Subsurface Conditions Data Report 404 Permit Support Third Runway Embankment



Prepared for HNTB Corporation and The Port of Seattle

July 1999 J-4978-06

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SUBSURFACE CONDITIONS DATA REPORT 404 PERMIT SUPPORT THIRD RUNWAY EMBANKMENT

INTRODUCTION

This data report presents a discussion of subsurface conditions, laboratory testing, and relevant geotechnical and hydrogeologic field testing to support the 404 Permit process for the Third Runway Project. The site is located at the Sea-Tac International Airport, in SeaTac, Washington (refer to Figure 1, Vicinity Map). Figure 1 shows specific areas within the airport vicinity where we have performed explorations for this study. These areas are presented as site and exploration plans, Figures 2 and 3. Cross sections showing inferred geologic conditions are provided on Figures 4 through 6. Finally, a groundwater elevation contour map for the Regional Shallow Aquifer is shown on Figure 7.

This report provides the data used in engineering analyses which will be presented in other reports. We have organized this report into several sections. The main text starts with a discussion of site surficial geology and subsurface conditions. This is followed by a discussion of the hydrogeologic conditions and testing information we have obtained from our explorations to date. Appendices A and B follow the main text and present results of our subsurface explorations and laboratory testing, respectively.

PURPOSE AND SCOPE

This report provides information on subsurface soil and groundwater conditions for the planned Third Runway within the areas represented by our explorations. This documents addresses scope item Task 2.3, "Characterization of Subsurface Conditions" discussed in our proposal dated January 28, 1999. Additional information on subsurface conditions will be obtained to support completion of design. Tasks 2.1, "Subsurface Explorations," and 2.2 "Laboratory Soils Testing," also part of the January proposal, were completed to provide information for this report.

GENERALIZED GEOLOGIC DESCRIPTION AND SUBSURFACE SOIL CONDITIONS

This section provides a description of the geologic and subsurface soil conditions within the areas shown on Figures 2 and 3 based on our recent explorations at the site and explorations by others. Previous studies into the

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local geologic conditions at the Third Runway have been accomplished by AGI Technologies (AGI, 1998 and 1996) and CivilTech (1997).

Generalized Geologic Conditions

The site is located on the Des Moines Drift Plain in the Puget Sound Lowland. Glacial soils have been deposited and extensively reworked by glacial episodes, the most recent being the Vashon glaciation. This section presents the geologic conditions within the study areas shown on Figures 2 and 3.

In summary, the following geologic units have been identified at the Third Runway project site:

- Fill (loose to medium dense, locally dense, variably graded, silt, sand, and gravel);
- Alluvium (primarily soft to stiff peat and silt; and very loose to medium dense, fine to medium sand);
- Recessional Outwash (primarily medium dense to dense, silty, sand and gravel, and/or medium stiff to hard, sandy silt and/or sandy clay);
- Glacial Till (dense to very dense, silty sand and gravel);
- Advance Outwash (dense to very dense, non-silty to silty sand and gravel); and,
- Lawton Clay (very stiff to hard silt and clay).

The area immediately adjacent to the western side of the existing runway embankment has been mapped as glacial till. This has been reported to occur as a band of material paralleling the existing runway (AGI, 1996). Our explorations adjacent to the existing runway embankment suggest that recessional outwash deposits are the predominant surficial material with glacial till typically at a relatively shallow depth. The glacial till appears to outcrop in small areas within recessional outwash.

Subsurface Conditions

Subsurface soil conditions interpreted from materials encountered in explorations at the site and soil properties inferred from laboratory tests formed the basis for the information contained within this report. Variations between explorations are pronounced due to the variability in gradation, moisture

content, and density/consistency of soils at the site. The nature and extent of these variations may not become evident until construction. If variations become evident, it will be necessary to re-evaluate our interpretation of the soil conditions at the site, as well as any recommendations based on those interpretations.

Subsurface conditions in the north area shown on Figure 2, generally consists of a glacial sequence (recessional outwash sands over glacial till over silty advance outwash), and in low-lying areas, an alluvial sequence over glacial materials (alluvial silt, sand, and peat over glacial till). Subsurface conditions encountered on the west side were very similar. Figures 4 through 6 provide generalized geologic cross sections through the north end and west side of the proposed embankment. Each area has two associated sections, one cross section taken perpendicular to the wall/embankment, and one profile along the alignment of the proposed retaining wall. Detailed descriptions of the materials we encountered are provided below.

The following descriptions have been separated into categories entitled "Shallow Soils" and "Deeper Soils."

- Shallow soils are those that would be encountered during construction excavations into surficial soils for base preparations purposes.
- Deeper soils are considered the dense to very dense or hard, glacially overridden soils.

The latter are materials that will provide foundation support for the embankment fill and retaining wall sections without need for modification.

Shallow Soils

Topsoil. This soil was not consistently encountered in our explorations. Typically, this soil consists of a loose mixture of silt and sand with roots and other organic material. Topsoil is generally 1/2 to 1 foot thick where encountered. Many of the surficial soils at the site appear to be glacial soils at different stages of weathering. This is further discussed in the **Recessional Outwash** and **Glacial Till** sections below.

Fill Soils. Fill soils were encountered in both the north and west study areas, typically associated with access roads, paved streets, or general grading activities. Fill is generally absent in the low-lying portions of the site, adjacent to wetlands. Fill soils are generally loose to medium dense, variable mixture of silt, sand, and gravel. The density and granular nature of the fill materials resembles

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the recessional outwash deposits and the fill is sometimes difficult to distinguish from the outwash.

North of the runway safety area, fill thickness is generally up to about 8 feet and is primarily associated with roads and grading for residential development (refer to Figure 1). Fill was also encountered in some of the 1999 test pits (i.e., HC99-TP10 to HC99-TP21) performed on the western side of the north safety area. This material was up to 3 feet in thickness and contained brick fragments, concrete pieces, wood, and other miscellaneous debris.

Within the west study area, fill was encountered near the existing runway embankment in the area of the Hart Crowser 1998 and 1999 test pits (i.e., HC98-TP1 to HC98-TP12 and HC99-TP1 to HC99-TP21).

Alluvial Deposits. These soils occur in the low-lying areas and generally consist of soft/loose, moist to wet, interlayered silt, sand, and peat or, in places, a single peat layer. The north study area contains a thick layer of very soft, highly compressible peat, generally less than about 15 feet thick (CiviITech, 1997). However, other locations in the north study area contain thick sequences of very soft to soft peat, silt, and clay with layers of loose to medium dense, fine sand (e.g., CT97-B1, contained the soils described, throughout the 46.5-foot depth of the exploration). Peat also occurs as interbedded layers within very soft to medium stiff silt and very loose, slightly silty to silty sand. These silt and sand layers range up to about 6 feet thick. Standard penetration test (SPT) blow counts within the peat layers in the west study area borings, HC99-B37 and HC99-B38, indicates these soils range up to a relatively stiff condition.

Recessional Outwash. This material is generally medium dense to dense, slightly silty to silty, slightly gravelly to gravelly sand. Recessional outwash overlies the glacial till, or advance outwash where the glacial till has been eroded. Thickness of the recessional deposits varies over the site, but is generally less than 20 feet. Localized areas have thicker deposits of recessional outwash, such as in the west study area near AT94b-B4. The recessional deposits are generally absent where alluvial materials are located and dense to very dense glacial till or advance outwash sand and gravel underlies the alluvium.

Where recessional soils are located at the ground surface, the soil is in a weathered condition, typically more loose and higher in moisture content. These loose materials become medium dense at relatively shallow depths, typically less than about 10 feet. This layer may become colluvium where deposits are on sufficiently sloping ground. Gradation of the recessional outwash varies both vertically and laterally throughout the layer as shown in the relevant grain size

curves of Appendix B (e.g., HC99-B40, S-4; HC98-TP4, S-4; and HC98-TP10, S-4).

In the north study area, layers of soft to hard, sandy silt to silt were encountered interbedded with the sand and gravel layers of the recessional outwash deposits. The profile along the north wall (refer to Figure 6) illustrates the interbedding of this soil unit above the glacial till layer. This soil typically has a consistency of medium stiff to hard, but becomes soft near the surface. The soil is of low plasticity, generally with a plasticity index less than about 16. This material has some frictional strength due to its low plasticity and sand content as shown from the laboratory testing. In addition, this soil is of significantly lower permeability than the surrounding recessional soils.

Deeper Soils

Glacial Till. The till soils comprise the predominant glacially overridden soil unit underlying the surficial materials discussed above. This material is generally dense to very dense, slightly gravelly to gravelly, silty to very silty sand. The gradation of the till soils varies both vertically and laterally (e.g., HC99-B32, S-4; HC99-B35, S-4; HC99-38, S-4; and HC98-TP6, S-6).

In general, glacial till differs from the overlying recessional soils by having a higher silt content and much higher density. The top of the glacial soils is generally within 10 to 20 feet of the ground surface at the north end and west side. Some weathering was noted near the surface of the glacial till soils in explorations for both study areas.

Advance Outwash Sand. This material is generally dense to very dense, slightly silty, slightly gravelly to gravelly sand. In general, the advance outwash can be distinguished from the glacial till by lower silt content. Representative gradation curves would typically resemble those for samples HC99-B31, S-5; HC98-TP4, S-4; and HC98-TP7, S-8. However, observations at the site suggest that some areas of advance outwash are silty, which adds complexity to interpretation.

Lawton Silt/Pre-Vashon Deposits. The hard silt soils interpreted to be part of these geologic units in previous studies were not encountered in our explorations, but would likely be encountered at greater depths. These hard silt soils may be laminated or contain planes of separation (partings). Furthermore, these silt deposits are typically reported to be relatively plastic and are often slickensided (i.e., showing evidence of previous failure planes).

Study Area Generalized Hydrogeologic Regime

Within the Miller Creek drainage, the Advance Outwash appears to be thicker to the north and to the east of the creek drainage, beneath the airport (AGI, 1998). The Advance Outwash, also known as the Shallow Regional Aquifer, discharges to Miller and Des Moines Creeks, and via underflow to Puget Sound and the Green River valley (AGI, 1996).

Hydrogeologic Conditions

Groundwater elevation data were collected and slug testing performed to obtain data for estimating hydraulic conductivity values. These data and analyses are discussed below. The slug testing was performed in several areas of the drainage basin adjacent to Miller Creek, and water level measurements were collected within the drainage basin near Miller Creek, and on the flanks of the drainage basin beneath the existing airport embankment. Water levels vary over time, as indicated in Table 1.

Artesian conditions were encountered east of the north safety area. Initially, our exploration HC99-B43 encountered artesian pressure at 24.5 feet in depth. The water flowed freely from the well. Later, we advanced exploration HC99-B43A in the same area to install an observation well with a pressure gage to measure the excess head. HC99-B43A encountered the artesian pressure condition at a depth of 29 feet. The pressure gage was installed and read less than 5 psi.

Artesian conditions were also encountered in exploration AT97-B41, located near HC99-B43 but no pressure measurements are reported.

Artesian pressures are likely sustained by recharge occurring in higher elevation areas of the existing airport area to the south. However, continuity of the advance outwash soils and extent of such conditions will need to be further assessed.

Hydraulic Conductivity Testing

A pumping test was originally planned for HC-B33. However, the well yield was inadequate because of lower permeability soils, making a pumping test impractical based on the well's low flow-rate. Therefore, slug tests were performed on a larger number of wells.

Slug testing was performed on wells within the study areas shown on Figures 8 and 2. Slug tests were performed on six wells in the area northwest of the airport (HC99-B31 through HC99-B36, shown on Figure 2), and on four wells to the

west of the airport (HC99-B37 through HC99-B40, shown on Figure 3). Hydraulic conductivity values are summarized in Table 2. Test results are grouped by material type observed within the screened interval and by area. In the northwest study area (Figure 2), the geometric mean hydraulic conductivity for gravelly coarse sands was 6.5×10^{-3} cm/sec. For silty sands in this area, the geometric mean was 1.8×10^{-4} cm/sec. In the western study area (Figure 3), the wells were screened in silty sands, and the geometric mean hydraulic conductivity was 1.1×10^{-4} cm/sec.

Groundwater Flow Mapping

Groundwater levels were measured in eighteen wells. Groundwater elevations are contoured on Figure 7 for the Shallow Regional Aquifer, illustrating groundwater flow directions.

Groundwater flow is generally toward Miller Creek from the higher ground of the airport. It appears that significant recharge occurs on the higher ground of the airport, and that water moves down into the Shallow Regional Aquifer, and discharges to the creek drainage. At greater depths in and near the Miller Creek drainage basin, there is an upward hydraulic gradient, indicating the groundwater flow is discharging to the creek drainage basin.

There are limited indications of downward gradients beneath the plateau formed by the airport. This pattern is consistent with the implied occurrence of significant recharge beneath the existing airport. Based on the stratified nature of the subsurface soils, perched zones can occur above the main water table. In turn, the water table may not always be clearly defined due to the presence of perching layers and the transition occurring from vertical to horizontal groundwater flow.

Hart Crowser completed this work in general accordance with our proposal dated January, 28, 1999. This report is for the exclusive use of HNTB, the Port of Seattle, and their design consultants for specific application to the Third Runway project and site. We completed this study in accordance with generally accepted geotechnical/hydrogeologic practices for the nature and conditions of the work completed in the same or similar localities, at the time the work was performed. We make no other warranty, express or implied.

Sincerely,

HART CROWSER, INC.



James R Benn

JAMES R. BEAVER, E.I.T. Senior Staff Geotechnical Engineer

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MICHAEL J. BAILEY, P.E. Project Manager

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Bouwer, H. and R.C. Rice, 1976. A slug test for determining hydraulic conductivity of unconfined aquifers with completely or partially penetrating wells, V.12 No. 3, 423-428, Water Resources Research.

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Table 1 - Water Level Data	vel Data									
East of 12th	A79 Depth*	AT96-B1 th* Elevation	AT97-869 Depth* Eleva in Foot in F	- B69 Elevation in Feet	AT96A-B8 Depth* Eleva in Foot in F	A-B8 Elevation in Feet	AT96/ Depth* in Feet	AT96A-B10 pth* Elevation Feet in Feet	AT97-841 Depth* Elevi in Feet In F	- B41 Elevatio In Feel
Ton of Monument	102111									
Measuring Point	0.00	407.7	0.00	337.2	0.00	412.7	0.00	319.7	0.00	312
Ground Level*	-0.3		3.2	334	<u>6.0-</u>	413	-0.3		3.2	30
Top of Screen ⁺	78	330	28	310	50	363	24	296	81	5
Bottom of Screen*	88	320	30	308	61	352	34	286	83	5
Date: 3/8/1999									Flowing	>312
e construction de la construction de la construcción de la construcció	dry	dry	6.18				8.15			
4/5/1999 dry	dry	dry	6.59				8.11		311.59 Flowing	>312
5/4/1999 dry 5/15/1999	dry	dry	7.43	329.77			8.35	311.35	0.91	311.
	•	-								
6/14/1999 dry	۲up	ζ	8.08	329.12	47.86	364.84	8.74	196'015	1.27	50.5
						·				
West of 12th	AT97	AT97-B57	HC9	HC99-B31	HC9	HC99-B32	HC9	HC99-B33	HCG	HC99-B34
	Depth		Depth.	Elevation	Depth*	Elevation	Depth.	Elevation		
	in Feet	in Feet	in Feet	in Feet	in Feet	in Feet	in Feet	in Feet	in Feet	in Fe
Top of Monument	000	225 7	000	766 74		766.79	000	365.65	000	767
Ground Level*	£.0-		2.5				2.9			
Top of Screen*	13		17.50		13		=			
Bottom of Screen*	23	385	27.50	238.74	23.10	243.19	21.90	243.75	17.40	250
Date: 3/8/1999			2.38	263.86	3.55	262.74	2.71	262.94	4.72	i 262
			2.41	263.83	3.51	262.78	2.64	1 263.01	4.68	3 262
5/4/1999			2.58	263.66	4.14				5.44	
6/14/1999	2.11	233.59	2.93	263.31	4.75	261.54	2.61	1 263.04	5.88	3 261
		_			_		_		_	
		Bold = Measured or Surveyed	d or Surve	pəki						

308.16 307.56 307.49

308.86

31.87

303.94

21.21

537.93 302.93 292.93

0.00 2.8 37.80 47.80

325.2 322

0.00 3.2

303 298

23 28

231 229 312.2 309

340.73

in Feel

in Feet

in Feel

in Feet

in Feet

HC99-841

Depth* Elevation Depth* Ilevation Depth* Elevation

AT97-842

33.56 307.17

22.58 302.57

310.88

to be abandoned

to be abandoned

33.24

302.93 302.98

22.22

33.17

32.57

303.56

21.59 22.17

0.91 311.24

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269.20 268.80 270.02

5.83 6.23

270.30

4.73 5.01

289.89 289.45 289.00 288.10

4.69

262.91

5.13 5.58 6.48

262.95 262.19 261.75

260.63

2.4 6.40 10.40

264.63

269.58

272.63

275.03

0.00

294.58 292.58 279.58

0.00

267.63 265.23 260.23 250.23

2.0 15.00 25.00

Depth* Elevation

Depth* Elevation

Depth* Elevation

HC99-B35

HC99-B36

in Feet in Feet

in Feet

in **F**cet

in Feet

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Depth* All depths are below **Measuring Point** (NOT below the ground surface)

Italics = Estimated

Sheet 2 of 2

Table 1 - Water Level Data

East of 12th	HC99	HC99-B43A	HC99-B45	-845	HC99-B46	-846	HC99-847	- B 47
	Depth*	Elevation	Depth*	Elevation	Depth*	Elevation	Depth*	Elevation
	in Feet	in Feet	in Feet	in Feet	in Feet	in Feet	in Feet	in Feet
Top of Monument								
Measuring Point	0.00	295.58	0.00	285.29	0.00	332.82	0.00	281.22
Ground Level*	5	292.58	3.1	282.19	2.0	330.82	2.4	278.82
Top of Screen*	27	268.58	8.10	277.19	30.00	302.82	7.4	273.62
Boltom of Screen *	37	258.58	13.10	272.19	40.00	292.82	12.4	268.82
<u>10/1999</u> 3/10/1999			6.70	278.59	22.01	310.81		
4/5/1999	4/5/1999 Under Pressure	ssure	7.50	277.79	22.48	310.34		
5/4/1999	-10	306	7.93	277.36		309.73	6.26	274.96
5/15/1999								
6/14/1999		304.81	8.99	276.30	23.75	309.07	7.44	273.78
				•			_	-
West of 12th	HC9	HC99-B37	HC99-B38	-B38	HC99-839	-839	HC96	HC99-840
	Depth	Elevation	Depth•	Elevation	Depth*	Elevation	Depth*	Elevation
	in Feet	in Feet	in Feet	in Feet	in Feet	in Feet	in Feet	in Feet
Top of Monument								
Measuring Point	0.00	237.65	0.00	230.88	0.00	230.80	0.00	250.63
Ground Level*	3.1	234.55	3.3	227.58	<u>6.9</u>	231.10	2.0	248.63
Top of Screen*	9.10	228.55	12.30	218.58	4.70	226.10	14.00	236.63
Bottom of Screen*	19.10	218.55	22.30	208.58	14.70	216.10	24.00	226.63
Date: 3/8/1999	3.52	234.13	4.40	226.48	0.69	11 05 0	88 1	745 75
4/5/1000	158		1 4 1	71 200		20000		
				14.022		90.022		245.37
9991/8/c		233.83	4.60	226.28		229.94		244.88
6/14/1999	5.12	232.53	5.90	224.98	1.68	229.12	6.89	243.74
_				-				

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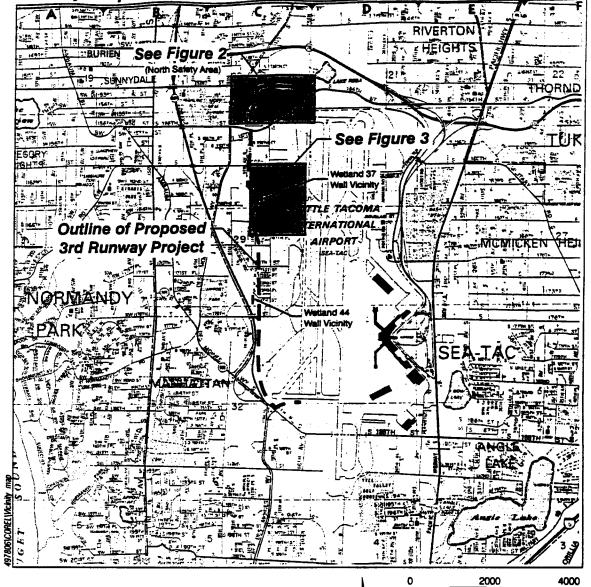
		Hydraulic
Location	Soil Types in Screen Interval	Conductivity
		in cm/sec
Northwest Are	2	
	Gravelly Coarse Sands	
НС-В31	Dense, gravelly, fine to coarse SAND	1.0 x 10 ⁻²
HC-B32	Loose to dense, slightly silty to silty, medium to coarse SAND	3.7 x 10 ⁻³
HC-B34	Medium dense to dense, very silty SAND to very gravelly, coarse SAND	7.5 x 10 ⁻³
	Geometric Mean:	6.5 x 10 ⁻³
	Silty Sands	
НС-В33	Very dense, slightly gravelly, very sandy SILT to very silty SAND	2.0 × 10 ⁻⁴
HC-B35	Dense to very dense, slightly gravelly, very silty SAND	3.0 × 10⁴
HC-B36	Medium dense, very silty SAND	<u>9.5 × 10^{.5}</u>
	Geometric Mean:	1.8 × 10 ⁻¹
West Area		
	Silty Sands	
HC-B37	Dense, very silty, fine to medium SAND, and sandy silty PEAT	9.5 x 10 ^{.5}
HC-B38	Soft, slightly sandy SILT, and very dense, slightly gravelly to gravelly, silty SAND	7.0 x 10 ⁻⁵
HC-B39	Medium dense to very dense, slightly gravelly, silty, fine SAND	1.5 x 10⁴
HC-B40	Medium dense to very dense, slightly gravelly, silty SAND	<u>1.3 × 10⁻⁴</u>
	Geometric Mean:	1.1 x 10 ⁻⁴

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Table 2 - Summary of Hydraulic Conductivity Estimates

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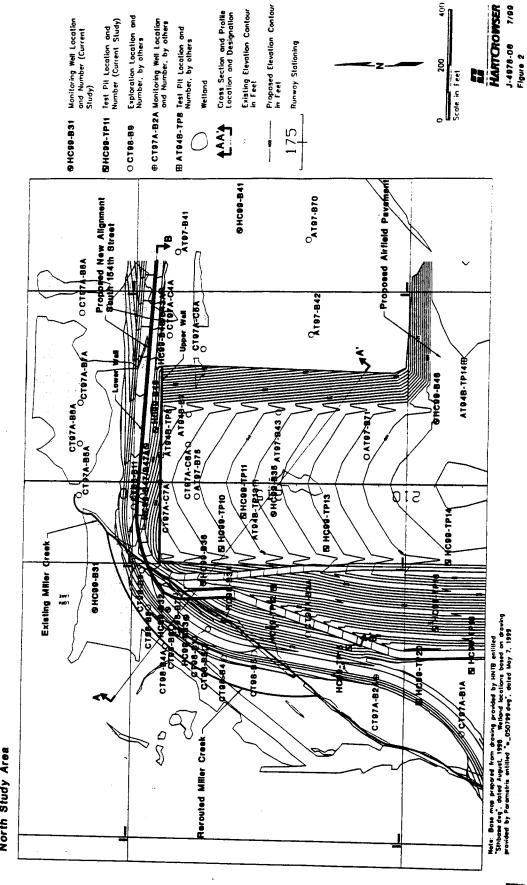
Vicinity Map



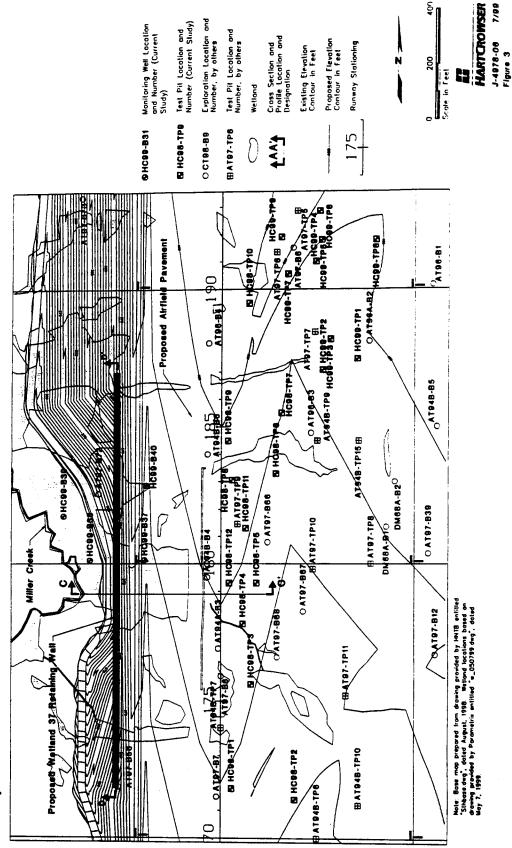
Scale in Feet

HARTCROWSER J-4978-06 7/99 Figure 1

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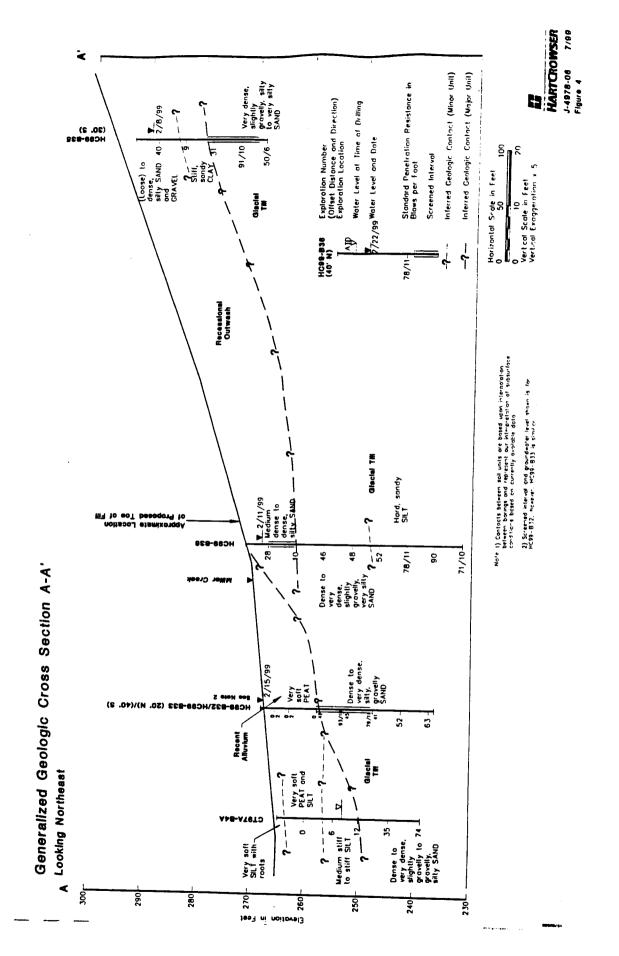
Site and Exploration Plan - 1 of 2 North Study Area

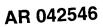


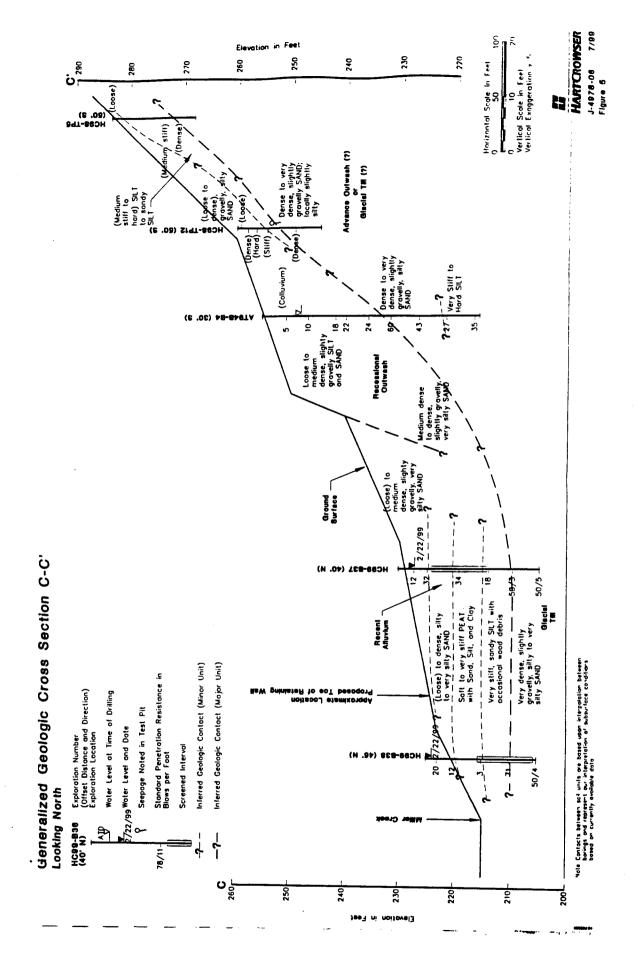
Site and Exploration Plan - 2 of 2 West Study Area

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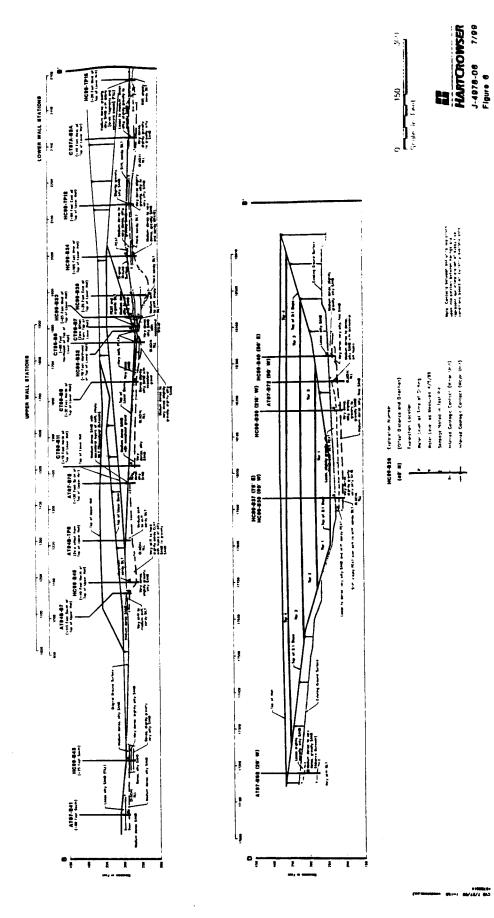
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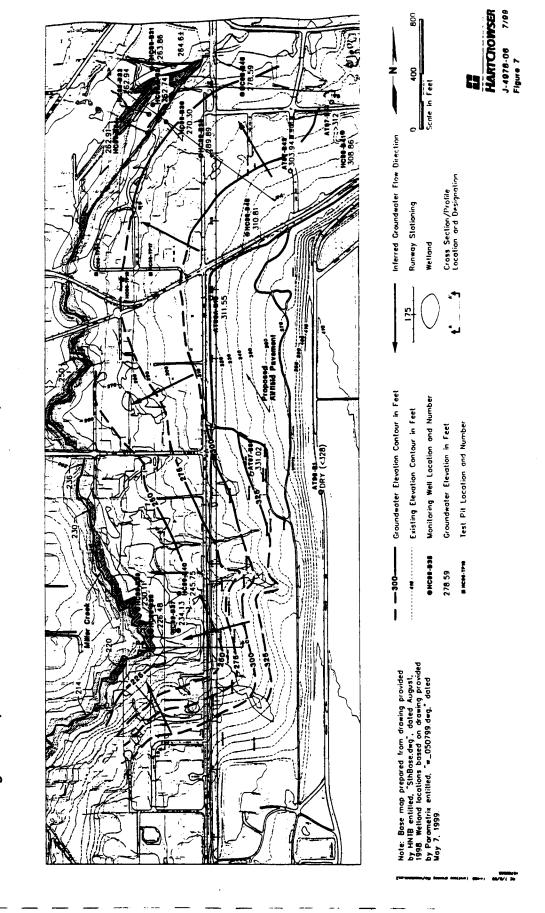












Shallow Regional Aquifer Groundwater Elevation Contour Map

APPENDIX A FIELD EXPLORATIONS METHODS AND ANALYSIS

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APPENDIX A FIELD EXPLORATIONS METHODS AND ANALYSIS

This appendix documents the processes Hart Crowser used in determining the nature of the soils underlying the project site addressed by this report. The discussion includes information on the following subjects:

- Explorations and Their Location;
- The Use of Auger Borings;
- Standard Penetration Test (SPT) Procedures;
- Use of Shelby Tubes;
- Excavation of Test Pits;
- Hydraulic Conductivity Testing (Slug Testing); and
- Water Level Measurement.

Explorations and Their Location

Subsurface explorations for this project include the following:

Borings

HC99-B31 through HC99-B41, HC99-B43, HC99-B43A, HC99-B45, HC99-B46, HC99-B47, and HC99-B47A

Test Pits

HC98-TP1 through HC98-TP12; and HC99-TP1 through HC99-TP21.

The exploration logs within this appendix show our interpretation of the drilling (or excavation), sampling, and testing data. They indicate the depth where the soils change. Note that the change may be gradual. In the field, we classified the samples taken from the explorations according to the methods presented on Figure A-1 - Key to Exploration Logs. This figure also provides a legend explaining the symbols and abbreviations used in the logs.

Location of Explorations. Figures 2 and 3 show the location of explorations. In the field, borings were originally located by hand taping or pacing from existing physical features. The ground surface elevations at these locations were interpreted from the aerial survey topography shown on the figures. The method used determines the accuracy of the location and elevation of the explorations.

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The Use of Auger Borings

With depths ranging from 15.8 to 45.9 feet below the ground surface, fourteen hollow-stem auger borings, designated HC99-B31 through HC99-B41, HC99-B43, HC99-B43A, HC99-B45, HC99-B46, HC99-B47, and HC99-B47A were drilled from February 8 through 22, 1999, and April 19-20, 1999. The borings used a 3-3/8-inch inside diameter hollow-stem auger and were advanced with a truck-mounted drill rig subcontracted by Hart Crowser. The drilling was continuously observed by an engineering geologist from Hart Crowser. Detailed field logs were prepared of each boring. Using the Standard Penetration Test (SPT), we obtained samples at 2-1/2- to 5-foot-depth intervals.

The borings logs are presented on Figures A-2 through A-17 at the end of this appendix.

Standard Penetration Test (SPT) Procedures

This test is an approximate measure of soil density and consistency. To be useful, the results must be used with engineering judgment in conjunction with other tests. The SPT (as described in ASTM D 1587) was used to obtain disturbed samples. This test employs a standard 2-inch outside diameter split-spoon sampler. Using a 140-pound hammer, free-falling 30 inches, the sampler is driven into the soil for 18 inches. The number of blows required to drive the sampler the last 12 inches only is the Standard Penetration Resistance. This resistance, or blow count, measures the relative density of granular soils and the consistency of cohesive soils. The blow counts are plotted on the boring logs at their respective sample depths.

Soil samples are recovered from the split-barrel sampler, field classified, and placed into water tight jars. They are then taken to Hart Crowser's laboratory for further testing.

Several instances of "heave" are noted on boring logs. Heave is a phenomenon that occurs typically within a sand soil instigated by seepage pressure at the bottom of the auger (i.e., water within the augers is at a lower elevation than the groundwater level surrounding the boring). A sufficient difference in water levels will cause the sandy soils to be thrust upward into augers, thereby disturbing the soil formation. Therefore, the corresponding SPT N-values do not accurately indicate density. Heave is typically controlled by sustaining the water level within the augers at or near the surrounding groundwater level, or alternatively using drilling muds. Neither of these methods were readily available to the drilling program at the site, drilling mud could not be used under the terms of the wetland permit.

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In the Event of Hard Driving

Occasionally very dense materials preclude driving the total 18-inch sample. When this happens, the penetration resistance is entered on logs as follows:

Penetration less than six inches. The log indicates the total number of blows over the number of inches of penetration.

Penetration greater than six inches. The blow count noted on the log is the sum of the total number of blows completed <u>after</u> the first 6 inches of penetration. This sum is expressed over the number of inches driven that exceed the first 6 inches. The number of blows needed to drive the first 6 inches are not reported. For example, a blow count series of 12 blows for 6 inches, 30 blows for 6 inches, and 50 (the maximum number of blows counted within a 6-inch increment for SPT) for 3 inches would be recorded as 80/9.

Use of Shelby Tubes

To obtain a relatively undisturbed sample for classification and testing in finegrain soils, a 3-inch-diameter thin-walled steel (Shelby) tube sampler was pushed hydraulically below the auger. This was performed for HC99-B47 and HC99-B47A to obtain to samples from 12.5 to 15 feet (Greg, confirm?). The tubes were sealed in the field and taken to our laboratory for extrusion and classification. These samples were taken for consolidation and direct shear testing.

Excavation of Test Pits

Twelve and twenty-one test pits, designated HC98TP-1 through HC98-TP12; and HC99-TP1 through HC99-TP21, respectively, were excavated across the site with a tractor-mounted backhoe subcontracted by our firm. The '98 test pits were excavated on July 30, 1998. The '99 test pits were excavated on February 16, 1999, and April 7-12, 1999. The sides of these excavated pits offer direct observation of the subgrade soils. The test pits were located by and excavated under the direction of an engineering geologist from Hart Crowser. The geologist observed the soil exposed in the test pits and reported the findings on a field log. Our geologist took representative samples of soil types for testing at Hart Crowser's laboratory. He noted groundwater levels or seepage during excavation. The density/consistency of the soils (as presented parenthetically on the test pit logs to indicate their having been estimated) is based on visual observation only as disturbed soils cannot be measured for in-place density in the laboratory.

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The test pit logs are presented on Figures A-18 through A-34.

Hydraulic Conductivity Testing (Slug Testing)

Hydraulic conductivity testing was performed using the slug test method. In this method the water level (hydraulic head) in the well is rapidly raised or lowered, and the rate at which it returns to its initial state is used to calculate hydraulic conductivity for the formation surrounding the wellscreen. Data were collected using an Aquistar data logger in conjunction with a Instrumentation Northwest PSI9000 pressure transducer. Tests were conducted as follows:

- A transducer was set in the well and allowed to equilibrate with ambient conditions, and background water level data were collected.
- One or two slug rods (solid PVC rods) were rapidly introduced into the well (causing a near-instantaneous rise in water level), to initiate a falling head test. Water level data were collected in logarithmically increasing time increments using the data logger and transducer. For wells where depth to water was small, a falling head test was not attempted.
- ▶ Water level in the well was allowed to re-equilibrate.
- The slug rod or rods were rapidly pulled from the well (causing a nearinstantaneous drop in water level) to initiate a rising head test. Water level data were collected in logarithmically increasing time increments using the data logger and transducer.
- Most of the wells responded reasonably quickly, and therefore multiple slug tests were performed for most wells.

Data were pre-processed as described in Butler (1998), and hydraulic conductivity values were estimated using the method of Bouwer and Rice (1976) for unconfined aquifers. The estimated values are summarized in Table 1.

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Water Level Measurement

Water levels were measured using a Solinst water level probe, graduated in 0.01-foot increments. Depth to water was measured below the top of casing, and recorded to the nearest hundredth of a foot. Depth to water was converted to groundwater elevation using survey information for the top of casing in the wells. Depth to water data and groundwater elevations are summarized in Table 2.

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Key to Exploration Logs

Sample Description

Classification of soils in this report is based on visual field and laboratory observations which include density/consistency. moisture condition, groin size, and plasticity estimates and shade not be construct to imply fierd nor incordery testing unless presented herein. Visual-manual classification methods of ASTM D 2488 were used as an identification guide.

Soil descriptions consist of the following:

Density/consistency, moisture, color, minor constituents, MAJOR CONSTITUENT, additional remarks.

Density/Consistency

Soil density/consistency in borings is related primarily to the Standard Penetration Resistance. Soil density/consistency in test pits is estimated based on visual observation and is presented parentmetically on the test pit logs. Approximate Shear Strength in TSP Stondard Penetration Stongord Penetration SET or CLAY SAND or GRAVE_ Resistance (N) in Blows/Foot Resistance (N) in Blows/Foot Consistency Density <0.125 0 - 2 Very soft 0 - 4 Very loose 0.125 - 0.25 2 - 4 Soft 4 - 10

Medium stiff

Very stiff

Stiff

Hord

Moisture

Very dense

Medium dense

Loose

Dense

Dry Little perceptible moisture

- Demp. Some perceptible moisture, probably below optimum
- Moist Probably near optimum moisture content
- Much perceptible moisture, probably above optimum Wet

10 - 30

30 - 50

>50

Legends

ž

(Test Pits)

	Logo	
-	Sam	pling Test Symbols
Ì	BORING	S SAMPLES
	\boxtimes	Spiit Spoon
	$\overline{\Sigma}$	Snelby Tube
		Cuttings
	\square	Core Run
	*	No Sample Recovery
ļ	₽	Tube Pushed, Not Driven
İ	TEST	PIT SAMPLES
	\boxtimes	Grab (Jor)
	\square	Bag
	\Box	Sneiby Tube
Ì		
	Grou	Indwater Observations
		Surface Seal
HOHING DWG	_⊽	Groundwater Leve: on Date (ATD) At Time of Drilling
HOHIN		Observation Well Tip or Slotted Section
_		Groundwater Seepage

Minor Constituents Estimated Percentage

4 - 8

8 - 15

15 - 30

>30

0 - 5
5 - 12
12 - 30
30 - 50

0.25 - 0.5

0.5 - 1.0

1.0 - 2.0

>2.0

Test Symbols

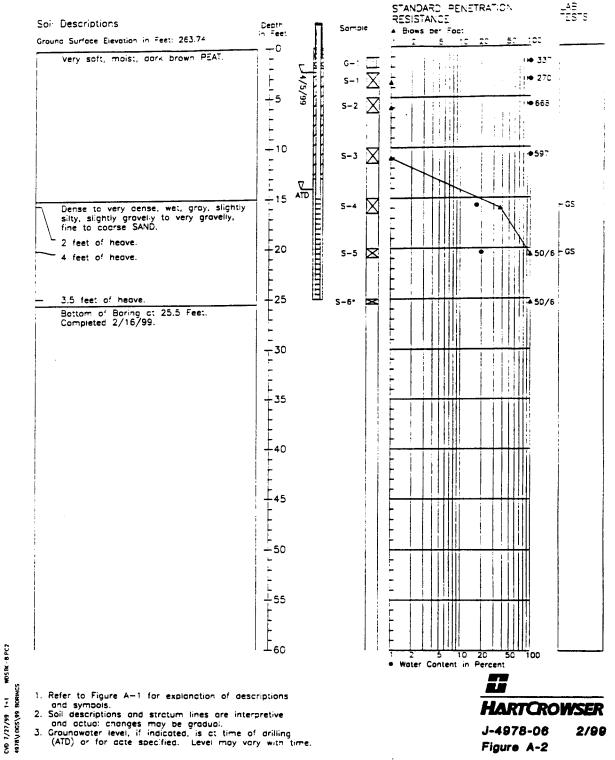
NS	No Sheen
S S	Slight Sheen
MS	Moderate Sheen
HS	Heovy Sheen
TCD	Triaxial Consolidated Drainec
0 0	Unconfined Compression
DS	Direct Shear
к	Permecbility
PD	Pocket Penetrometer Approximate Compressive Strength in TSF
τv	Torvane Approximate Shear Strength in TSF
CBR	California Bearing Ratio
мD	Maisture Density Relationship
AL.	Atterberg Limits
	Water Content in Percent
	Liquid Limit
	Natural Plastic Limit
P:D	Photoionization Detector Reading
CA	Chemica: Analysis
DT	In Situ Density Test



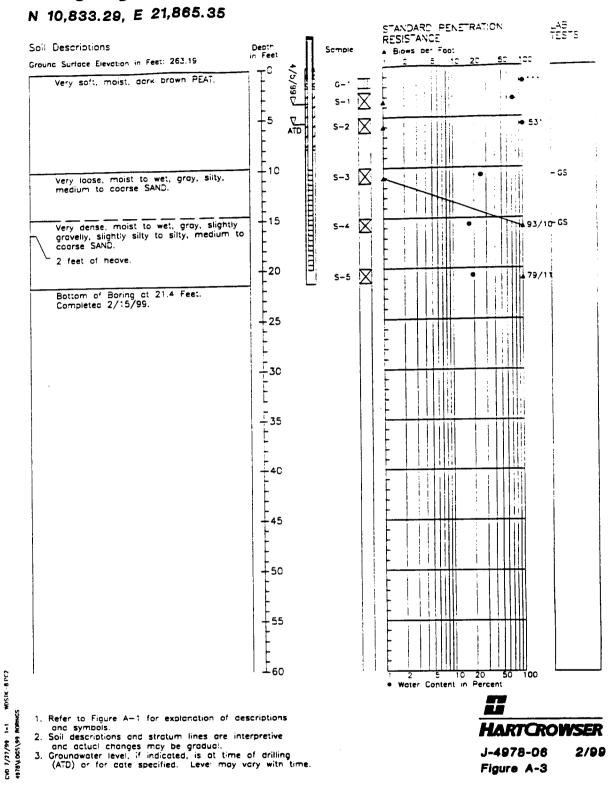
Boring Log HC99-B31

N 10,827.55, E 22,134.13

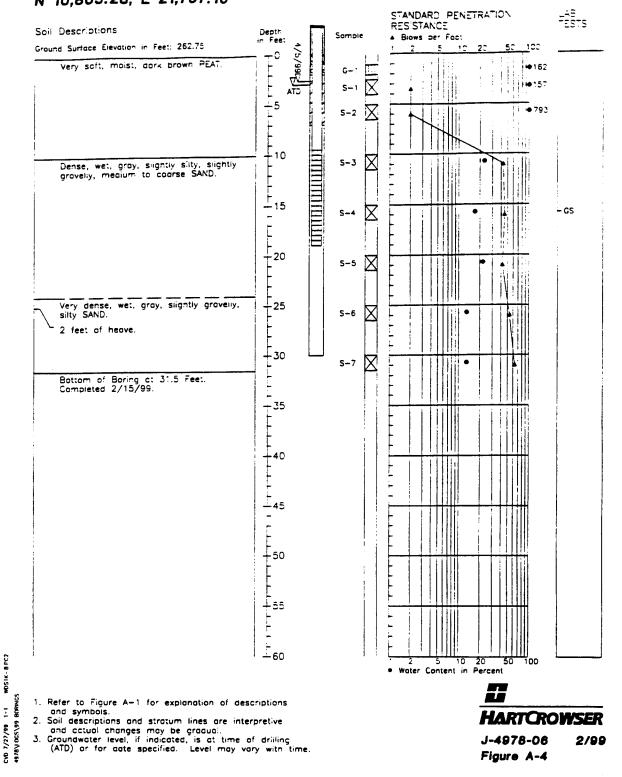
WDSTK - B PC2



Boring Log HC99-B32

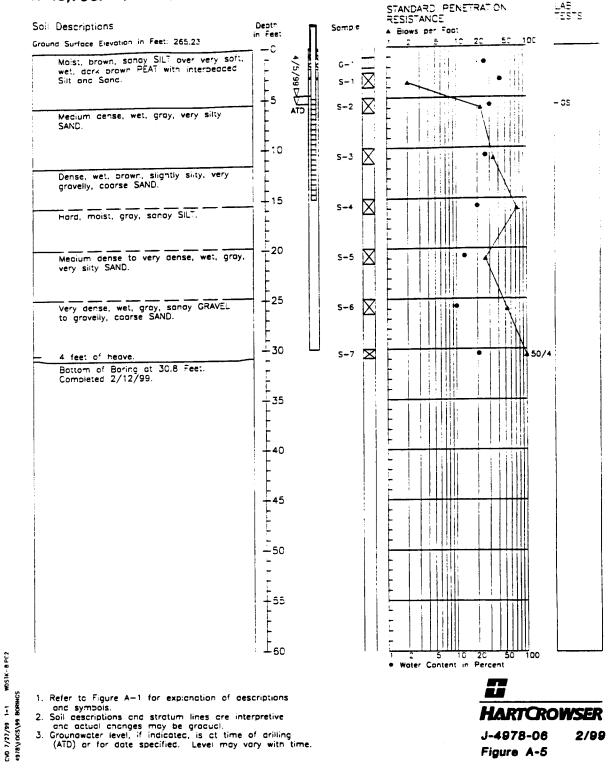


Boring Log HC99-B33 N 10,805.28, E 21,797.16



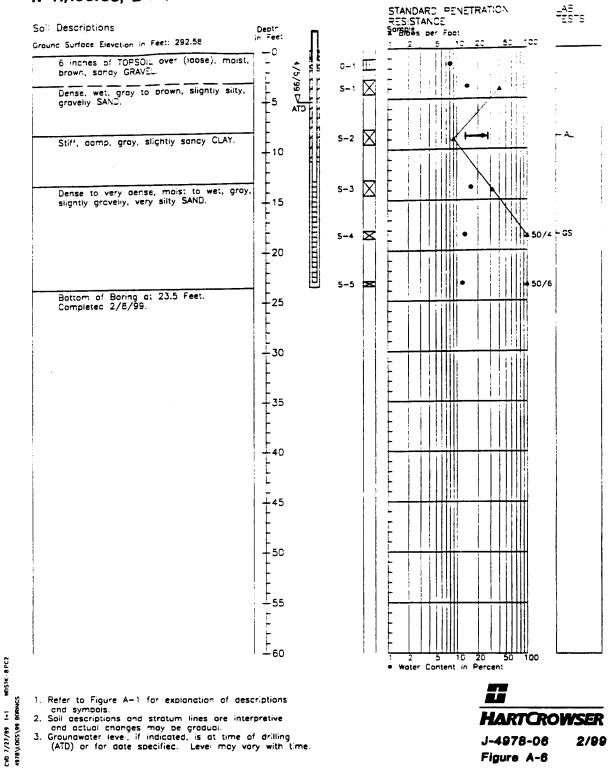
Boring Log HC99-B34 N 10,796.45, E 21,659.37

WDS1K-B PC2



Boring Log HC99-B35 N 11,188.88, E 21,481.49

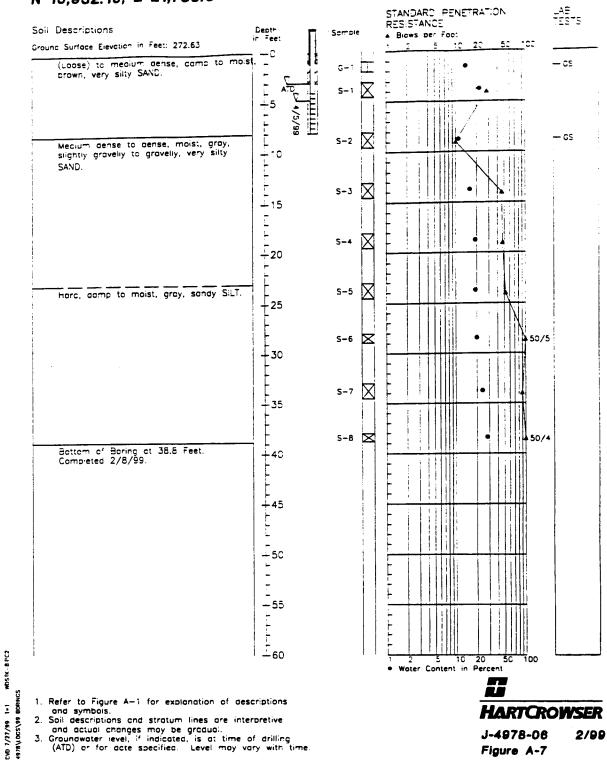
WDS1K-8 PC2



Boring Log HC99-B36

N 10,932.10, E 21,736.5

MD514 - 8 PC2



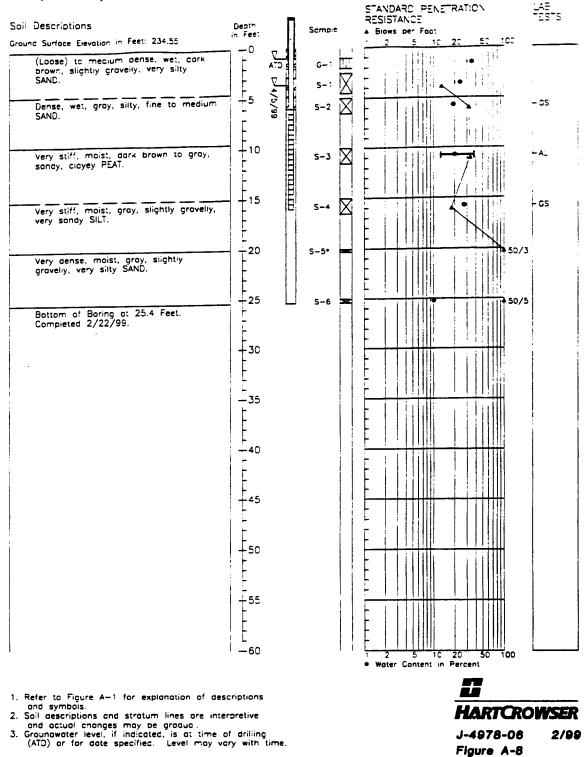
Boring Log HC99-B37

N 11,020.06, E 18,013.81

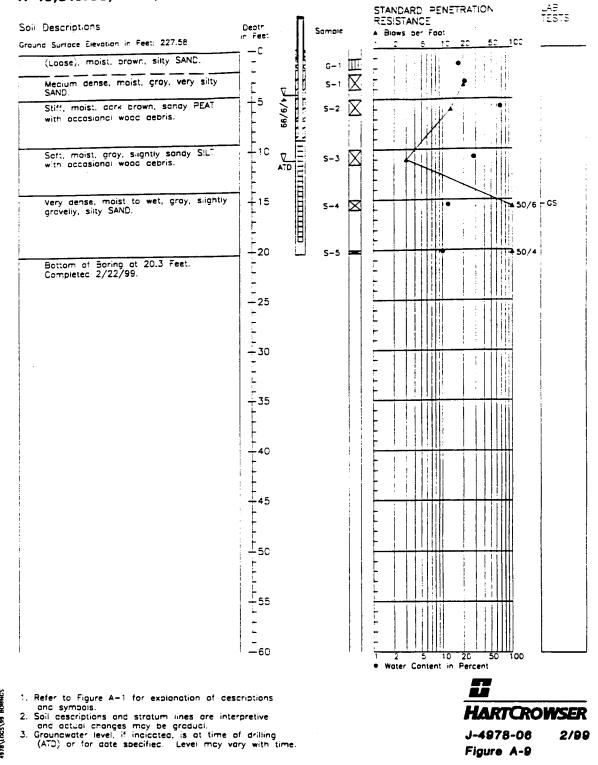
- B PC2

- XESOM

CVD 7/27/99 1=1 1



Boring Log HC99-B38 N 10,819.39, E 18,011.99

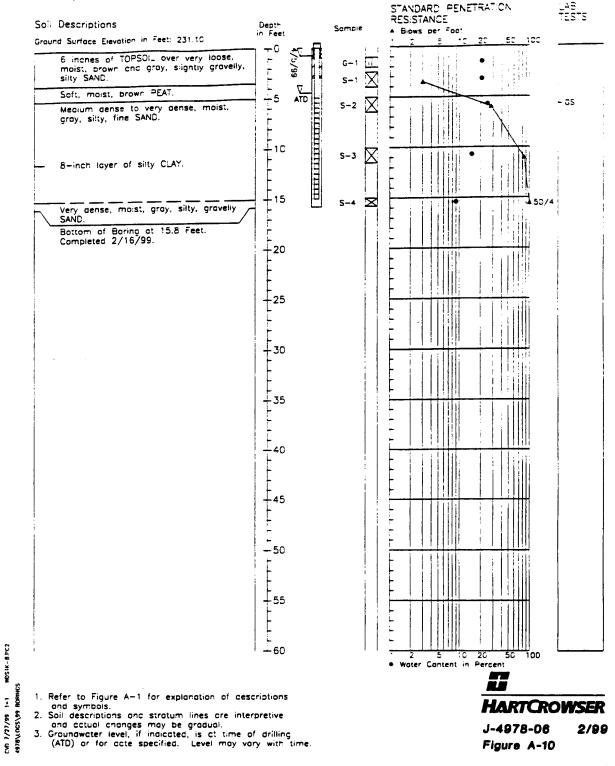


- B PC2 MDS1K -1=1 M

CVD 7/27/99 1 4978\LOCS\99 E

Boring Log HC99-B39 N 10,722.31, E 18,174.14

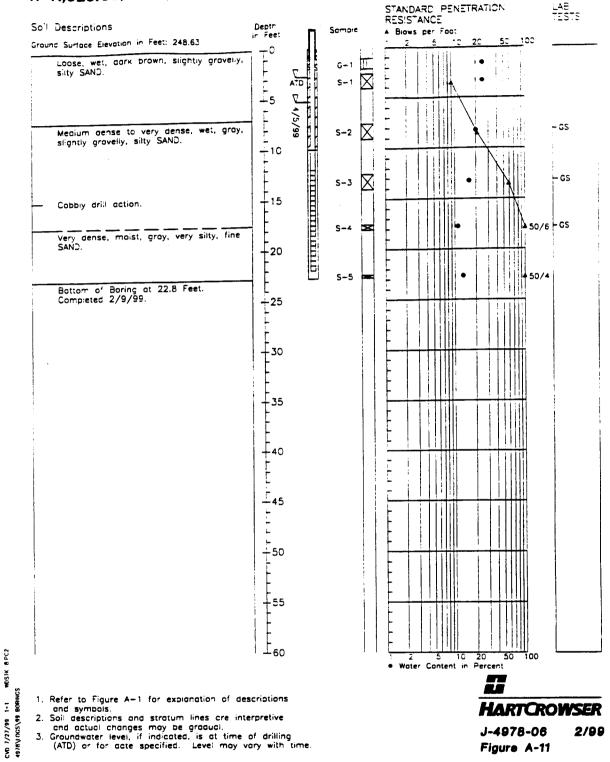
MDS1K-8.PC2



Boring Log HC99-B40

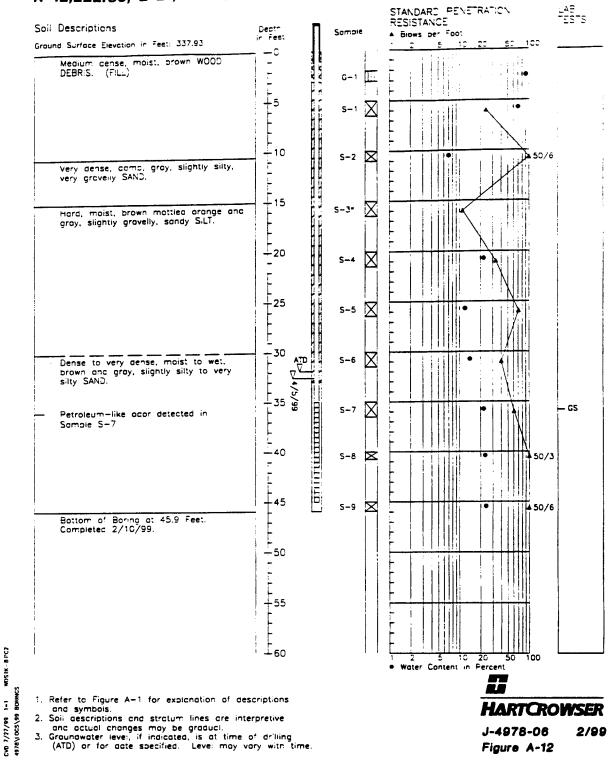
N 11,025.60, E 18,285.23

MDS1K - B PC2

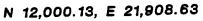


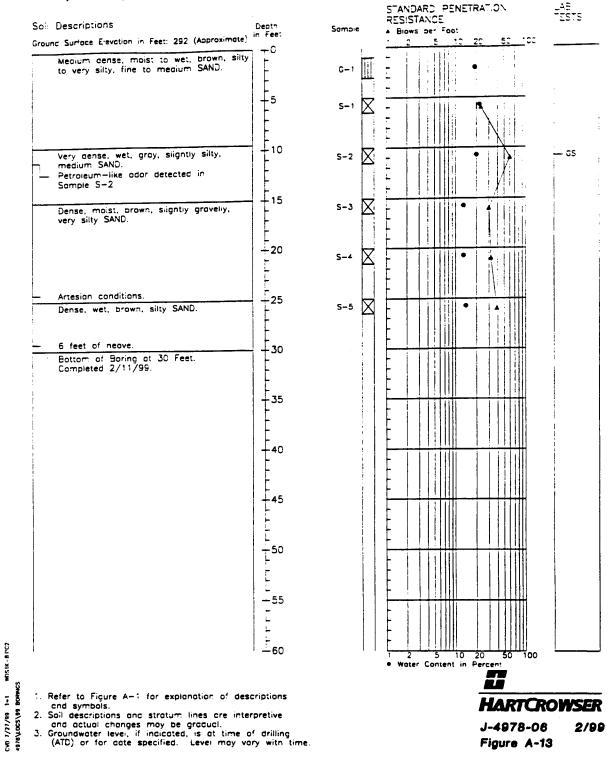
Boring Log HC99-B41 N 12,222.85, E 21,624.38

WDS IK - 8 PC2



Boring Log HC99-B43

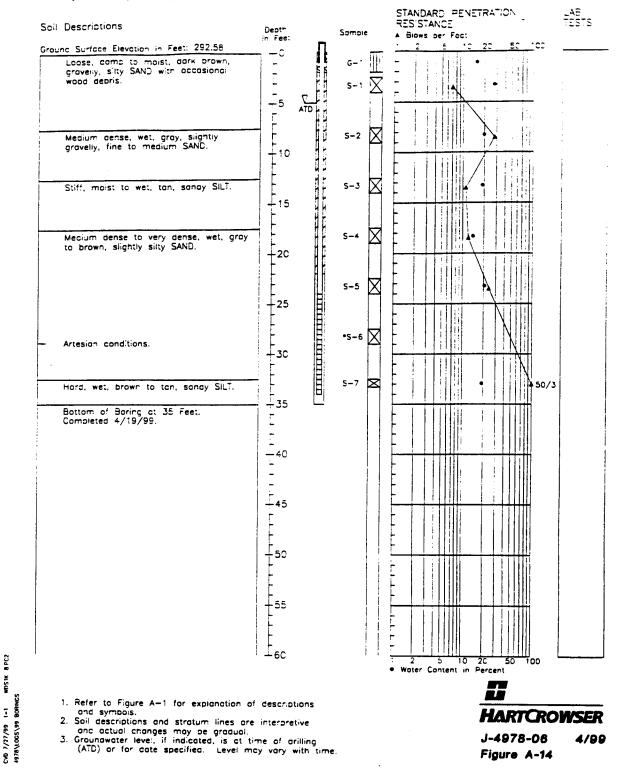




Boring Log HC99-B43A N 11,998.17, E 21,914.80

WDSTK BPC2

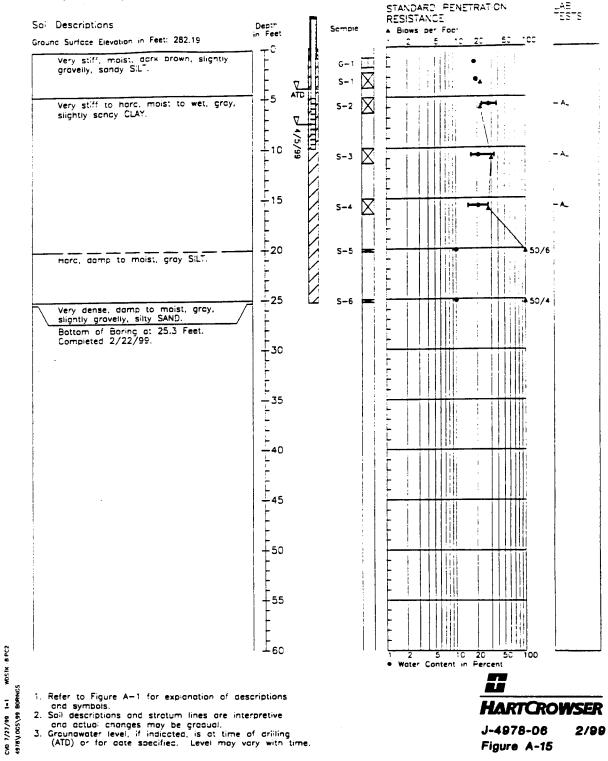
Ξ



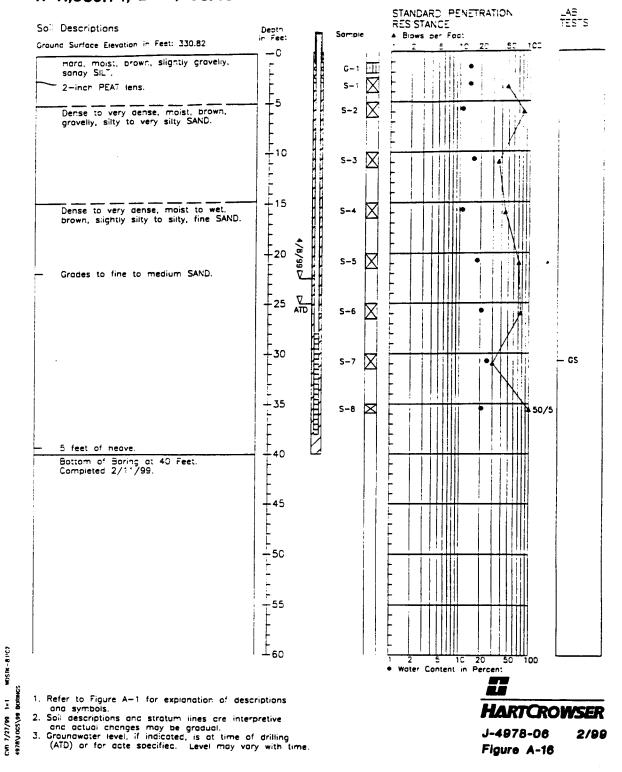
Boring Log HC99-B45

N 11,492.55, E 21,921.99

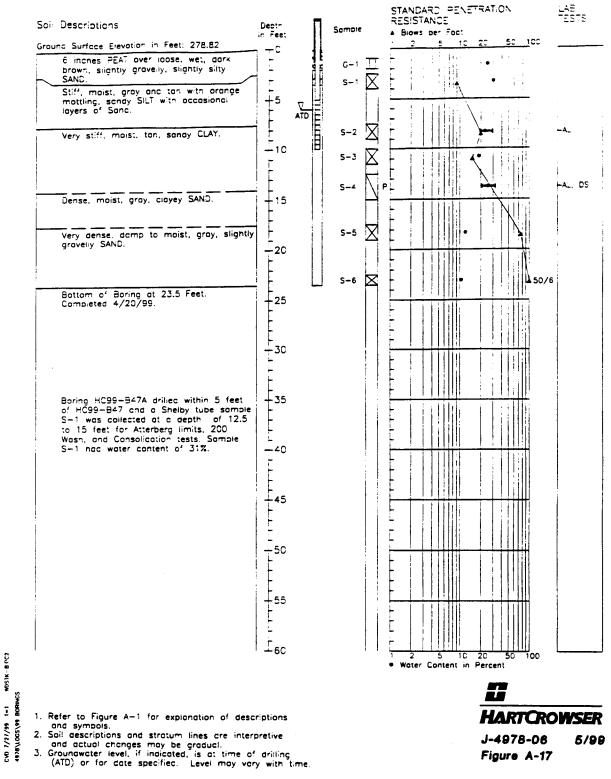
WDSTK - B PC2



Boring Log HC99-B46 N 11,530.74, E 20,896.43



Boring Log HC99-B47 N 11,432.63, E 21,955.31



WDSTK-B PC2

1=1 W

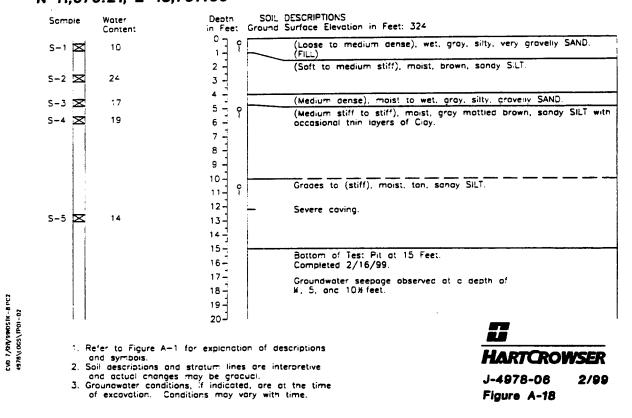
Test Pit Log HC99-TP1 N 11,795.46, E 18,749.38

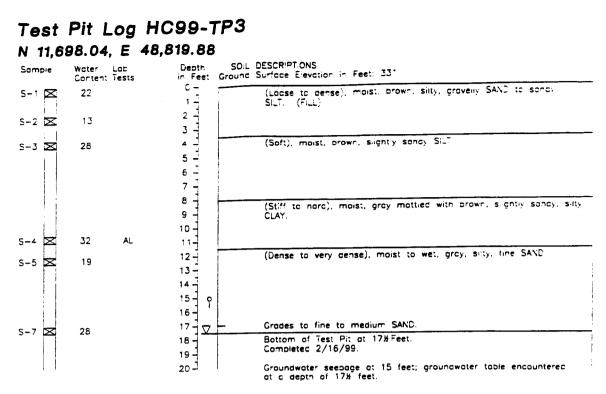
Sample	Water Lab Content Tests		SOL DESCRIPTIONS Ground Surface Elevation in Feet: 342
s-1 🗵	32	0 -	(Loose), moist, prown, silty, very gravely SAND. (Fill over (loose to medium dense), moist, groy, very silty, fine SAND to
5-2 🗷	19 GS	2	very sandy SLT.
s-3 🛛	16 GS	<u>د</u> -	
S-4 🕱	13	5 - 6 - 7 -	
5-5 🗷	18	8 -	(Meaium stiff), moist, gray, slightly sonay Si
		9	Bottom of Test Pit ot 8½ Feet. Completed 2/16/99.

Test Pit Log HC99-TP2 N 11,670.21, E 18,707.60

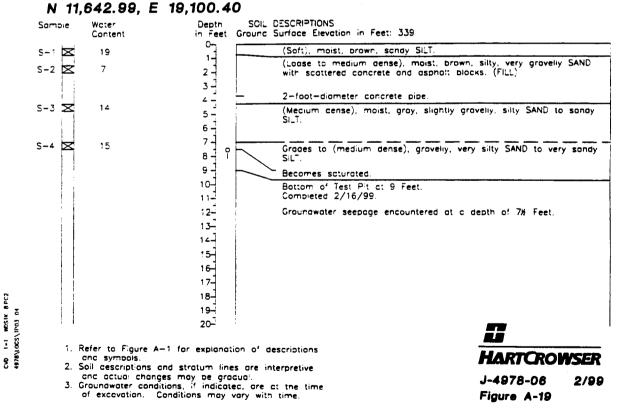
.

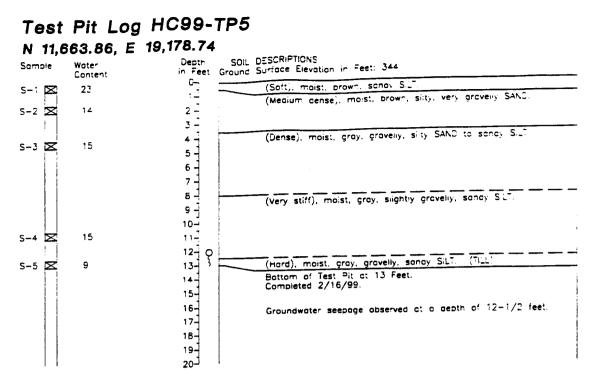
-



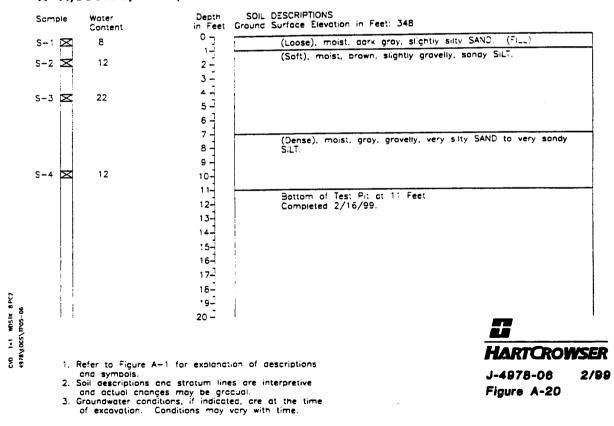


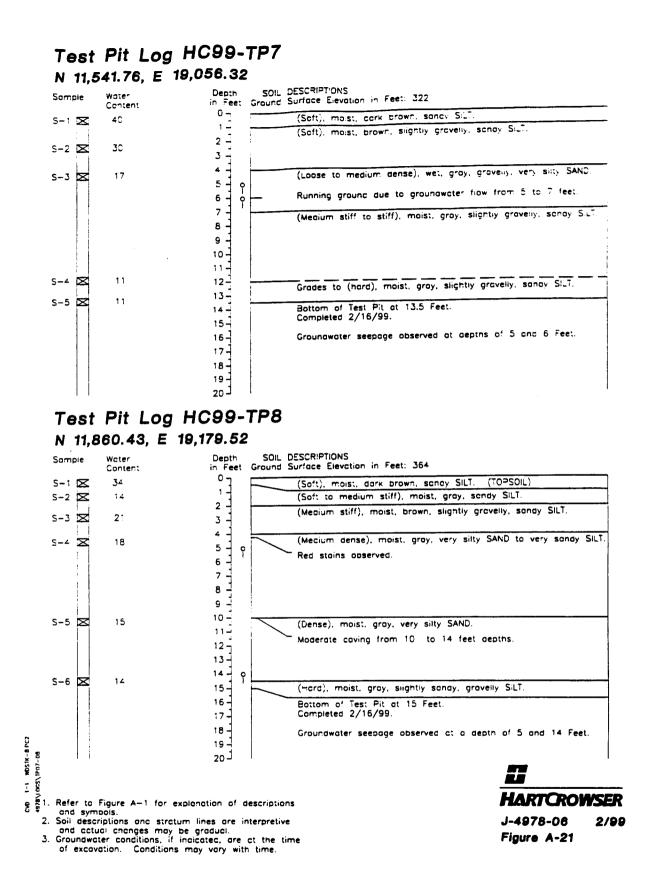
Test Pit Log HC99-TP4



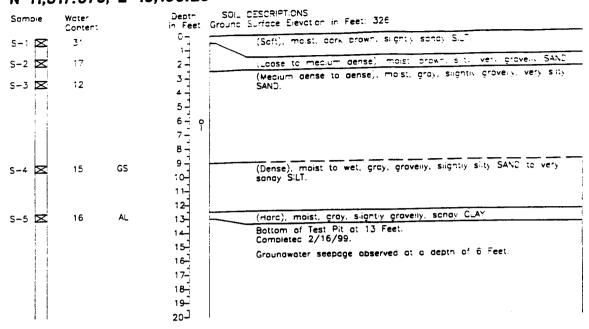


Test Pit Log HC99-TP6 N 11,656.03, E 19,284.06

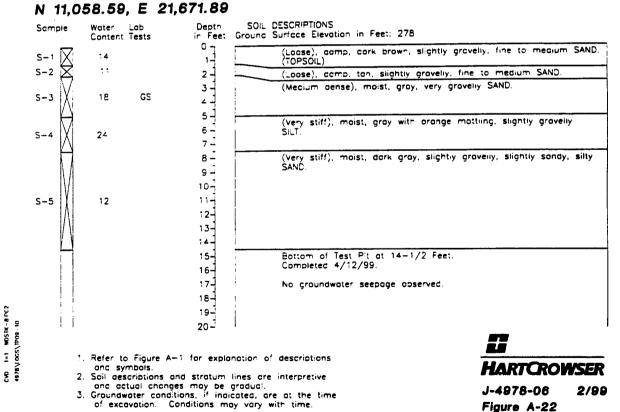


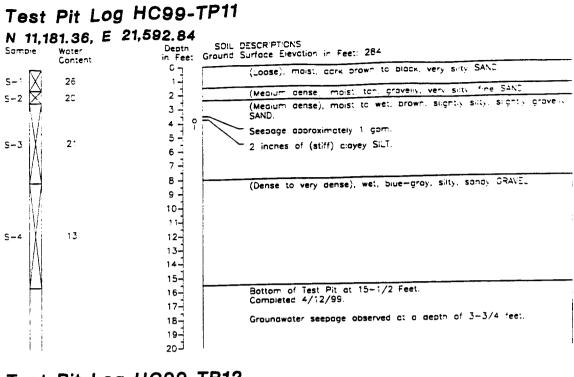


Test Pit Log HC99-TP9 N 11,517.076, E 19,190.28

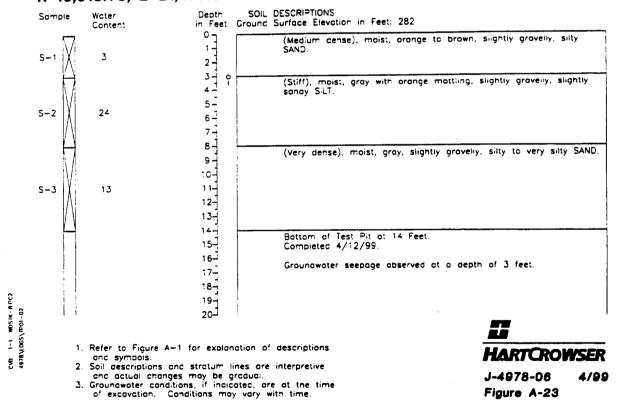


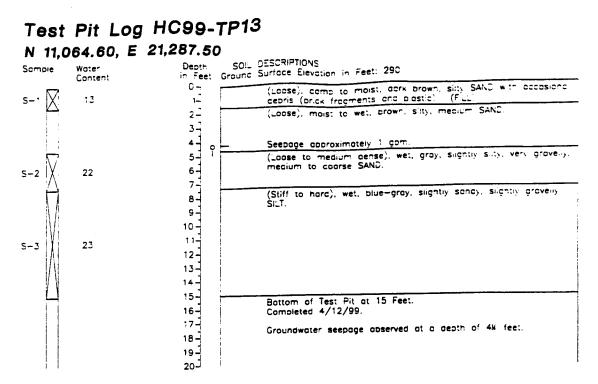
Test Pit Log HC99-TP10



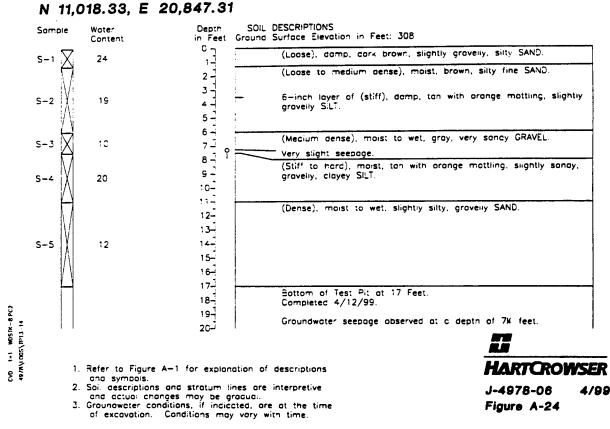


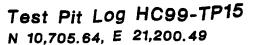
Test Pit Log HC99-TP12 N 10,918.78, E 21,477.90

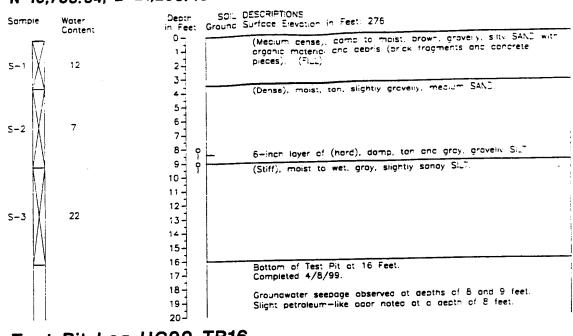




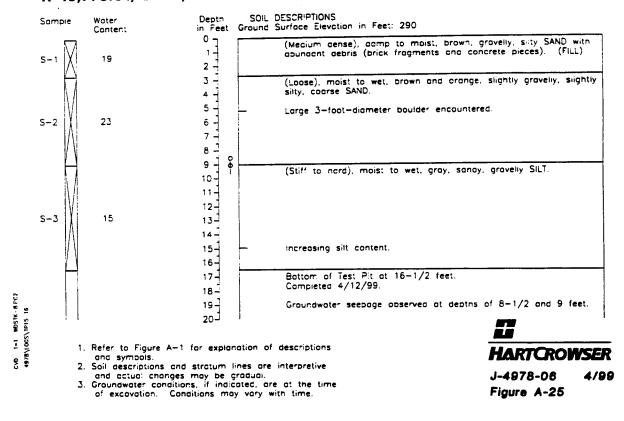
Test Pit Log HC99-TP14

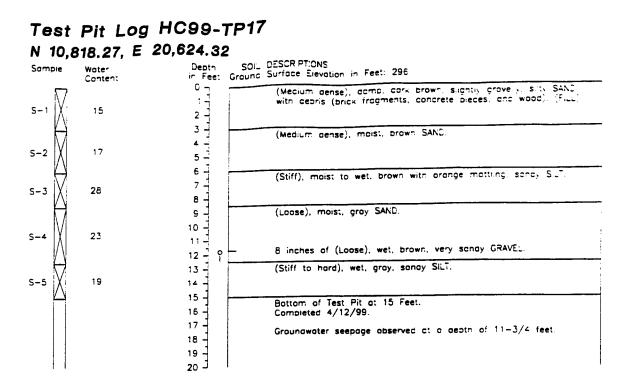




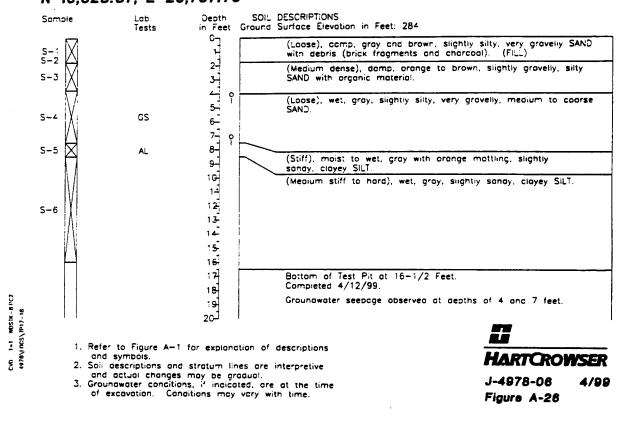




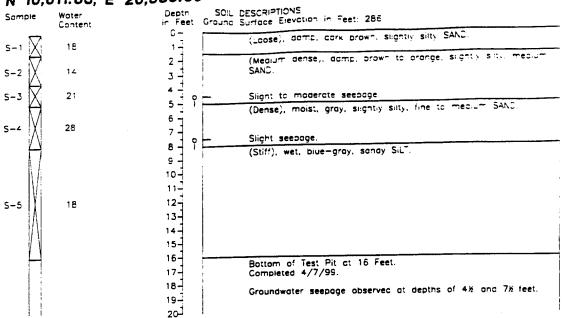




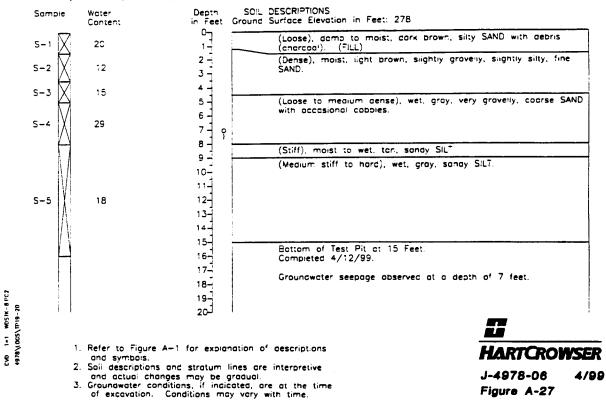
Test Pit Log HC99-TP18 N 10,628.87, E 20,757.75



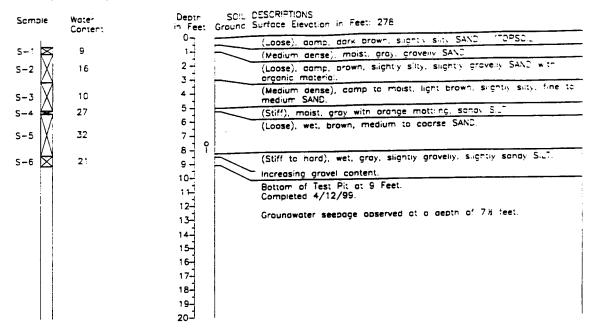
Test Pit Log HC99-TP19 N 10,611.83, E 20,585.59



Test Pit Log HC99-TP20 N 10,513.61, E 20,945.70



Test Pit Log HC99-TP21 N 10,416.98, E 20,627.60



MDS1K-8PC2 NPO1-02 CVD 1+1

- 1. Refer to Figure A-1 for explanation of descriptions and sympols.



and symbols.
 Soli descriptions and stratum lines are interpretive and actual changes may be gradual.
 Grounowater conditions, if indicated, are at the time of excavation. Conditions may vary with time.

Test Pit Log HC98-TP1

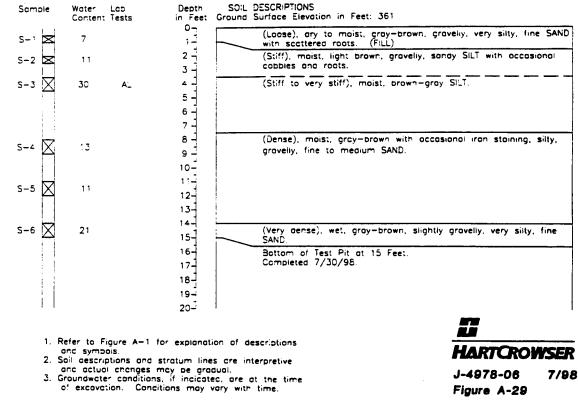
N 11,340, E 17,180 Deptr. SOIL DESCRIPTIONS in Feet Ground Surface Elevation in Feet: 346 Semple Woter Content (Loose), by to moist, silly, gravely, fine SAND with southered roots (Fig.) C٦ 1 s-: 🖾 Е rcots. (Stiff), cry to moist, gray, soncy, gravely Sill with 2 s-2 ⊠ s-3 ⊠ scattered roots. 12 3 -(Medium stiff), moist, gray-brown, slightly gravely, sanay S.-12 4 -(Medium dense to dense), moist, gray-brown, gravely, sity. fine SAND. 7 -S-4 🛛 10 8 -9 -10s-5 🕅 9 11-Iron staining. 12-13-(Dense to very dense), moist, gray-brown, slightly, silty, fine s-6 🗙 7 14-SAND. 15-Bottom of Test Pit of 15 Feet. Completed 7/30/98. 16-17-Slight caving from depth of 10 to 14 feet. 18-19-20 -

Test Pit Log HC98-TP2



4

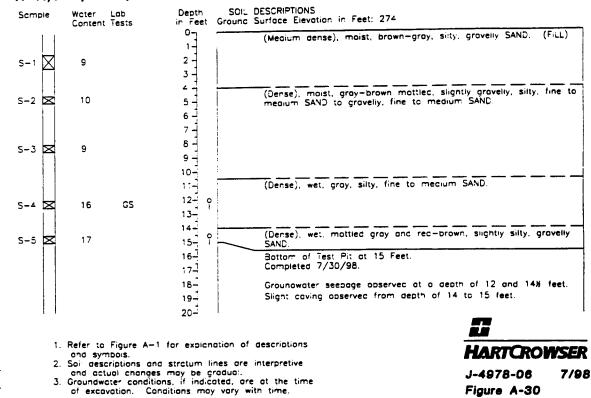
CVD 5/3/99 1-1 WDS14 RPC2 9/8/LOGS/98 1251 PUS



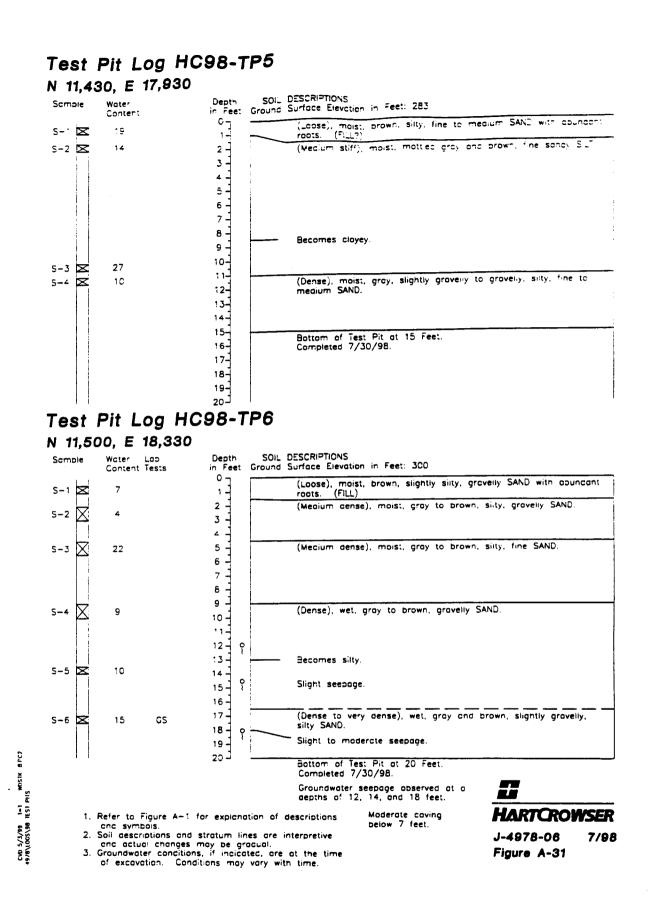
Test Pit Log HC98-TP3 N 11,410, E 17,560

SOIL DESCRIPTIONS Depth Water Ground Surface Elevation in Feet: 299 Sample in Feet Content (Lease to meaium dense), moist, gray, sughtly gravely, sily, fine to meaium SAND, (FILL) 67 1 s-1 🛛 8 2 s-2 🕅 10 3 -(Very stiff), moist, gray-prown mottled, fine samey SLT. 4 -S-3 ₹ 21 16 (Dense), moist, gray, sitty, fine SAND. 5 -6 7 -(very dense), moist, gray, silty, gravely, the SAND to gravely SAND. 14 5-5 🖾 8 -S-6 🖾 3 9 1 (Stiff), moist, gray, clayey SILT with slickensides and fractures. 10s-7 🖾 27 11-12-13-14-15-Bottom of Test Pit at 15 Feet. Completed 7/30/98. 16-17-18-19-20]

Test Pit Log HC98-TP4 N 11.380, E 17,780

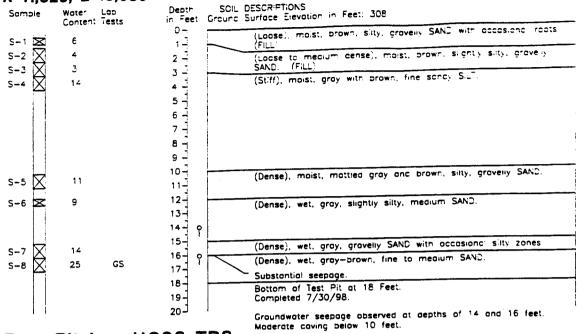


CV0 5/3/99 1=1 WDSTK- 8.PC2 1978\005\98 H.ST PI15

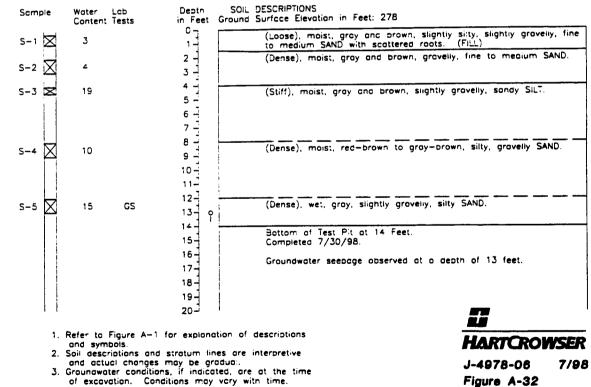


Test Pit Log HC98-TP7

N 11.520, E 18,550



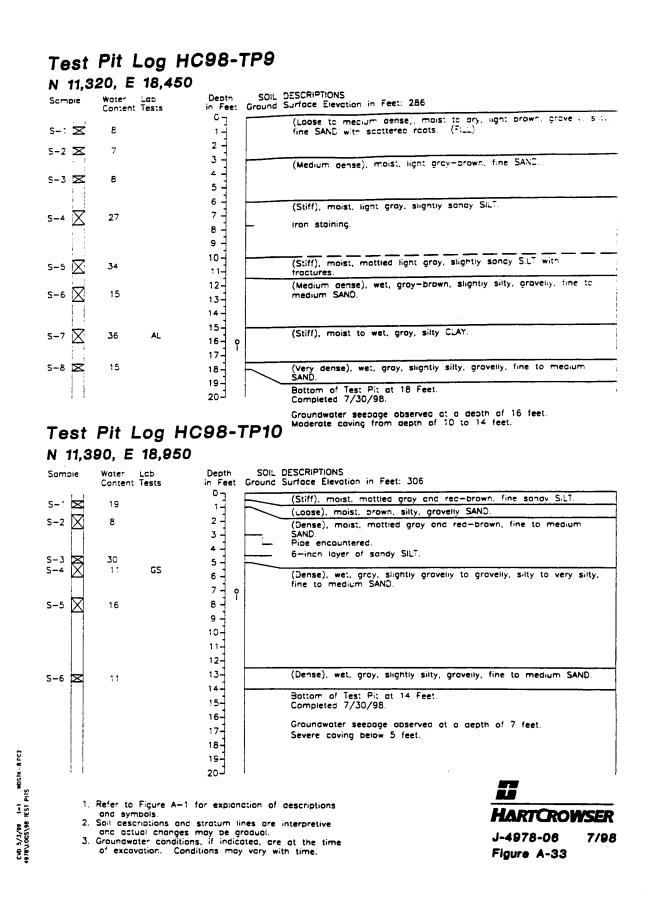
Test Pit Log HC98-TP8 N 11,339.54, E 18,305.82

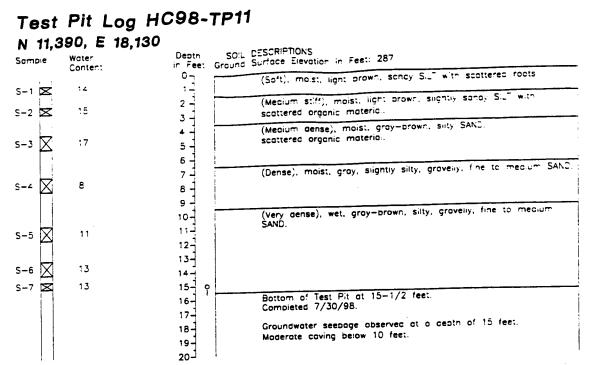


of excavation. Conditions may vary with time.

1=1 MDSIK-BPC7 TEST PITS

CVD 5/3/99





Test Pit Log HC98-TP12 N 11,330, E 17,930

SOIL DESCRIPTIONS Water Lop Content Tests Depth Sample Ground Surface Elevation in Feet: 260 in Feet 0-(Loose), moist, brown, silty, fine to medium SAND. (FILL) (Dense), moist, gray, slightly silty, gravely, fine to medium SAND. s-1 🛛 17 1-S-2 🖾 7 2 -3 -Pipe encountered. Flow approximately 2 gpm 18 (Hord), moist, gray, sandy, gravely SiL* S-3 S-4 ጅ 4 -AL 35 5-(Stiff), wet, gray and brown, clayey SILT. 6 -(Dense), wet, gray, slightly silty, gravelly, fine to medium SAND. 7-S-5 🖾 18 Ŷ 8 -9 -10-11-12-13-j 14-15-Bottom of Test Pit at 15 Feet. Completed 7/30/98. 16 -17-Groundwater seepage observed at a depth of 7-1/2 feet. Severe caving at 7-1/2 feet. 18-19tet MDSIK-BPC2 IEST PIIS تـ 20 1. Refer to Figure A-1 for explanation of descriptions HARTCROWSER and sympols. 2. Soil descriptions and stratum lines are interpretive J-4978-08 7/98

CVD 5/3/99 4978\1005\98 1

and actual changes may be gradual. 3. Groundwater conditions, if indicated, are at the time

of excavation. Conditions may vary with time.

Figure A-34

APPENDIX B LABORATORY TESTING PROGRAM

Hart Crowser J-4978-06

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APPENDIX B LABORATORY TESTING PROGRAM

A laboratory testing program was performed for this study to evaluate the basic index and geotechnical engineering properties of the site soils. Both disturbed and relatively undisturbed samples were tested. The tests performed and the procedures followed are outlined below.

Soil Classification

Field Observation and Laboratory Analysis. Soil samples from the explorations were visually classified in the field and then taken to our laboratory where the classifications were verified in a relatively controlled laboratory environment. Field and laboratory observations include density/consistency, moisture condition, and grain size and plasticity estimates.

The classifications of selected samples were checked by laboratory tests such as Atterberg limits determinations and grain size analyses. Classifications were made in general accordance with the Unified Soil Classification (USC) System, ASTM D 2487, as presented on Figure B-1.

Note that the term "with" used on boring logs generally indicates a material within the soil matrix that constitutes a relatively small fraction by weight of the total soil. The usage of this term in not associated with the ASTM simplified classification procedure.

Water Content Determinations

Water contents were determined for most samples recovered in the explorations in general accordance with ASTM D 2216, as soon as possible following their arrival in our laboratory. Water contents were not determined for very small samples nor samples where large gravel contents would result in values considered unrepresentative. The results of these tests are plotted or recorded at the respective sample depth on the exploration logs. In addition, water contents are routinely determined for samples subjected to other testing. These are also presented on the exploration logs.

Grain Size Analysis (GS)

Grain size distribution was analyzed on representative samples in general accordance with ASTM D 422. Wet sieve analysis was used to determine the size distribution greater than the U.S. No. 200 mesh sieve. The size distribution for particles smaller than the No. 200 mesh sieve was determined by the

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hydrometer method for a selected number of samples. The results of the tests are presented as curves on Figures B-2 through B-12 plotting percent finer by weight versus grain size.

200-Wash

One sample was subjected to a modified grain size classification known as a 200-wash. The samples were "washed" through the No. 200 mesh sieve to determine the relative percentages of coarse- and fine-grained material in the samples. The tests were performed in general accordance with ASTM D 1140. This was performed for Shelby tube sample HC99-B47A at a depth interval between 12.5 and 15 feet. The results indicated 28 percent passing the No. 200 sieve; therefore, the soil is a silty fine sand at the location the sample for analysis was taken. We expect that this is a sandier zone in the overall Shelby sampled interval, as the majority of the sample was sandy silt.

Atterberg Limits (AL)

We determined Atterberg limits for selected fine-grained soil samples. The liquid limit and plastic limit were determined in general accordance with ASTM D 4318-84. The results of the Atterberg limits analyses and the plasticity characteristics are summarized in the Liquid and Plastic Limits Test Report, Figures B-13 through B-18. This relates the plasticity index (liquid limit minus the plastic limit) to the liquid limit. The results of the Atterberg limits tests are shown graphically on the boring logs as well as where applicable on figures presenting various other test results.

Atterberg limits provides a classification of the fine-grained fraction of a soil (i.e., passing the U.S. No. 200 sieve). This is based on the behavior of the soil in response to accepted mechanical tests, but does not accurately distinguish between clay and silt-size particles. Our visual classifications were, in our opinion, more representative of the soil than the Atterberg classification. This was the case for samples visually classified as sandy silt or silt, by Hart Crowser that were classified as "CL" by the Atterberg chart. The low plasticity indices of these samples further support our use of the classification of silt rather than clay.

Consolidation Test (CN)

The one-dimensional consolidation test provides data for estimating settlement and preconsolidation pressure. The test was performed in general accordance with ASTM D 2435. A relatively undisturbed, fine-grained sample was carefully trimmed and fit into a rigid ring with porous stones placed on the top and bottom of the sample to allow drainage. Vertical loads were then applied

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incrementally to the sample in such a way that the sample was allowed to consolidate under each load increment. Measurements were made of the compression of the sample (with time) under each load increment. Rebound was measured during the unloading phase. In general, each load was left in place until the completion of 100 percent primary consolidation, as computed using Taylor's square root of time method. The next load increment was applied soon after attaining 100 percent primary consolidation. For the 4 tsf load increment, the load was left in-place for about 16 hours to record secondary compression characteristics. The test results plotted in terms of axial strain and coefficient of consolidation versus applied load (stress) are presented on Figure B-19.

Direct Shear Test (DS)

The undrained direct shear test was performed by PSI, Inc., in general accordance with ASTM D 3080-90. The test sample was trimmed from a relatively undisturbed soil sample and placed in the direct shear box. The sample was not allowed to consolidate under an applied vertical load prior to shearing. A horizontal force was applied to the shear box containing the sample. In this way, the sample fails along a predetermined failure plane. The shearing took place at a constant strain rate, and was done quickly enough so that no drainage would occur.

The data are presented on a Mohr-Coulomb diagram plotting shear (failure) stress versus normal stress. The line through the points of failure represents the effective angle of internal friction (\emptyset) and the intercept along the vertical axis the apparent cohesion (c'). The test results are shown in Figure B-20.

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Unified Soil Classification (USC) System

	Ş	Size	of O	peni	ng ir	n inche	5			i			Number of I (US SI					!			Grau	n Size in	Mille	metr	es		
		-	~	20	-	58	3 3	5		,		ę	8	Ş	8	8	5	88	5	8	8	5	8	ŝ	8	200	
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	-	-											Grain Size	in Milli	metre	s							-	-	-	-	
COBBL	ES	1			G	RAVEL							SA	ND				ļ				SILT and	CLA	Ŷ			
							Coa	rse	-Gr	ain	ed S	oils						;			Fi	ne-Grain	ed S	oris			

Coarse-Grained Soils

GW	GP	GM	GC	SWS	5 P 🚶	SM SC						
Ciean GRAV	EL <5% fines	GRAVEL with	>12% fines	Clean SAND <5%	ines	SAND with >12% fines						
GRA	VEL >50% coarse f	raction larger than	No. 4	SAND >50% coarse fraction smaller than No. 4								
		Coarse-(Grained Soils >50	& larger than No. 200 seve	•							
G W and S V	$W\left(\frac{D_{60}}{D_{60}}\right) > 4$ for G	W $\frac{1}{8} 1 \leq \frac{1}{(D_{30})^2}$	2	GP and SP C	ean GRAVE	EL or SAND not meeting						

$$W \text{ and } S W \left(\frac{D_{60}}{D_{10}} \right) > 6 \text{ for } S W \quad \& 1 \le \left(\frac{(D_{30})}{D_{10} \times D_{60}} \right) \le$$

G M and S M Atterberg limits below A line with PI <4

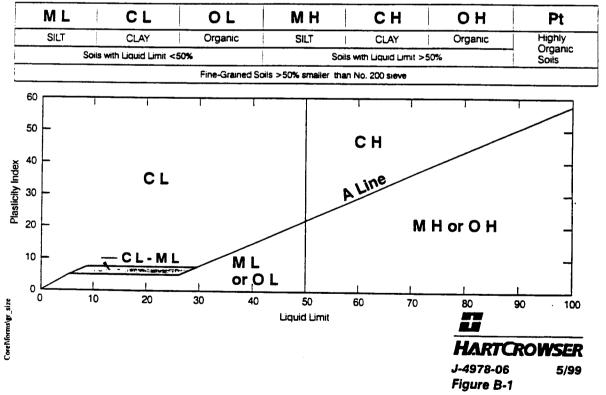
G P and S P Clean GRAVEL or SAND not meeting requirements for G W and S W

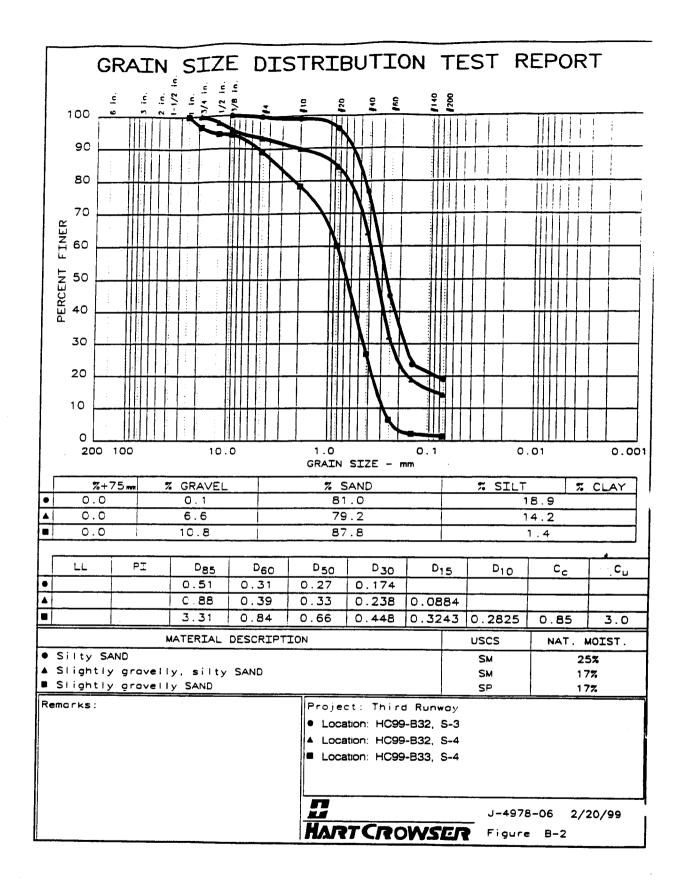
G C and S C Atterberg limits above A Line with PI >7

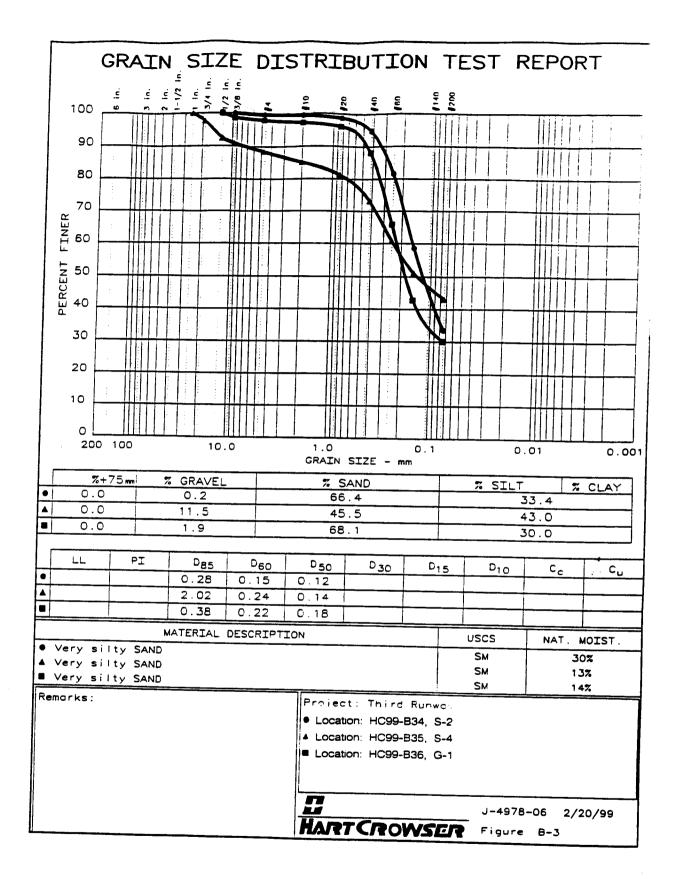
* Coarse-grained soils with percentage of fines between 5 and 12 are considered borderline cases required use of dual symbols.

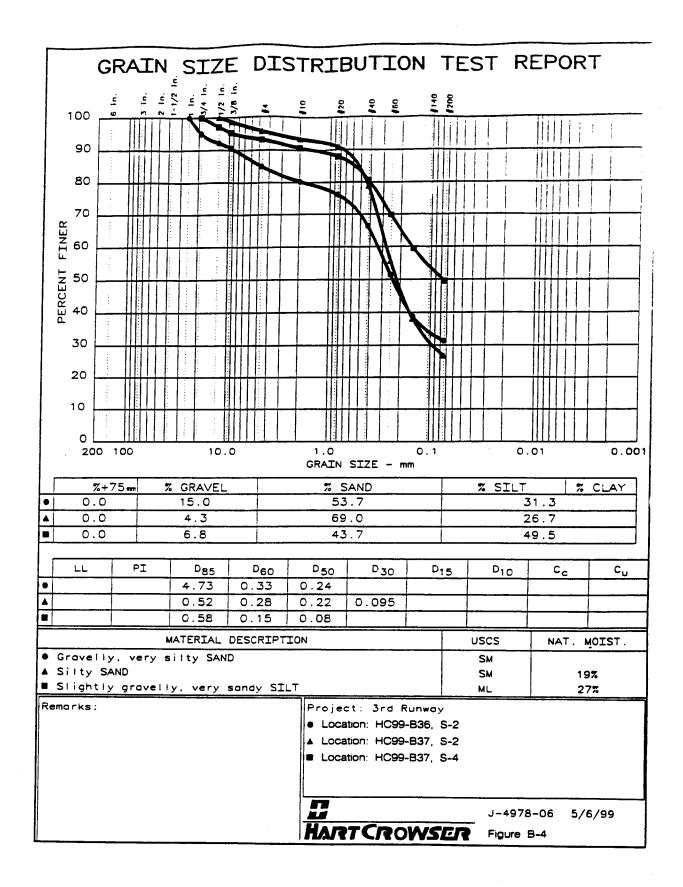
D₁₀, D₃₀, and D₆₀ are the particles diameter of which 10, 30, and 60 percent, respectively, of the soil weight are finer.

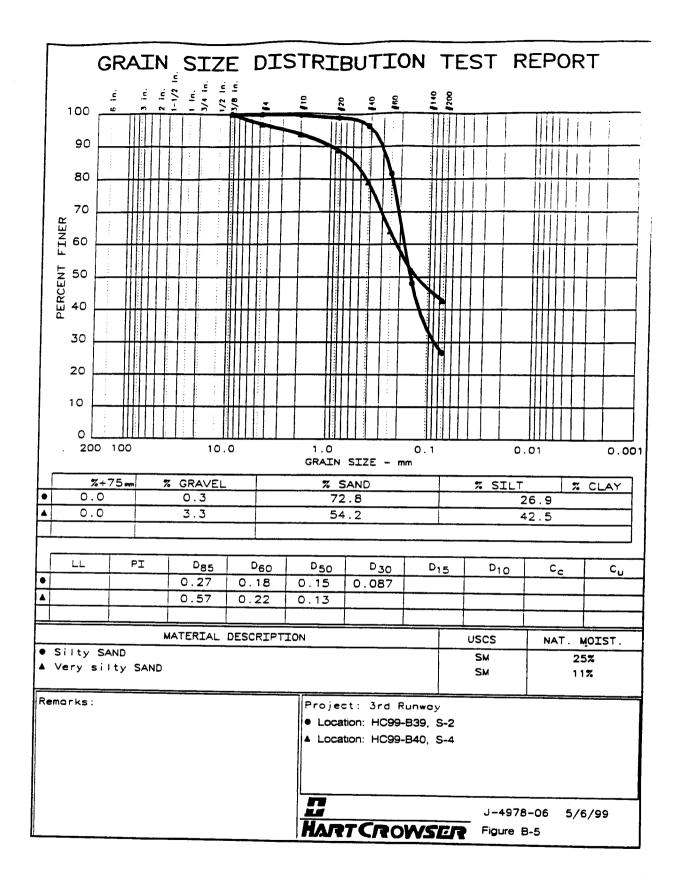
Fine-Grained Soils

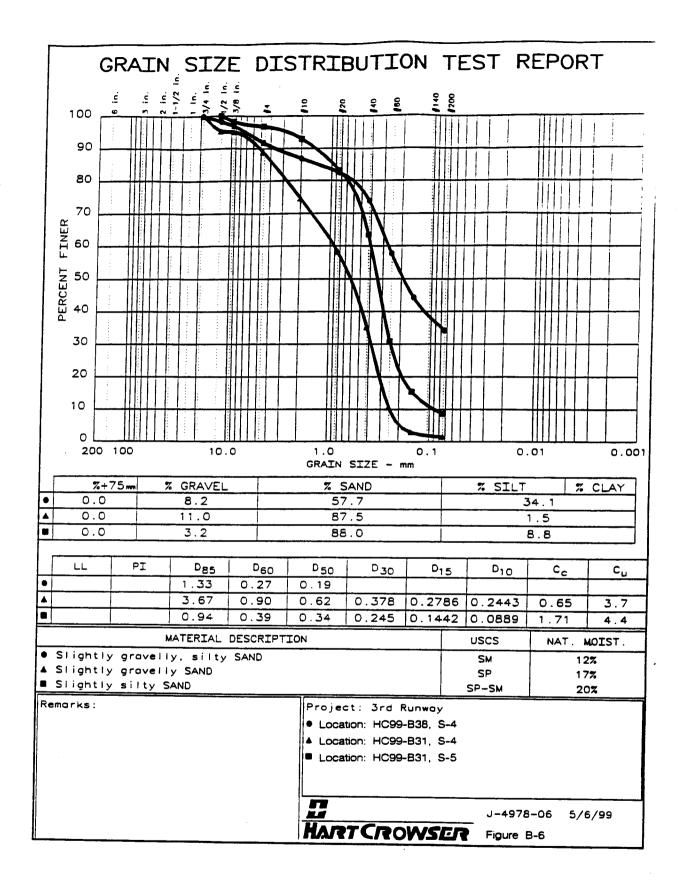


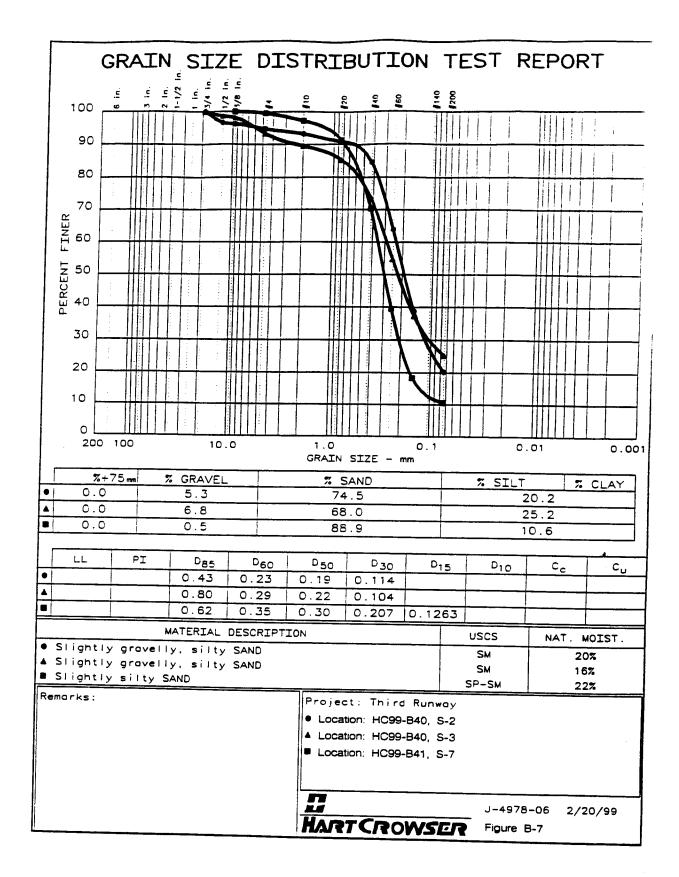


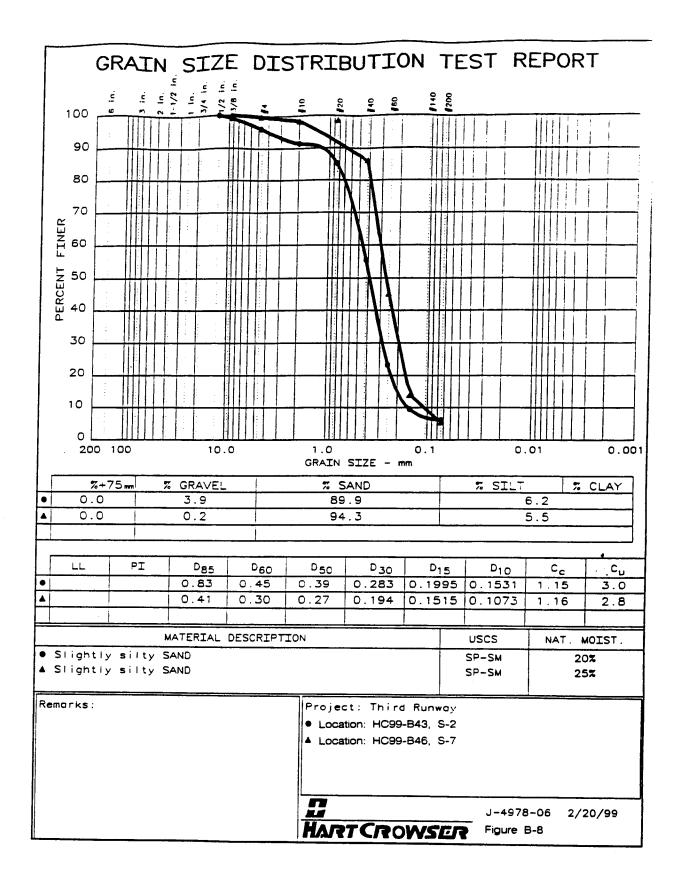


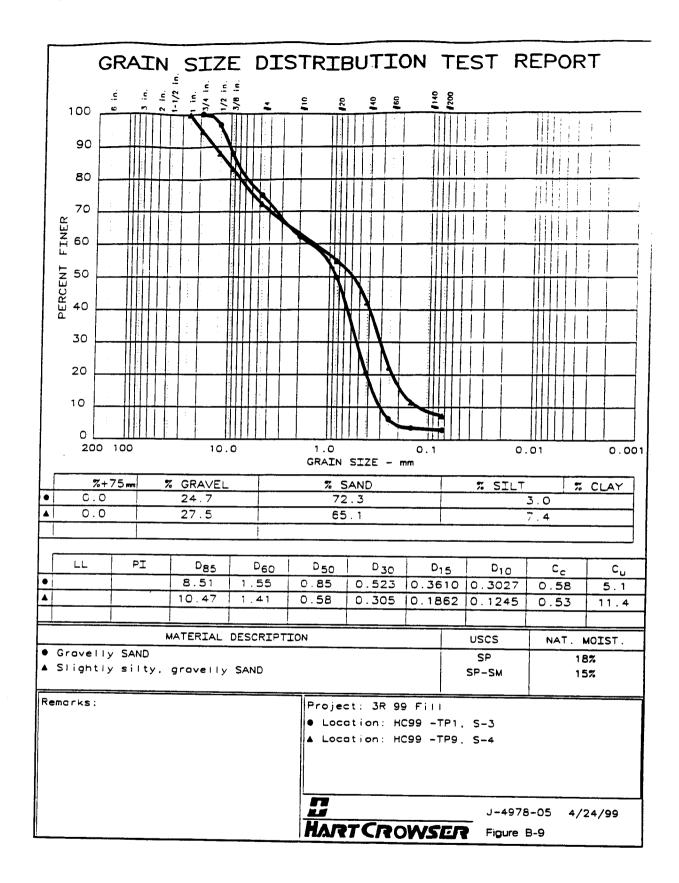


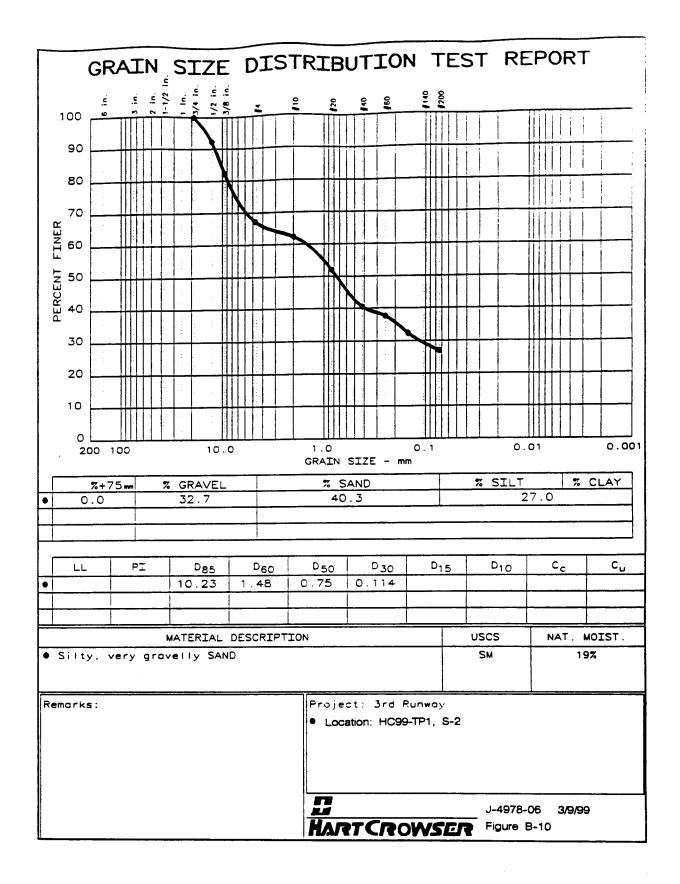


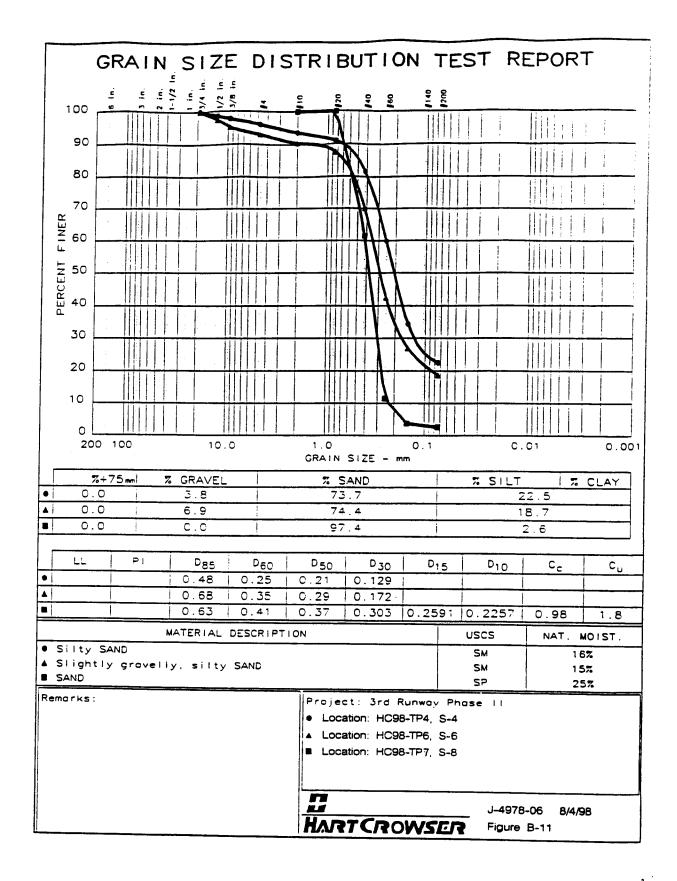


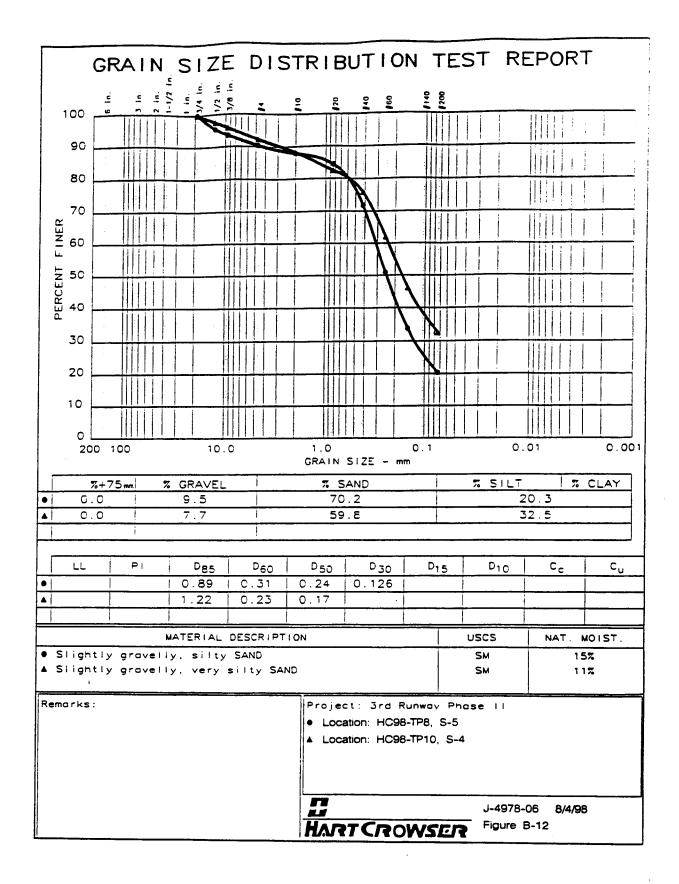












LIQUID AND PLASTIC LIMITS TEST REPORT							
60					or OH		
50							
	CL or OL						
PLASTICITY INDEX							
ASTICI 6							
ਕੋ ₂₀	HATCHED AREA IS		\land				
10		ML or C				MH or OH	
0	10 20 30	40	50	60	> 70	80 90 100	
LIQUID LIMIT							
	Description	LL	PL	PI	-200	ASTM D 2487-90	
 HC99-B47A, S-1 Depth 12.5 to 15 feet 			20	10		Clayey, fine SAND	
▲ HC99-B47, S-2 Depth 7.5 to 9 feet			19	10		Sandy CLAY	
■ HC99-B47, S-4 Depth 12.5 to 15 feet			21	11		Sandy CLAY	
Remarks: Project: 3rd Runway							
HC99-B47A, S-1, confirmed clayey, fine SAND using 200 wash mechanical sieve procedure; Client:							
Location: SeaTac Airport, Washington							
	J-4978-06 4/30/99						
		HA	RTC	ROWS	ER	Figure B-13	

