time.

J-4978-21 3/00 Figure A-26

HARTCROWSER

N 17373

AR 045309

Pc2



Hand-Auger Boring Log HC00-A137



and actual changes may be gradual. 3. Groundwater conditions, if indicated, are at the time

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H_augers

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of excavation. Conditions may vary with time.

AR 045310

Figure A-27

N 18666

Hand-Auger Boring Log HC00-A143

N 18733 E 10621

Sample	Waler Content	Lab Tests	Depth in Feet A	SOIL DESCRIPTIONS LIVE TOOZT pproximate Ground Surface Elevation in Feet: 237
s-1 🛛	23			(Loose), wet, brown, slightly gravely, very silty SAND with trace organic material.
S-2	4 7		2 - 3 -	(Very soft), wet, brown, sandy, organic SILT with organic materici.
S-3	39	GS	4 5	(Loose), wet, brown, very sitty SAND with zones of sanay silt with organic material.
S-4	30		8 9 10	(Medium aense), wet, gray SAND.
			11	Bottom of Hand Auger at 11 Feet. Completed 2/14/00.

H...ougers woodslck pc2 497821 1=1 HEW 3/27/00

- Refer to Figure A-1 for explanation of descriptions and symbols.
 Soil descriptions and stratum lines are interpretive and actual changes may be gradual.
 Groundwater conditions, if indicated, are at the time of excavation. Conditions may vary with time.

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N 16784 Test Pit Log HC00-TP101 E 11109

Sample SOIL DESCRIPTIONS Water Depth in Feet Content Ground Surface Elevation in Feet: 356 Tests 0 S-1 X 19 1 2 S-2 S-3 ₩ 70 25 3 4 5 6 7 S-4 🔀 9 8 9 10 11-12 13 14 -15 16 17 18 19 20]

Lab

N 16778

(Loose), moist, brown, silty, gravely SAND with roots. (FILL) (Very loose), wet, black, silty, gravelly SAND with PEAT. (Medium dense), wet, gray and orange mottled, slightly gravelly, very silty SAND. (Dense to very dense), moist, gray, silty, gravely SAND. Note: Seepage from abandoned septic drain field encountered below 3 feet. Bottom of Test Pit at 15 Feet. Completed 1/25/00.



497821 testpits woodstck pc2 1=1 3/15/00

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- 1. Refer to Figure A-1 for explanation of descriptions and symbols.
- 2. Soil descriptions and stratum lines are interpretive and actual changes may be gradual. 3. Groundwater conditions, if indicated, are at the time
- of excavation. Conditions may vary with time.



N 17037

SOIL DESCRIPTIONS



Test Pit Log HC00-TP103



2. Soil descriptions and stratum lines are interpretive

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and actual changes may be gradual. 3. Groundwater conditions, if indicated, are at the time of excavation. Conditions may vary with time.

AR 045313

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J-4978-21

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N 17030 E 10874



Test Pit Log HC00-TP105





of excavation. Conditions may vary with time.

Sample	Water Content	Lab Tests	Depth in Feet	SOIL DESCRIPTIONS Ground Surface Elevation in Feet: 328
S-1	26			(Loose), moist, dark brown, slightly gravelly, silty SAND. (TOPSOIL)
s-2 X	16		2 -	(Loose), red-brown, moist, silty, gravelly SAND.
			3 -	(Medium dense), moist, gray-brown, silty, gravelly SAND.
s-3 🛛	13		4 - 5 - 6 - 7 -	(Dense to very dense), moist, gray, silty, gravelly SAND.
S-4 X	20	GS	8 - 9 - 10 - 11 - 12 - 13 - 14 -	(Dense), wet, gray, slightly gravelly SAND with silty Sand layers.
			16 - 17 - 18 - 19 - 20 -	Bottom of Test Pit at 15 Feet. Completed 1/26/00. Note: No seepage noted.

N 17151 E 10925

N 17415

Test Pit Log HC00-TP107



- 1. Refer to Figure A-1 for explanation of descriptions and symbols.
- 2. Soil descriptions and stratum lines are interpretive
- and actual changes may be gradual. 3. Groundwater conditions, if indicated, are at the time

of excavation. Conditions may vary with time.

HARTCROWSER J-4978-21 1/00 Figure A-32





Bottom of Test Pit at 15 Feet.

Note: Slight groundwater seepage noted at depth of 10% feet.

Completed 1/26/00.

3/9/00 i=1 497821 testpils woodstck pc2

¥ ₩ Refer to Figure A-1 for explanation of descriptions and symbols.
 Set descriptions and stratum lines are interpretive.

13 -14 -

15 -

16

17 -18 -

19 -20 -

- Soil descriptions and stratum lines are interpretive and actual changes may be gradual.
 Groundwater conditions, if indicated, are at the time
- Groundwater conditions, if indicated, are at the time of excavation. Conditions may vary with time.

HARTCROWSER J-4978-21 1/00 Figure A-33



N 18325



Test Pit Log HC00-TP115



1. Refer to Figure A-1 for explanation of descriptions and symbols.

- 2. Soil descriptions and stratum lines are interpretive and actual changes may be gradual. 3. Groundwater conditions, if indicated, are at the time
- of excavation. Conditions may vary with time.



AR 045317

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Depth SOIL DESCRIPTIONS in Feet Approximate Ground Surface Elevation in Feet: 257 SOIL DESCRIPTIONS Sample Water l ab Tests Content 0 (Loose to medium dense), moist, gray and brown mottled, S-1 14 1 non-silty to silty SAND. 2 (Medium dense), moist, gray, SAND with slightly silty zones. 3 S-2 GS 6 4 (Dense), moist, gray, fine to medium SAND. 5 6 7 8 9 10 11 (Dense) wet, gray, slightly gravelly SAND. Ŷ 12 13 Becomes gravelly. 14 s-3 🛛 19 15 Bottom of Test Pit at 15 Feet. Completed 1/26/00. 16 Note: Slight groundwater seepage noted at a depth of 11% feet. 17 18 19 20

Test Pit Log HC00-TP117





- 1. Refer to Figure A-1 for explanation of descriptions and symbols.
- 2. Soil descriptions and stratum lines are interpretive
- and actual changes may be gradual. 3. Groundwater conditions, if indicated, are at the time of excavation. Conditions may vary with time.

HARTCROWSER J-4978-21 1/00 Figure A-35

N 18412 E 10798

N 18529

Somple	Water Content	Lob Tests	Depth in Feet Gr	SOIL DESCRIPTIONS ound Surface Elevation in Feet: 236
S-1 🖂	30		.7 F	(Loose), wet, dark brown, silty SAND with trace organic material.
S-2	27		2 - 3 - 9	(Medium dense), wet, brown to gray, slightly silty SAND with trace organic material.
S-3 🔀	13	GS	4 - 5	(Dense), wet, gray, slightly gravelly to gravelly, non-silty to very silty SAND.
S-4	15		10 - 11 - 12 - 13 - 14 -	(Dense), wet, gray, slightly silty to silty, very grovely SAND.
			15 - 16 - 17 - 18 - 19 - 20 -	Bottom of Test Pit at 15 Feet. Completed 1/26/00. Note: Slight groundwater seepage noted at a depth of 3 feet.

Test Pit Log HC00-TP119



1. Refer to Figure A-1 for explanation of descriptions and symbols.

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- 2. Soil descriptions and stratum lines are interpretive
- and actual changes may be gradual.3. Groundwater conditions, if indicated, are at the time of excavation. Conditions may vary with time.

HARTCROWSER 1/00 J-4978-21 Figure A-36



2. Soil descriptions and stratum lines are interpretive

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- and actual changes may be gradual. 3. Groundwater conditions, if indicated, are at the time
- Groundwater conditions, if indicated, are at the time of excavation. Conditions may vary with time.

AR 045320

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J-4978-21

N 19126 E 10873

N 18973



Test Pit Log HC00-TP124



 Soil descriptions and stratum lines are interpretive and actual changes may be gradual.

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and actual changes may be gradual. 3. Groundwater conditions, if indicated, are at the time of excavation. Conditions may vary with time.

AR 045321



N 19443 E 10773



Test Pit Log HC00-TP126

SOIL DESCRIPTIONS Depth Sample Water Lab Approximate Ground Surface Elevation in Feet: 272 in Feet Content Tests 0 (Loose), wet, brown, silty SAND with some roots and trace S-1 🖂 26 1 organic material. 20 S-2 🖂 (Medium dense), wet, gray with orange mottling, silty, gravely 2 SAND 3 4 5 6 7 8 (Very dense), moist, gray, silty, gravely SAND. S-3 🖾 8 9 10 11 -Bottom of Test Pit at 11 Feet. 12 Completed 1/28/00. 13 -14 15 Note: Septic drainfield encountered at 3 feet. 16 17 18 19 20] 1. Refer to Figure A-1 for explanation of descriptions HARTCROWSER and symbols. 1/00 2. Soil descriptions and stratum lines are interpretive J-4978-21 and actual changes may be gradual. 3. Groundwater conditions, if indicated, are at the time Figure A-39

of excavation. Conditions may vary with time.

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Test Pit Log HC00-TP128



of excavation. Conditions may vary with time.

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Test Pit Log HC00-TP129

N 18899 E 10623

Sample	Water Content	Lab Tests	Depth in Feet	SOL DESCRIPTIONS Approximate Ground Surface Elevation in Feet: 250
S-1	28			(Laose), moist, brown, very silty SAND with trace organic materia
S-2 ⊠	22	GS	2- 3-	(Medium dense), wet, gray, very sandy SILT.
S−3 🛛	16		4- 5-	(Stiff), wet, gray and orange mottled, sandy SILT.
			6- 7-	(Dense), moist, gray and orange mottled, silty, gravelly SAND.
			8- 9-	
			10-	
			12-	
			13- 14-	
			15- 16-	Bottom of Test Pit at 15 Feet. Completed 1/28/00.
			17- 18-	
			19- 20-	

- 1. Refer to Figure A-1 for explanation of descriptions
- Refer to right A=1 for exploration of descriptions and symbols.
 Soil descriptions and stratum lines are interpretive and actual changes may be gradual.
 Groundwater conditions, if indicated, are at the time of excavation. Conditions may vary with time.



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APPENDIX B LABORATORY TESTING PROGRAM

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APPENDIX B LABORATORY TESTING PROGRAM

A laboratory testing program was performed for this study to evaluate the basic index and geotechnical engineering properties of the site soils. Disturbed and relatively undisturbed samples were tested. The tests performed and the procedures followed are outlined below.

Soil Classification

Field Observation and Laboratory Analysis. Soil samples from the explorations were visually classified in the field and then taken to our laboratory where the classifications were verified in a relatively controlled laboratory environment. Field and laboratory observations include density/consistency, moisture condition, and grain size and plasticity estimates.

The classifications of selected samples were checked by laboratory tests such as Atterberg limits determinations and grain size analyses. Classifications were made in general accordance with the Unified Soil Classification (USC) System, ASTM D 2487, as presented on Figure B-1.

Note that the term "trace" used on exploration logs generally indicate a material within the soil matrix that constitutes a relatively small fraction by weight of the total soil. The usage of this term in not associated with the ASTM simplified classification procedure.

Water Content Determinations

Water contents were determined for most samples recovered in the explorations in general accordance with ASTM D 2216, as soon as possible following their arrival in our laboratory. The results of these tests are plotted or recorded at the respective sample depth on the exploration logs. In addition, water contents are routinely determined for samples subjected to other testing. These are also presented on the exploration logs.

Grain Size Analysis (GS)

Grain size distribution was analyzed on representative samples in general accordance with ASTM D 422. Wet sieve analysis was used to determine the size distribution greater than the U.S. No. 200 mesh sieve. The size distribution for particles smaller than the No. 200 mesh sieve was determined by the hydrometer method for selected samples. The results of the tests are presented

Page B-1

as curves on Figures B-2 through B-22 plotting percent finer by weight versus sieve size.

Atterberg Limits (AL)

We determined Atterberg limits for selected fine-grained soil samples. The liquid limit and plastic limit were determined in general accordance with ASTM D 4318-84. The results of the Atterberg Limits analyses and the plasticity characteristics are summarized in the Liquid and Plastic Limits Test Report, Figures B-23 through B-29. This relates the plasticity index (liquid limit minus the plastic limit) to the liquid limit. The results of the Atterberg limits tests are also shown graphically on the boring logs.

Consolidation Test (CN)

The one-dimensional consolidation test provides data for estimating settlement and preconsolidation pressure. The test was performed in general accordance with ASTM D 2435. A relatively undisturbed, fine-grained sample was carefully trimmed and fit into a rigid ring with porous stones placed on the top and bottom of the sample to allow drainage. Vertical loads were then applied incrementally to the sample in such a way that the sample was allowed to consolidate under each load increment. Measurements were made of the compression of the sample (with time) under each load increment. Rebound was measured during the unloading phase. In general, each load was left in place until the completion of 100 percent primary consolidation, as computed using Taylor's square root of time method. The next load increment was applied soon after attaining 100 percent primary consolidation. For the 4 tsf load increment, the load was left in-place for about 16 hours to record secondary compression characteristics. The test results plotted in terms of axial strain and coefficient of consolidation versus applied load (stress) are presented on Figures B-30 through B-36.

Consolidated Undrained Triaxial Compression Test (CU)

The consolidated undrained triaxial compression test with pore pressure measurements estimates the effective strength of the soil at various stress levels. The test was performed in general accordance with ASTM D 4767.

A relatively undisturbed fine-grained sample was trimmed to a length of about 6 inches, encased in a rubber membrane, and placed in the triaxial cell. With the sample in the triaxial test cell, an all-around pressure was applied hydraulically. The sample was allowed to consolidate under the applied pressure with drainage occurring through porous stones and slotted filter paper placed around the

Page B-2

sample. When consolidation was completed, drainage lines from the sample were closed, a back pressure was applied to saturate the sample, and the sample was loaded to failure under undrained conditions by application of increasing axial load at a constant strain rate.

During loading, we recorded the magnitude of excess pore water pressure developed. From the data, an effective stress plot was developed to illustrate the variation in effective shear strength with varying consolidation (or overburden) pressures. The data are plotted using shear stress versus principal stress as Mohr's circles. The tangent to the Mohr's circles for a test series represents the effective angle of internal friction (ϕ '). The intercept along the vertical axis is the effective cohesion (c').

Test results for the samples tested are presented on Figures B-37 through B-40. For each sample the first figure presents shear stress and normal stress data in a Mohr's circle format along with stress-strain plots, while the second figure in the set presents the stress-stain data and a stress path plot. The effective friction angles (ϕ') provided in Table 2 of the main text were determined by assuming that c' = 0 for drained conditions.

Unconsolidated Undrained Triaxial Compression Test (UU)

The unconsolidated undrained triaxial compression test estimates the total strength of the soil at various stress levels. The test was performed in general accordance with ASTM D 2850. A relatively undisturbed fine-grained sample was trimmed to a length of about 6 inches, encased in a rubber membrane, and placed in the triaxial cell. With the sample in the triaxial test cell, an all-around pressure was applied hydraulically, although the drainage valves remained closed. Thus the sample was not allowed to consolidate. The sample was loaded to failure under undrained conditions by application of increasing axial load at a constant strain rate.

The data are plotted (Figures B-41 through B-44) using shear stress versus principal stress as Mohr's circles. Because the test is a measure of the total stress strength of a soil, the tangent to the Mohr's circle for a test extends horizontally to the vertical axis in a straight line. The intercept along the vertical axis is the cohesion (c = undrained shear strength, τ , of the soil).

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Unified Soil Classification (USC) System

Soil Grain Size

Γ	Size of Opening In Inches				Number of Mesh per Inch (US Standard)							Grain Size in Millimetres									
12			4	<u>بر</u> ک	v ,	3/4	1/4	3/8	4		5	50	40	60	<u>10</u>	90 50	8	8	8	01 006 003 002	8
_			T								1	i		- T			11				
i	· · ·	i i	L I	11		1	TT	TIT	11	1	1			1 1							
8	8	8	8 8	8 9	8	8	9	æ ¢	, ,	r m	N	- eç (o 4	e c)	- 10 10 10 10	0	8	.02	00 000 003 003 003	8
e)		•										Grain Size	in Millir	netres							
COBBLES		BLES GRAVEL					1	SAND							SILT and CLAY						
T			J			<u></u>	Coa	arse-	Grai	ned S	oils								F	ine-Grained Soils	

Coarse-Grained Soils

GW	GP	GM GC		SW	SP	SM	SC			
Clean GRAVEL <5% fines		GRAVEL with	h >12% fines	Clean SAND) <5% fines	SAND with >12% fines				
GRA	VEL >50% coarse	fraction larger than	n No. 4	SAND >50% coarse fraction smaller than No. 4						
		Coarse-	Grained Soils >50	% larger than No. 20	00 sieve					

G W and S W
$$\left(\frac{D_{60}}{D_{10}}\right) > 4$$
 for G W & $1 \le \left(\frac{(D_{30})^2}{D_{10} \times D_{60}}\right) \le 3$

G P and S P Clean GRAVEL or SAND not meeting requirements for G W and S W

G M and S M Atterberg limits below A line with PI <4

G C and S C Atterberg limits above A Line with PI >7

* Coarse-grained soils with percentage of fines between 5 and 12 are considered borderline cases required use of dual symbols.

D₁₀, D₃₀, and D₆₀ are the particles diameter of which 10, 30, and 60 percent, respectively, of the soil weight are finer.

Fine-Grained Soils

















AR 045336



AR 045337

















AR 045345





AR 045347





AR 045349



LIQUID AND PLASTIC LIMITS TEST REPORT											
Dashed line indicates the approximupper limit boundary for natural sc	mate bils			04							
	, / /		C	Aor							
▲ ML or O	L		Mł	l or OH							
10 30 50 70 90 110 LIQUID LIMIT											
Location + Description	LL	. PL	PI	-200	USCS						
• Source: HC00-B107 Sample No.: S-3 Very sandy, lean CLAY	27	15	12	53.2	CL						
 Source: HC00-B110 Sample No.: S-4 Slightly sandy CLAY-SILT 	19	15	4	89.7	CL-ML						
▲ Source: HC00-B110 Sample No.: S-11 Very clayey SILT	41	28	13	98.4	ML						
Source: HC00-B111 Sample No.: S-3 Clayey SILT	30	26	4	97.6	ML						
 Source: HC00-B111 Sample No.: S-6 Slightly clayey, gravelly, very silty, medium to fine SAND 	18	15	3	46.3	SM						
Remarks: • Project: Third Runway Westside											
■ ▲ ◆	Client: HN	TB									
▼	Location:										
	HAR	TCROM	VSER	J4978- Figure	21 3/10/2000 No. B-23						






































AR 045370





AR 045372

APPENDIX C ADDITIONAL EXPLORATIONS AND LABORATORY TESTS



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Key to Exploration Logs

Sample Description

Classification of soils in this report is based on visual field and laboratory asservations which include aensity/consistency, moisture condition, grain size, and plasticity estimates and should not be construed to imply field nor laboratory testing unless presented herein. Visual-manual classification methods of ASTM D 2488 were used as an identification guide.

Soil descriptions consist of the following:

Density/consistency, moisture, color, minor constituents, MAJOR CONSTITUENT, additional remarks.

Density/Consistency

Soil density/consistency in borings is related primarily to the Standard Penetration Resistance.Soil density/consistency in test pits is estimated based on visual observation and is presented parenthetically on the test pit logs.SaND or GRAVELStandardStandardSILT or CLAYResistance (N)Strength

Density	in Blows/Foot	Consistency	in Blows/Foot	in TSF	
Very loose	0 - 4	Very soft	0 - 2	<0.125	
Loose	4 - 10	Soft	2 - 4	0.125 - 0.25	
Medium dense	10 - 30	Medium stiff	4 - 8	0.25 - 0.5	
Dense	30 - 50	Stiff	8 - 15	0.5 - 1.0	
Very dense	>50	Very stiff	15 - 30	1.0 - 2.0	
		Hard	>30	>2.0	

Moisture

Dry Little perceptable moisture

Damp Some perceptable moisture, probably below optimum

- Moist Probably near optimum maisture content
- Wet Much perceptable moisture, probably above optimum

Legends





Test Symbols

GS	Grain	Size	Classification

Minor Constituents

Not identified in description

Slightly (clayey, silty, etc.)

Clayey, silty, sondy, gravelly

Very (clayey, silty, etc.)

- CN Consolidation
- TUU Unconsolidated Undrained Triaxial
- TCU Consolidated Undrained Triaxial
- TCD Consolidated Drained Triaxial
- QU QU
- DS Direct Shear
- K Permeability
- PP Pocket Penetrometer Approximate Compressive Strength in TSF
- TV Torvane Approximate Shear Strength in TSF
- CBR California Bearing Ratio
- MD Moisture Density Relationship

AL Atterberg Limits



- Liquid Limit
- ----- Plastic Limit
- PID Photoionization Reading
- CA Chemical Analysis



Estimated Percentage

0 - 5

5 - 12

12 - 30

30 - 50

Boring Log HC00-B113 N 17607 E 10945

Soil Descriptions	Depth	Sample	RESISTANCE	TESTS
Approx. Ground Surface Elevation in Feet: 283	in Feet	300.010	▲ Blows per Foot	100
(Loose), moist, brown, slightly grovelly, non-silty to silty, fine to medium SAND.] F°	G-1		
Very stiff, wet, brown and gray, sandy SILT.		S-2		~ AL
Medium dense, wet, brown, silty, fine to medium SAND with slightly silty SAND and sandy SILT layers.	- 10	s-3 🗙		
Stiff, wet, brown with orange mattling SILT.	 - 15 	S-4 S-5	P	
Medium dense to very dense, moist, gray—brown, slightly gravelly to gravelly, silty to very silty SAND.		S-6 🗙		50/5
Hord, moist, gray SILT layered with	25	s-7 🗙		
	- 30	S-8 🗙		
Bottom of Boring at 34.5 Feet. Completed 3/23/00.	35	S-9 🗙		
	40			
- C- LOGS	- - 45			
CHARLE - 6: PC2 A	- 50			
1 I=1 00/cf/				
	⊥ ₆₀		1 2 5 10 20 50 • Water Content in Percent	100
			====	

STANDARD PENETRATION

LAB

- 1. Refer to Figure C-1 for explanation of descriptions and symbols.
- 2. Soil descriptions and stratum lines are interpretive
- and actual changes may be gradual. 3. Ground water level, if indicated, is at time of drilling (ATD) or for date specified. Level may vary with time.

HARTCROWSER J-4978-21 3/00 Figure C-2

Boring Log HC00-B119 N 17560 E 10894



and actual changes may be gradual. 3. Ground water level, if indicated, is at time of drilling (ATD) or for date specified. Level may vary with time. 4. Shelby tube samples S-1A and S2A pushed in adjacent boring HC00-B119A.

5. No groundwater noted at time of drilling.

AR 045377

J-4978-21

Figure C-3

HARTCROWSER

3/00

LAB

STANDARD PENETRATION

Boring Log HC00-B120 N 17834 E 10964



2. Soil descriptions and stratum lines are interpretive

and actual changes may be gradual. 3. Ground water level, if indicated, is at time of drilling (ATD) or for date specified. Level may vary with time. 4. No groundwater noted at time of drilling.

J-4978-21 3/00 Figure C-4

HARTCROWSER

Boring Log HC00-B121 N 17881 E 10968



1. Refer to Figure A-1 for explanation of descriptions and symbols.

- 2. Soil descriptions and stratum lines are interpretive
- and actual changes may be gradual. 3. Ground water level, if indicated, is at time of drilling (ATD) or for date specified. Level may vary with time.

3/00 J-4978-21 Figure C-5

HARTCROWSER

Boring Log HC00-B122 N 17840 E 11087



- 1. Refer to Figure C-1 for explanation of descriptions and symbols.
- 2. Soil descriptions and stratum lines are interpretive
- and actual changes may be gradual. 3. Ground water level, if indicated, is at time of drilling (ATD) or for date specified. Level may vary with time.

AR 045380

3/00

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J-4978-21

Figure C-6

Boring Log HC00-B123

N 17958

E 11114

Approx. Ground Surface Elevation in Feet: 235 in Feet: Top of Casing Elevation in Feet: 237.64 (Soft). wet, dark brown, sandy SILT	∇ $G-1$
(Soft). wet, dork brown, sandy SILT with organics (PEAT). V Loose, wet, brown, very silty, fine to medium SAND with sandy SILT layers. ATO Soft to medium stiff, wet, brown to groy, sandy SILT with interbedded layers of peat, sand and silty sand. 5 Medium stiff, wet, gray and brown, slightly sandy PEAT with very silty SAND layers. 10 Medium stiff, wet, gray, and brown, slightly sandy PEAT with very silty SAND layers. 10 Dense, wet, gray, slightly gravelly SAND with sandy SILT layers. 15 Dense, wet, gray, slightly gravelly, very silty SAND. 20 Stiff, wet, gray, sandy CLAY. 25 Very dense, moist, gray, slightly silty to silty, gravelly SAND. 30 Bottom of Boring at 34.5 Feet. Completed 3/22/00. 35 40 45	∇ $G-1$ $G-1$ $S-2$ $S-3$
Loose, wet, brown, very silty, fine to medium SAND with sandy SILT loyers. Soft to medium stiff, wet, brown to gray, sandy SILT with interbedded loyers of peat, sand and silty sand. Medium stiff, wet, gray and brown, slightly sandy PEAT with very silty SAND layers. Medium dense, wet, gray, silty, gravelly SAND with sandy SILT loyers. 15 Dense, wet, gray, slightly gravelly, very silty SAND. 20 Stiff, wet, gray, sandy CLAY. Very dense, moist, gray, slightly silty to silty, gravelly SAND. Bottom of Boring at 34.5 Feet. Completed 3/22/00. 40	ATD S-2 X - •
Soft to medium stiff, wet, brown to gray, sandy SILT with interbedded layers of peat, sand and silty sand. Medium stiff, wet, gray and brown, slightly sandy PEAT with very silty SAND layers. Medium dense, wet, gray, silty, gravelly SAND with sandy SILT layers. Dense, wet, gray, slightly gravelly, very silty SAND. Stiff, wet, gray, sondy CLAY. Very dense, moist, gray, slightly silty to silty, gravelly SAND. Bottom of Boring at 34.5 Feet. Completed 3/22/00. Grad Additional Street S	P [P] S = 3 [X] [= + - + - + - + + + + + + +
Medium stiff, wet, gray and brown, slightly sandy PEAT with very slity SAND layers. 10 Medium dense, wet, gray, slity, gravelly SAND with sandy SILT layers. 15 Dense, wet, gray, slightly gravelly, very slity SAND. 20 Stiff, wet, gray, sandy CLAY. 20 Stiff, wet, gray, sandy CLAY. 25 Very dense, moist, gray, slightly silty to silty, gravelly SAND. 30 Battom of Boring at 34.5 Feet. 35 Completed 3/22/00. 40 45 50	
Medium dense, wet, gray, silty, gravelly SAND with sondy SILT layers. 15 Dense, wet, gray, slightly gravelly, very silty SAND. 20 Stiff, wet, gray, sandy CLAY. 21 Very dense, moist, gray, slightly silty to silty, gravelly SAND. Bottom of Boring at 34.5 Feet. Completed 3/22/00. 40 45 50	S-5 S-5
Dense, wet, gray, slightly gravelly, very silty SAND. 20 Stiff, wet, gray, sandy CLAY. 25 Very dense, moist, gray, slightly silty to silty, gravelly SAND. Bottom of Boring at 34.5 Feet. Completed 3/22/00. 40 45	S-6 S-7
Stiff, wet, gray, sandy CLAY. 25 Very dense, moist, gray, slightly silty to silty, gravelly SAND. Bottom of Boring at 34.5 Feet. Completed 3/22/00. 40 45 50	S-8 - GS
Very dense, moist, gray, slightly silty to silty, gravelly SAND. Bottom of Boring at 34.5 Feet. Completed 3/22/00. 40 45	
Very dense, moist, gray, slightly silty to silty, gravelly SAND. Bottom of Boring at 34.5 Feet. Completed 3/22/00. 40 45	S-9 S-10
Bottom of Boring at 34.5 Feet. Completed 3/22/00. 40 45 	S-11 S - 50/6
	• 50/6
730	
731 9 	
v +50	
→ 	
0 6/15/00	
°I I⊥60	<u>L </u>

- Refer to Figure C-1 for explanation of descriptions and symbols.
 Soil descriptions and stratum lines are interpretive and actual changes may be gradual.
 Ground water level, if indicated, is at time of drilling (ATD) or for date specified. Level may vary with time.

HARTCROWSER J-4978-21 3/00 Figure C-7

Boring Log HC00-B125 N 17686 E 10916



 Soli descriptions and stratum lines are interpretive and actual changes may be gradual.
 Ground water level, if indicated, is at time of drilling

 Ground water level, it indicated, is at time of driving (ATD) or for date specified. Level may vary with time.
 Shelby tube samples S-1A from adjacent boring HC00-B125A.

5. No groundwater noted at time of driving.

AR 045382

3/00

HARTCROWSER

J-4978-21

Figure C-8

Boring Log HC00-B128 N 17786 E 10918



- 1. Refer to Figure C-1 for explanation of descriptions and symbols.
- 2. Soil déscriptions and stratum lines are interpretive and actual changes may be gradual. 3. Ground water level, if indicated, is at time of drilling
- (ATD) or for date specified. Lever may vary with time.

3/00 J-4978-21 Figure C-9

HARTCROWSER

Boring Log HC00-B130 N 17901 E 10839



- 1. Refer to Figure C-1 for explanation of descriptions and symbols.
- 2. Soil descriptions and stratum lines are interpretive and actual changes may be gradual. 3. Ground water level, if indicated, is at time of drilling
- (ATD) or for date specified. Level may vary with time.

HARTCROWSER J-4978-21 3/00 Figure C-10

Boring Log HC00-B132 N 17914 E 10924



STANDARD PENETRATION

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4. Shelby tube samples S=1A from adjacent boring HC00-B132A.

AR 045385

Figure C-11

Test Pit Log HC00-TP110





Test Pit Log HC00-TP111

N 17585 E 11003



and actual changes may be gradual. 3. Groundwater conditions, if indicated, are at the time

of excavation. Conditions may vary with time.

AR 045386

Figure C-12

APPX-C-LOGS

Test Pit Log HC00-TP112



Sample	Water Content	Lab Tests	Depth in Feet	SOIL DESCRIPTIONS Approximate Ground Surface Elevation in ????
S-1	14		0- 1- 2- 3- 4-	(Loose), wet. brown, silty, gravelly SAND with trace organic material. (FILL and TOPSOIL)
S-2 🗵	14	GS	5 6 7 8 9	(Dense), wet. gray with brown mottling, non-gravelly to slightly gravelly, silty to very silty, fine to medium SAND. Grades to gravelly.
S-3 🔀	11		10- 11- 12- 13- 14-	(Very dense), moist, gray with orange mottling, silty, gravelly SAND.
			15- 16- 17- 18- 19- 20-	Bottom of Test Pit at 15 Feet. Completed 3/15/00. Note: Septic drain field seepage from a depth of 4 feet. Groundwater seepage noted at a depth of 7-1/2 feet.

- 1. Refer to Figure C-1 for explanation of descriptions and symbols. 2. Soil descriptions and stratum lines are interpretive
- and actual changes may be gradual. 3. Groundwater conditions, if indicated, are at the time of excavation. Conditions may vary with time.



Unified Soil Classification (USC) System

Soil Grain Size

		Size	of C	Openi	ng Ir	n Inches						Number of Mi US Sta	esh pe ndard)	r Inch					Grai	n Size in N	Ana⊓	netre	s		
12 [[]	9	₹		N +>C		3/4 5/8 1/2	1/4	3/в	4		10	20	40	60	100	200 06	04	63	05	01	900	004	003	005	6
[÷					:			1					I		:		-		
ğ	8	<u>8</u> 8	69	40	30	20	0	α c	٩	n n	C I	ب <u>ب</u> ح	4	ς Ω		~ 8 S	8	8	02	008	900	004	003	002	100
	ία.	÷										Grain Size in	n Millin	netres								,			
[COBBL	ES j			G	RAVEL						SAN	D							SILT and (CLA	Y			
							Coa	arse-	Grair	ned S	Soils								Fi	ine-Graine	d Se	oils			

Coarse-Grained Soils

GW	GP	GM	GC	SW	SP	SM SC				
Clean GRAV	EL <5% fines	GRAVEL with	n >12% fines	Clean SANI	D <5% fines	* SAND with >12% fines				
GRA	VEL >50% coarse	fraction larger than	No. 4	SAND >50% coarse fraction smaller than No. 4						
		Coarse-	Grained Soils >50	% larger than No. 2	200 sieve					

G W and S W $\left(\frac{D_{60}}{D_{10}}\right) > 4$ for G W $4 \le \left(\frac{(D_{30})^{-}}{D_{10} \times D_{60}}\right) \le 3$

I < 3</th>G P and S PClean GRAVEL or SAND not meeting
requirements for G W and S WPl < 4</td>G C and S CAtterberg limits above A Line with Pl > 7

G M and S M Atterberg limits below A line with PI <4

* Coarse-grained soils with percentage of fines between 5 and 12 are considered borderline cases required use of dual symbols.

D₁₀, D₃₀, and D₆₀ are the particles diameter of which 10, 30, and 60 percent, respectively, of the soil weight are finer.

Fine-Grained Soils













AR 045393














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